

ISSMGE TC 202, 2nd Japan-China Mini Workshop on High Speed Railway Geotechnics

Mechanical Properties of Reinforced Soil after Multiple Freeze-Thaw Cycles

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Lime and Cement Modified Soil for Harbin-Dalian HSR



Experimental Study on the Dynamic Properties of Cement- and Lime-Modified Clay Subjected to Freeze-Thaw Cycles. Cold Regions Science and Technology. Vol.61, No.1(2010), 29-33. Web of Science



Critical Dynamic Stress

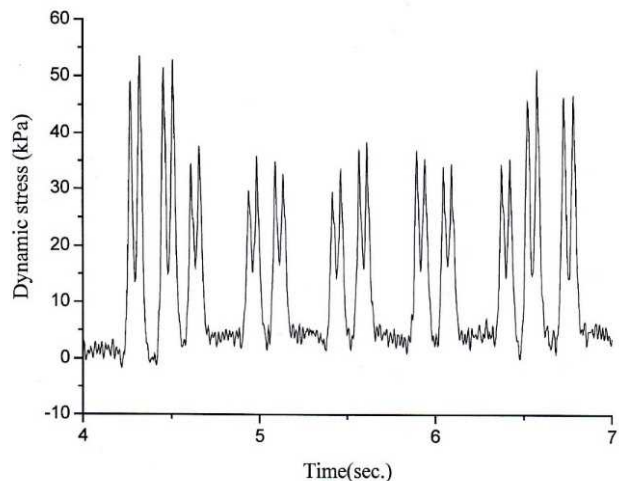


Fig. 1 Typical dynamic stress shape on subgrade surface

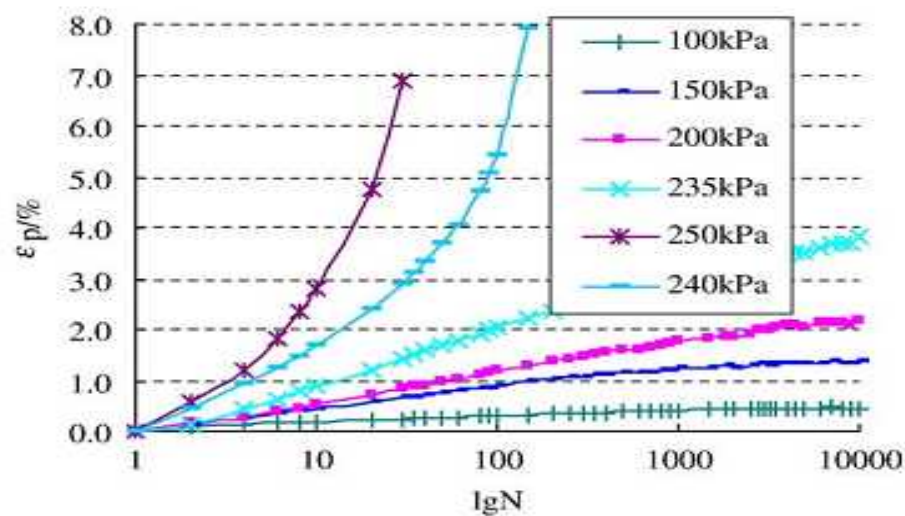
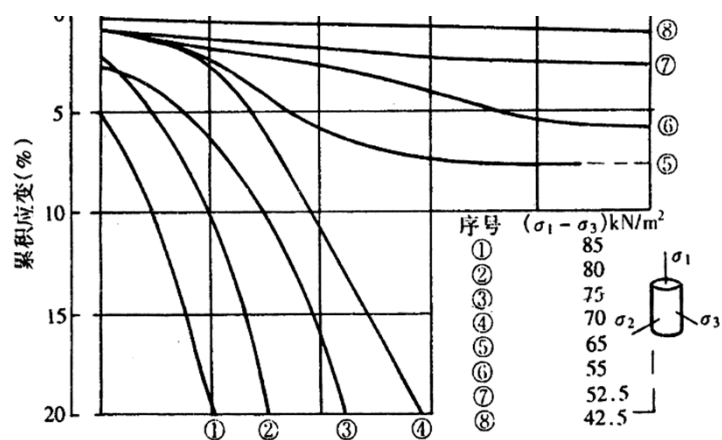
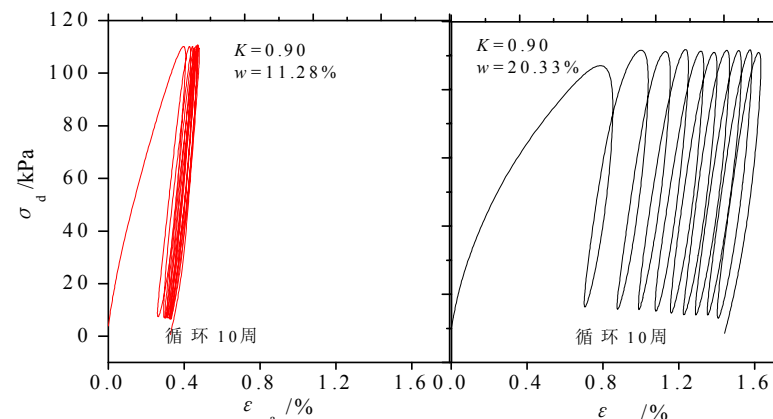


Fig. 5. ϵ_p -lgN curves of clay soil (20 kPa).

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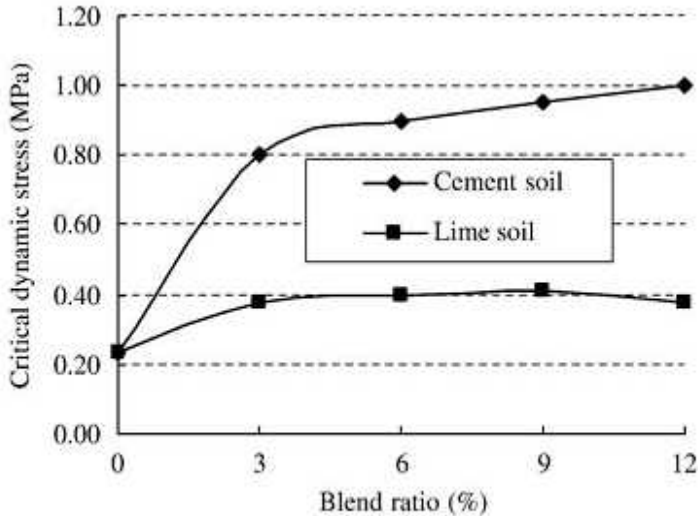


Fig. 6. Critical dynamic stress vs. blend ratio (20 kPa).

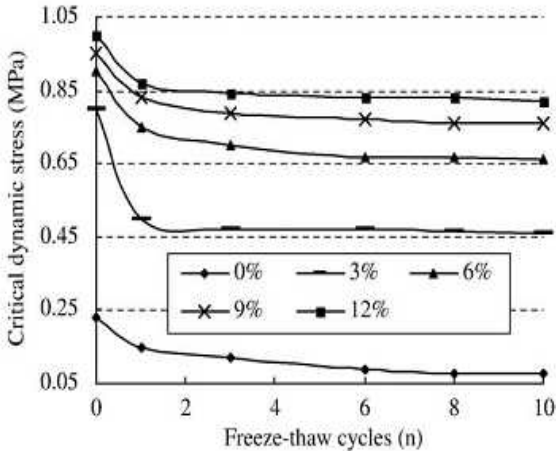


Fig. 7. Critical dynamic stress of cement-modified soil and clay vs. freeze-thaw cycles (confining pressure is 20 kPa).

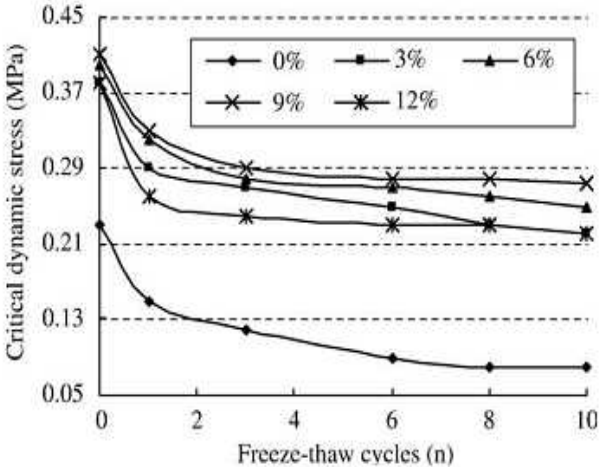


Fig. 8. Critical dynamic stress of lime-modified soil and clay vs. freeze-thaw cycles (confining pressure is 20 kPa).

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$$\eta_f = 1 - \frac{\sigma_{dcrb} - \sigma_{dcra}}{\sigma_{dcrb}}$$

- where σ_{dcrb} is the critical dynamic stress before a freeze-thaw cycle, and σ_{dcra} is the critical dynamic stress after a freeze-thaw cycle.

Table 3

Critical dynamic stress attenuation coefficient of modified soil and clay subjected to freeze-thaw cycles.

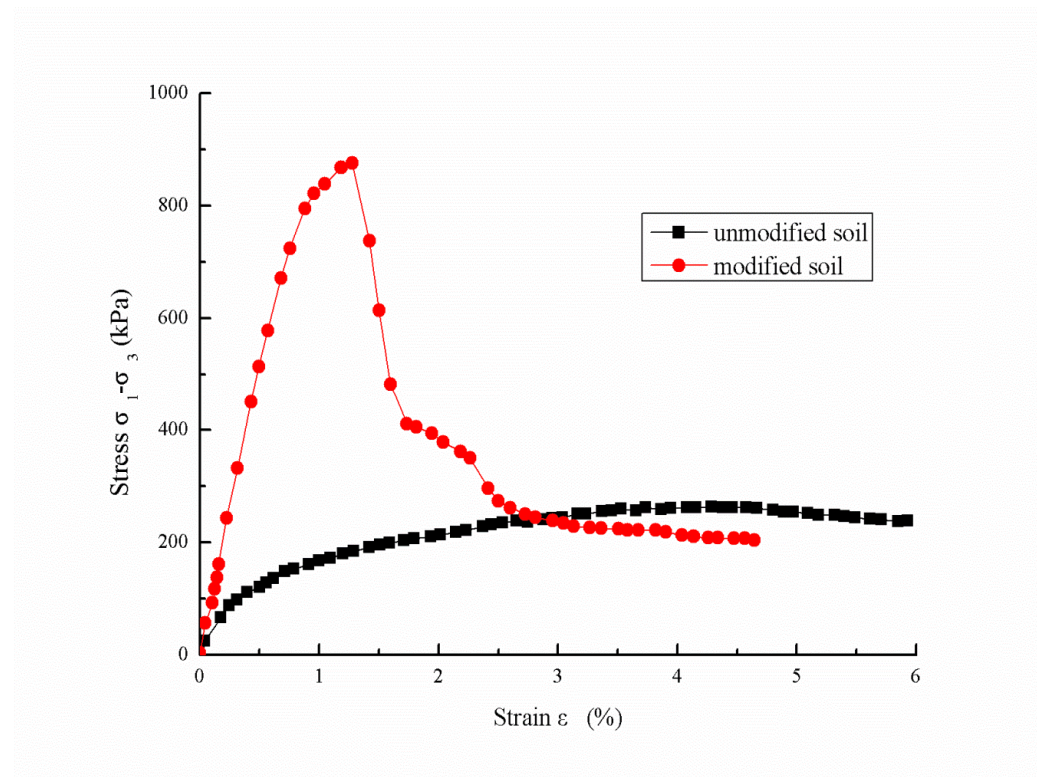
Freeze-thaw number	Critical dynamic stress attenuation coefficient of cement soil				Clay soil
	3%	6%	9%	12%	
1	0.63	0.83	0.87	0.87	0.65
3	0.59	0.78	0.83	0.84	0.52
10	0.58	0.73	0.80	0.82	0.35
Freeze-thaw number	Critical dynamic stress attenuation coefficient of lime soil				
	3%	6%	9%	12%	
1	0.76	0.80	0.80	0.68	
3	0.71	0.70	0.71	0.68	
10	0.58	0.63	0.67	0.68	

Experimental Study on the Dynamic Properties of Cement- and Lime-Modified Clay Subjected to Freeze-Thaw Cycles. Cold Regions Science and Technology. Vol.61, No.1(2010), 29-33. Web of Science

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The effect of freeze-thaw cycles on the static properties of modified Clay using Solidifying Agent

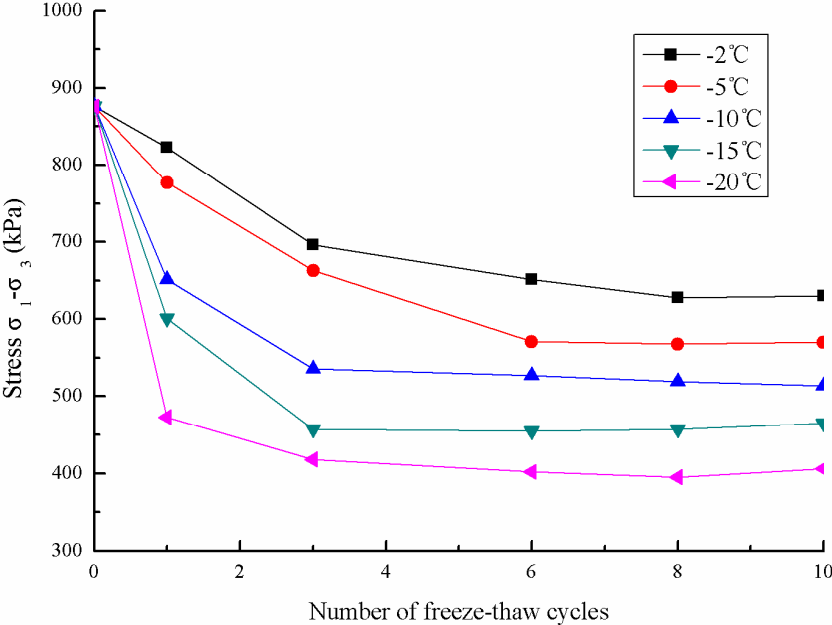
- Solidifying Agent, “Aught-Set” 3%,
- Freezing Temperature: -2°C , -5°C , -10°C , -15°C , -20°C
- Confining Pressure 20KPa



- The static strength of unmodified soil is 262kPa.
- the static strength of modified soil is 876kPa.

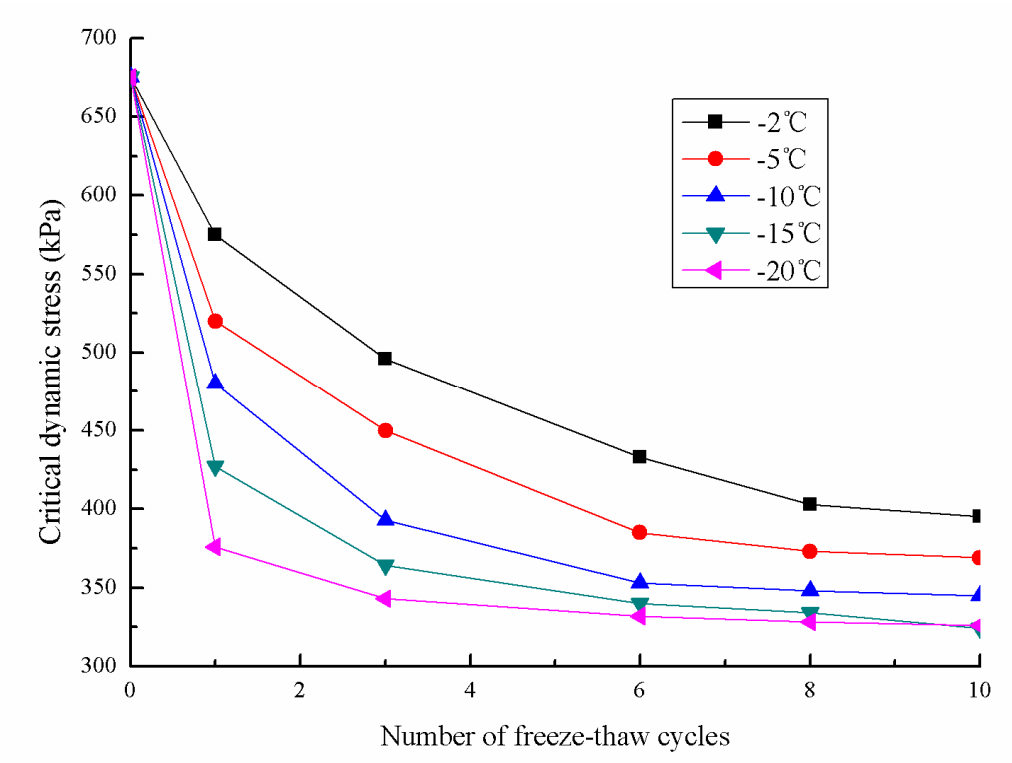
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The effect of freeze-thaw cycles on the static properties of modified Clay using Solidifying Agent



- The static strength of modified soil with different number and negative temperature of freeze-thaw cycles

The effect of freeze-thaw cycles on the dynamic properties of modified soil



- The relationship between critical dynamic stress, CDS and the freeze-thaw cycles

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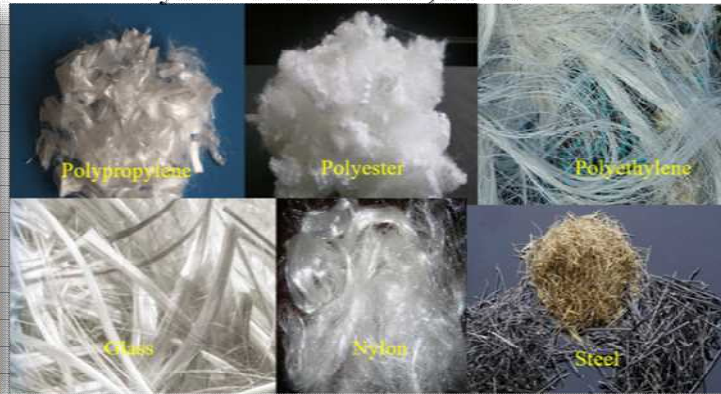
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Freeze-Thaw Effect on Fiber-Reinforced Soil

Natural Fibers



Synthetic Materials, Fibers



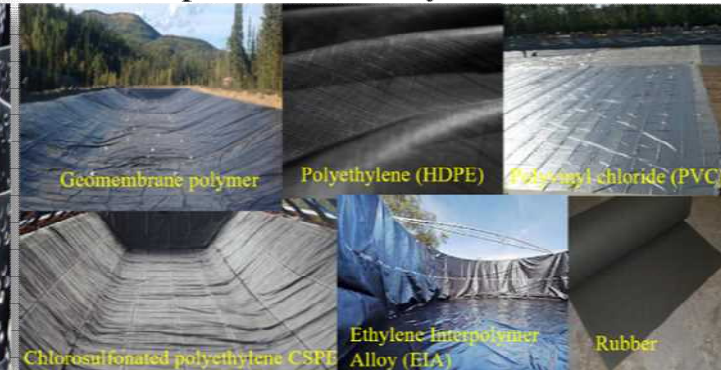
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- Long service life,
- Light weight
- Increase strength
- Lower thermal conductivity

Synthetic Materials, Geosynthetics

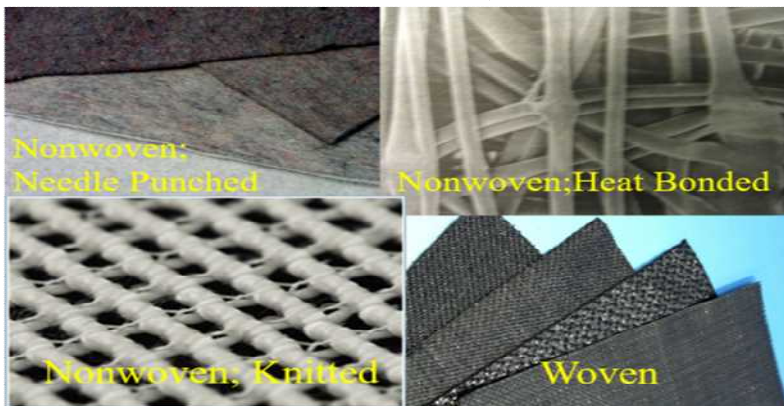


Impermeable, Geosynthetics



1. Glass fiber
Effective bulk density, hardness, stability, and flexibility and stiffness.

Permeable, Geosynthetics



2. Basalt fiber
Stabilization of road and highway to maintain the pavement life by decreasing the effects of cracks caused by excessive traffic loading, age hardening and temperature changes.





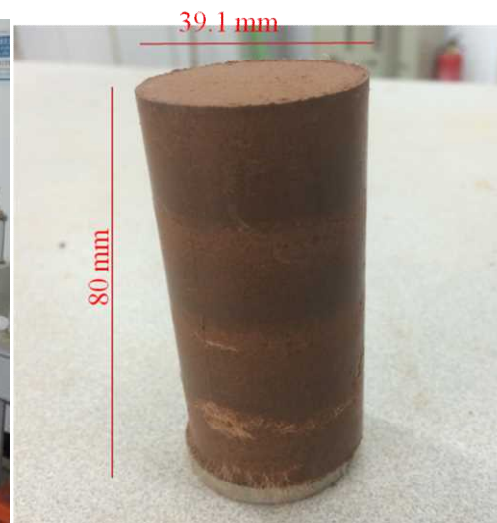
	Soil Properties	W _{opt} (%)	LL (%)	PI (%)	MDD (gr/cm ³)	Grain Composition* (%)			
						d>0.01	0.01 ≥d≥0.005	0.005≥d>0.005	d≤0.001
R1	-Physical properties -Mass loss -Changes of water content -Static triaxial test	12.9	30.04	12.09	1.93	78.87	7.96	7.30	5.86
R2	-Physical properties -Changes of height -Thermal conductivity test -Dynamic triaxial test	18.3	28.29	8.05	1.80	67.29	11.16	15.95	5.59
*Classified as CL according to		Fiber Properties				Basalt Fiber		Glass Fiber	
						Values		Values	
2nd Japan-China Mini Workshop on High Speed Railway Geotechnics						Modulus of elasticity		74 GPa	
						86.2 GPa			
						Breaking extension		4.7 %	
						3.1 %			
						Fiber diameter		10 μm	
						10 μm			
						Linear density		40-4,200 tex	
						60-4,200 tex			
						Length		15 mm	
						15 mm			
						Tensile strength		3450 MPa	
						3920 MPa			
						Thermal conductivity		0.04 W/m·K	
						0.03 W/m·K			

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Materials	(χ_w)
Glass Fiber (GF)	0%, 0.5%, 1%
Basalt Fiber (BF)	0%, 0.5%, 1%
Glass Fiber (GF)	0%, 0.5%, 1%
Basalt Fiber (BF)	0%, 0.5%, 1%
Glass Fiber (GF)	0%, 0.5%, 1%
Basalt Fiber (BF)	0%, 0.5%, 1%

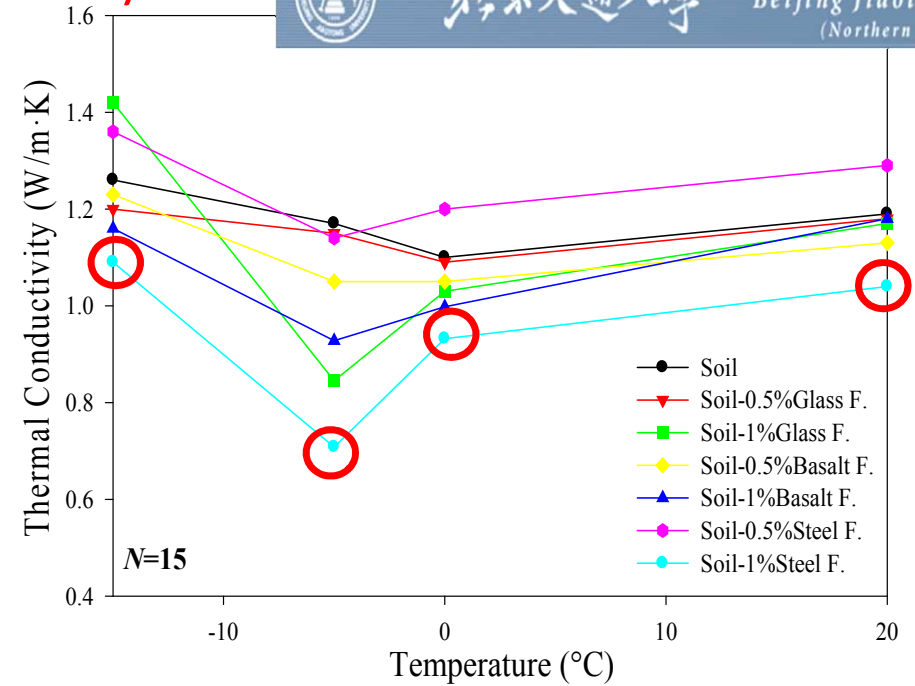
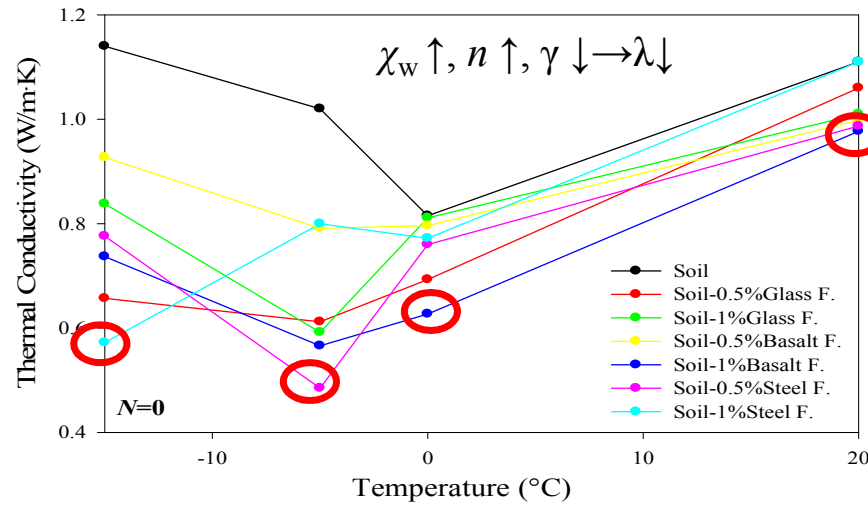
Series	Number of specimen	Dimension of test specimen (mm)		Freeze-thaw cycles	Temperature		Tested Temperature
		Height	Diameter		Freezing	Thawing	
Mass loss	12	80	39.1	0, 15	-20 °C	20 °C	~20 °C
Change of water content	12	80	39.1	0, 2, 5, 10, 15	-20 °C	20 °C	~20 °C
Change of height	12	80	39.1	0, 2, 5, 10, 15	-15 °C	20 °C	~20 °C
Thermal conductivity test	60	60	61.8	0, 2, 5, 10, 15	-15 °C	20 °C	20°C, 0°C, -5°C, -15°C
Static triaxial test	150	80	39.1	0, 2, 5, 10, 15	-20 °C	20 °C	~20 °C
Dynamic triaxial test	150	125	61.8	0, 2, 5, 10, 15	-15 °C	20 °C	~20 °C



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Thermal conductivity of fiber-reinforced soil



Dry density

Porosity

Saturation degree

Heat storage capacity,

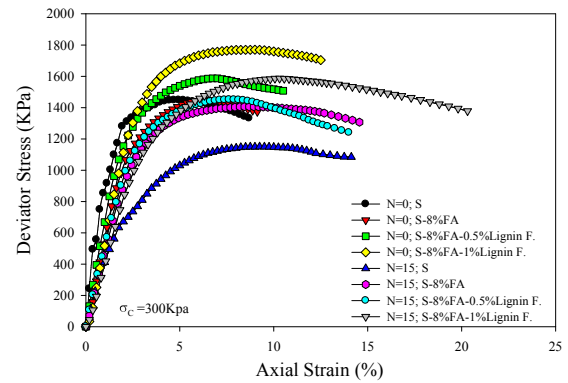
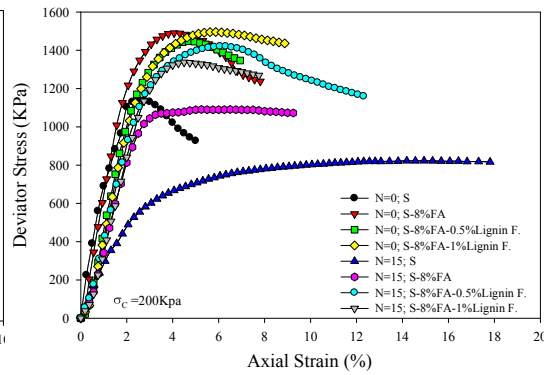
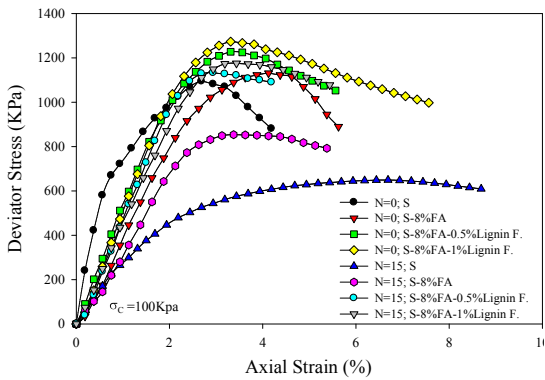
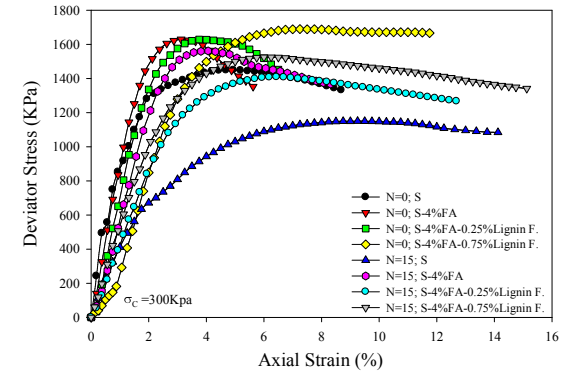
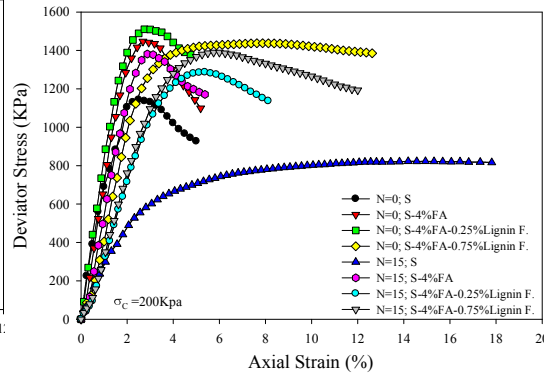
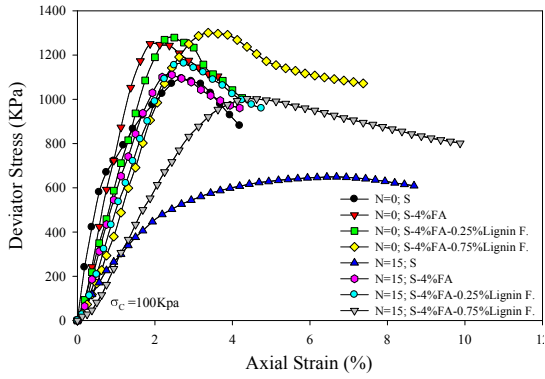
Saturation degree,

*Fiber dispersion in the mixture and
fiber type (unwoven or woven)*

Presence unfrozen water

$$\lambda_{\text{frozensoil}} > \lambda_{\text{unfrozensoil}} \rightarrow \lambda_{\text{ice}} > \lambda_{\text{water}}$$

- As $T \downarrow \rightarrow$ ice content in the soil \uparrow , *the density of the ions changes* in the phase boundary.
- During the thawing process, exchange cations exhibit the behavior of rehydration.
- $\gamma \uparrow \rightarrow \lambda \uparrow$



Static UU Triaxial

No	σ_c	χ_w	4FA	8FA	N	$(\sigma_1 - \sigma_3)_{max}$
1	→	0	↑	0	0	↑
2	→	0	0	↑	0	↑
3	→	↑	↑	0	0	↑
4	→	↑	0	↑	0	↑
5	↑	0/↑	↑	↑	0	↑
6	→	0	↑	0	↑	→
7	→	0	0	↑	↑	↑
8	→	↑	↑	0	↑	↑
9	→	↑	0	↑	↑	↑

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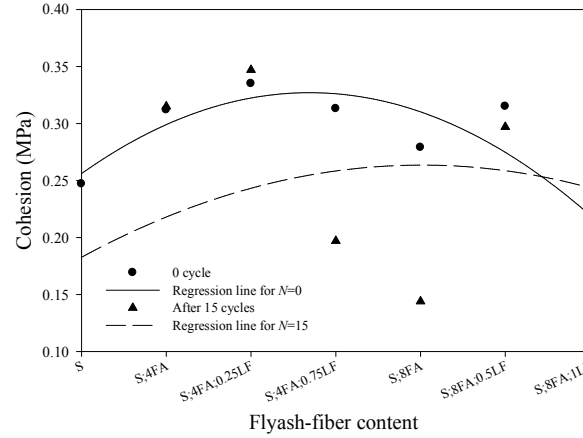
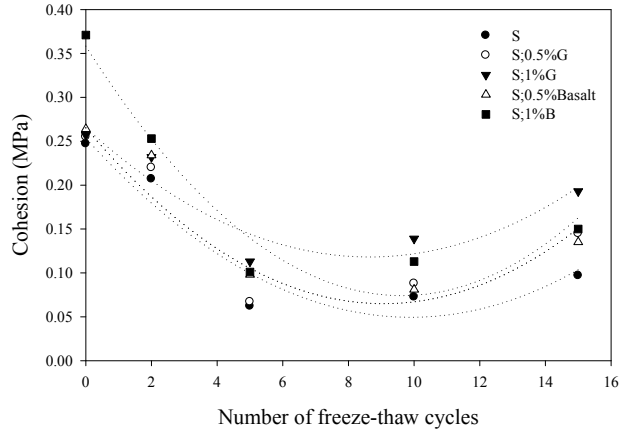
Static UU Triaxial

Cohesion and friction angles



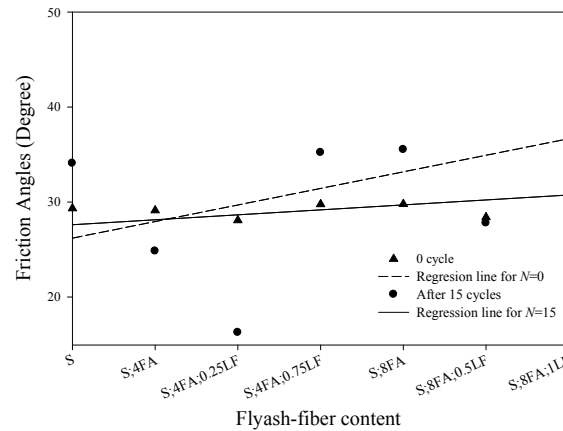
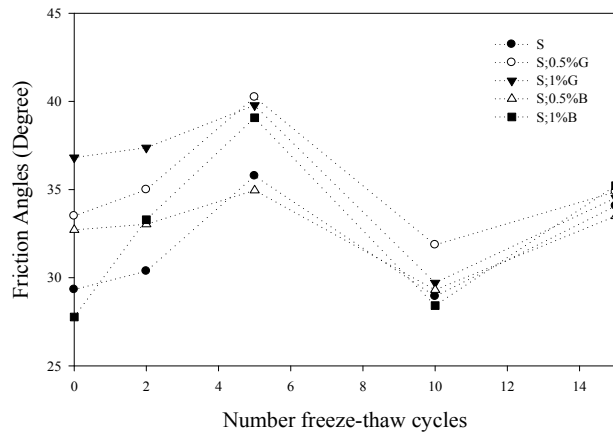
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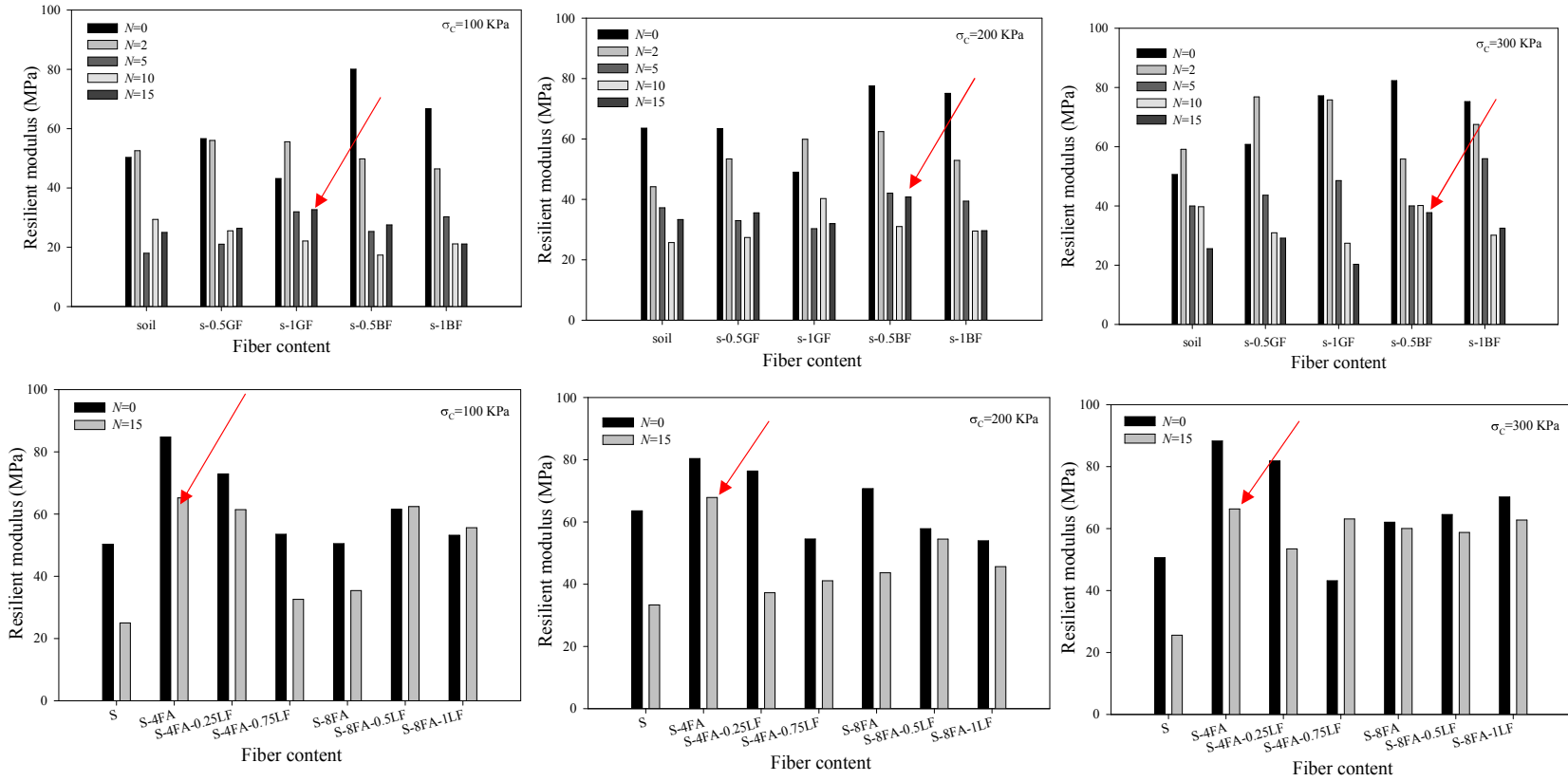
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	<i>Reduction ratio of cohesion</i>		<i>Reduction ratio of cohesion</i>
0.5% GF	43%	8% FA	48%
1% GF	25%	4% FA-0.75 %LF	37%
0.5% BF	49%	8% FA-0.5 %LF	6%
1% BF	59%		



$\phi \uparrow, w \downarrow$
 $N \uparrow, w \downarrow$
and $N=10$ w steadied.
 $\phi \uparrow, N \uparrow$

Resilient modulus $E = \frac{\Delta \sigma}{\Delta \varepsilon} = \frac{\sigma_{1.0\%} - \sigma_0}{\varepsilon_{1.0\%} - \varepsilon_0}$



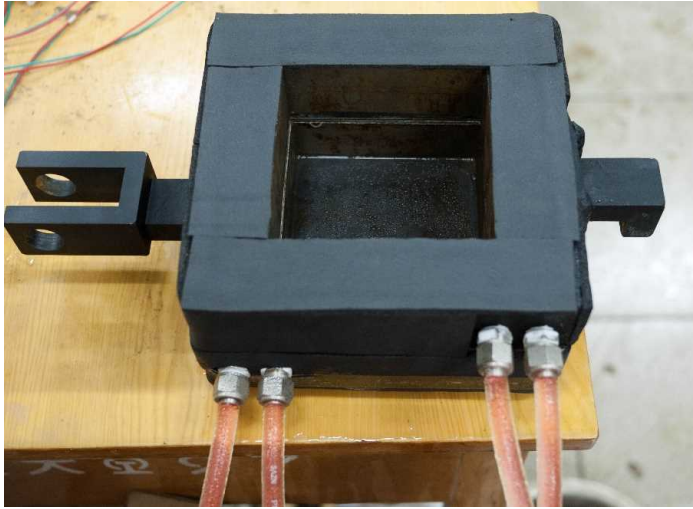
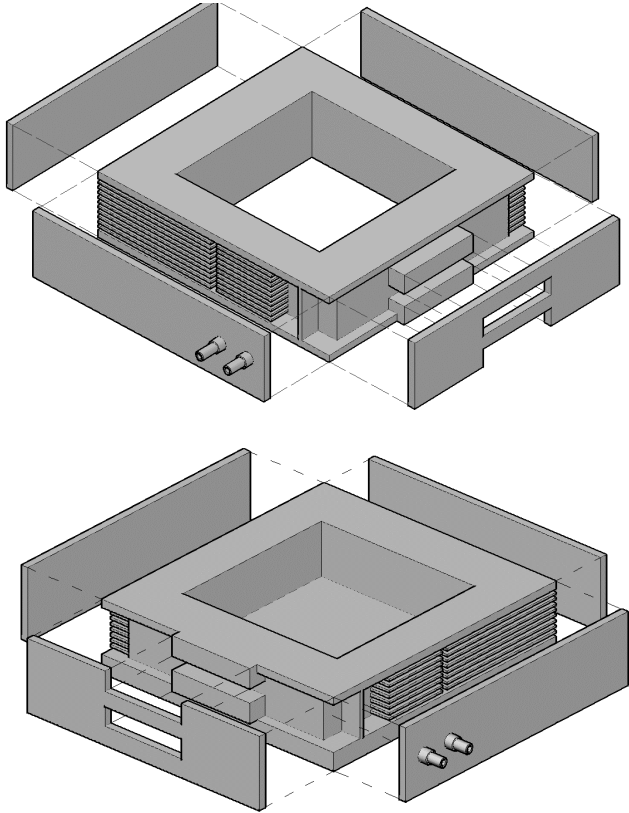
a resilient modulus < 55 kPa → negligible freeze-thaw effects
 a resilient modulus > 103 KPa → a decrease of more than 50 %

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Development of Dynamic Direct Shearing Box



Dynamic direct shear test — Temperature-controlled shear box



Schematic of temperature-controlled direct shear box

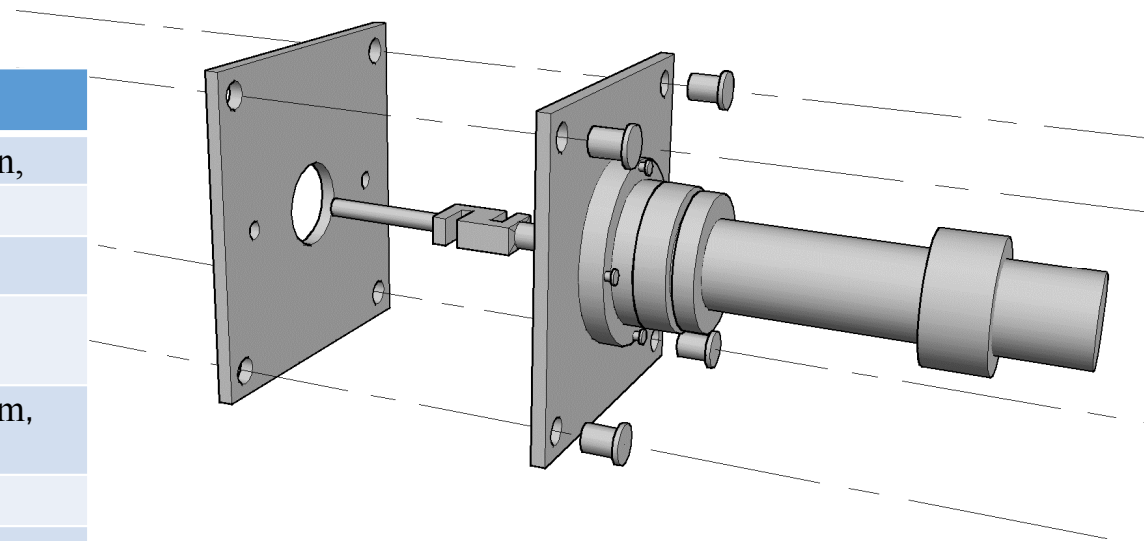


Dynamic direct shear test —

Dynamic actuator and connect to the workbench

Design Project	Load amplitude range (kN)	Piston stroke (mm)	Vibrational frequency (Hz)
Performance Parameters	1 ~ 20kN	-50mm ~ 50mm	0.5 ~ 5

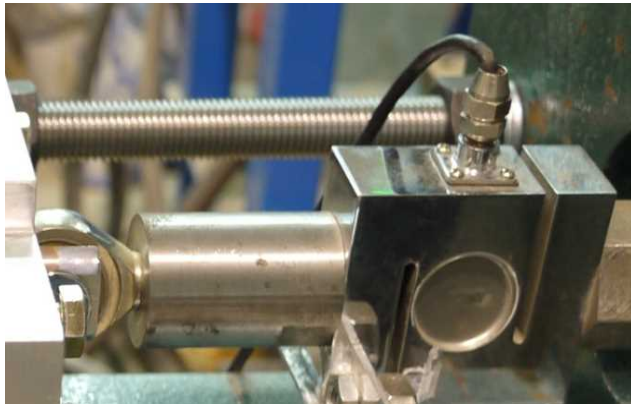
Unit name	Performance Parameters
Variable pump	Working pressure:7.0MPa, maximum flow:72L/min, System accuracy of filtration 25 μ
Pump motor	Motor power:15kW
Servo valve	Deflector jet valve: SFL223, no-load flow under 7MPa:60L/min
Actuator	Rated working pressure :7MPa, Piston stroke: 200mm, Piston diameter:70mm, Rod diameter:32mm
Fuel tank	Capacity:500L
Cooling tank	Water Cooling, column tubular oil cooler:2LQFL, Structural style: Tube-fin condenser, Cooling area:0.65m ² , Working Pressure:1MPa, Oil pressure drop \leq 0.1MPa, Water pressure drop \leq 0.015MPa, Working temperature of water:25~30 $^{\circ}$ C, Working temperature of oil \leq 100 $^{\circ}$ C。



Design of the actuator



Dynamic direct shear test — Measuring system



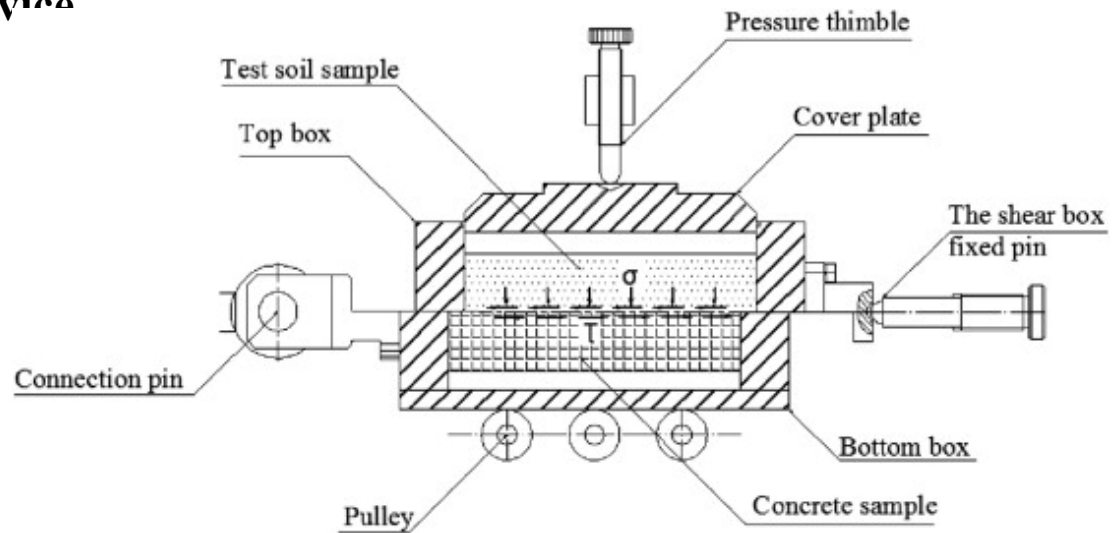
**Displacement and Force
Measuring Device**



Computer logger

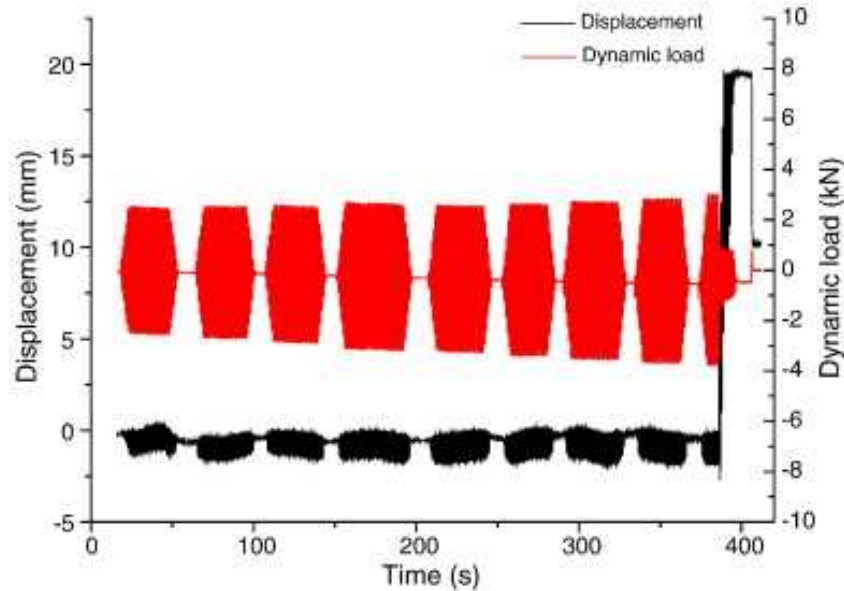


Temperature Sensor

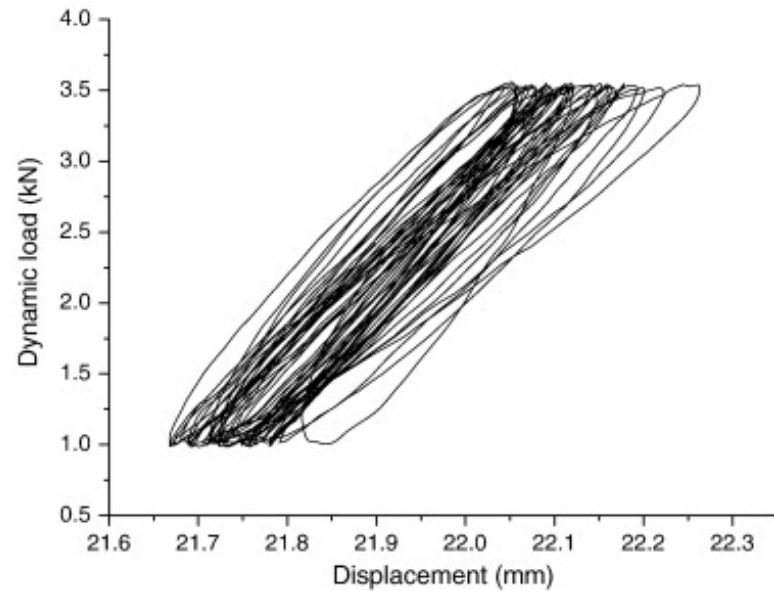




Dynamic direct shear test — Validation



Displacement and dynamic load curve of a typical loading process

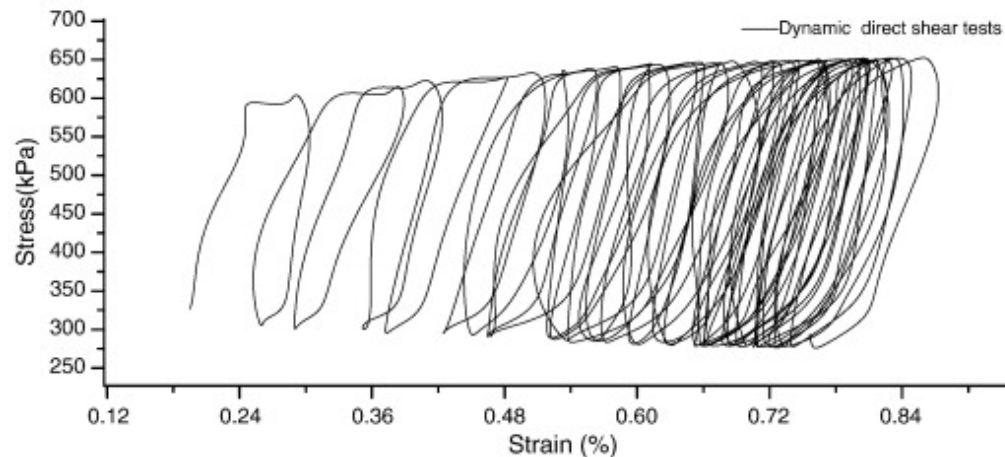
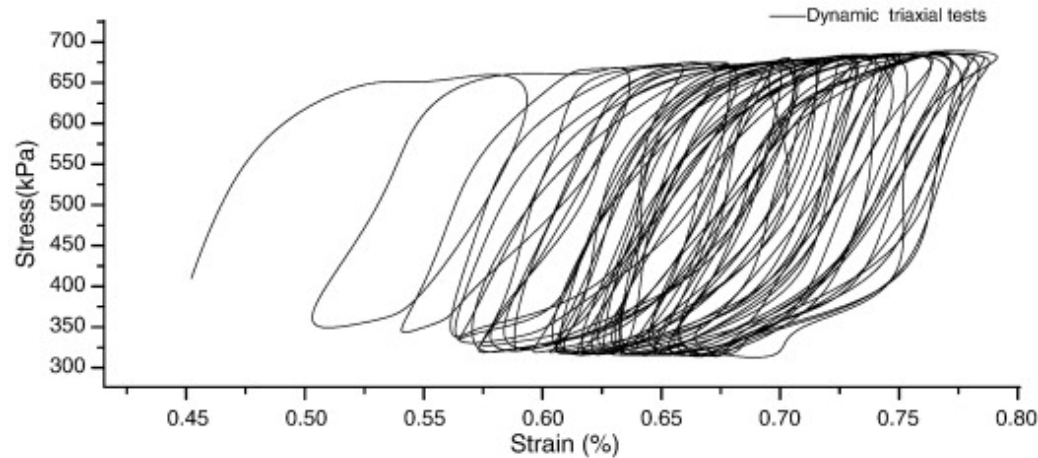


One level load–displacement hysteresis curve

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Dynamic direct shear test — Compared with the dynamic triaxial apparatus



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Comparison of hysteresis curve in two tests

Comparison with Triaxial Tests

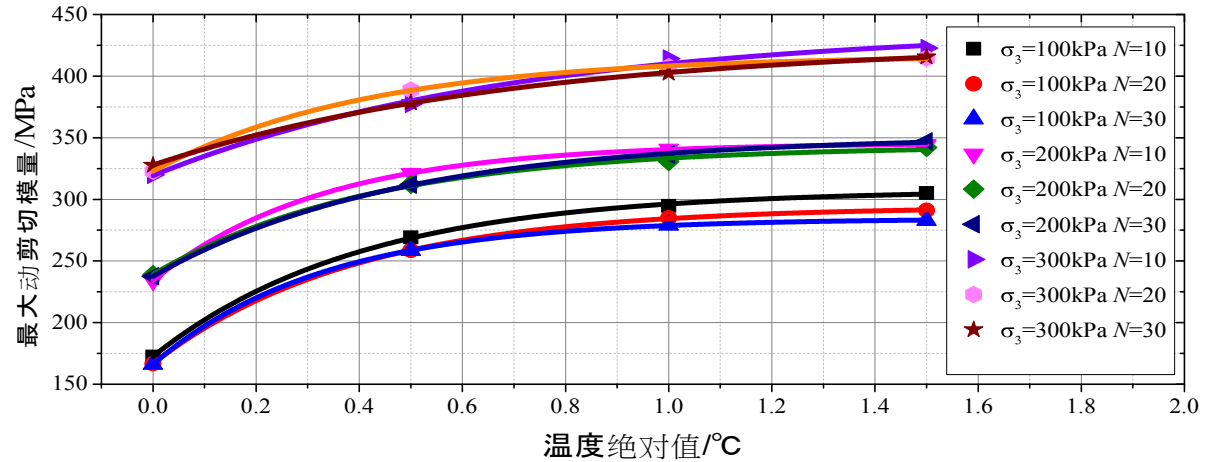
- Modulus of Frozen Soil
- Damping Ratio of Frozen Soil

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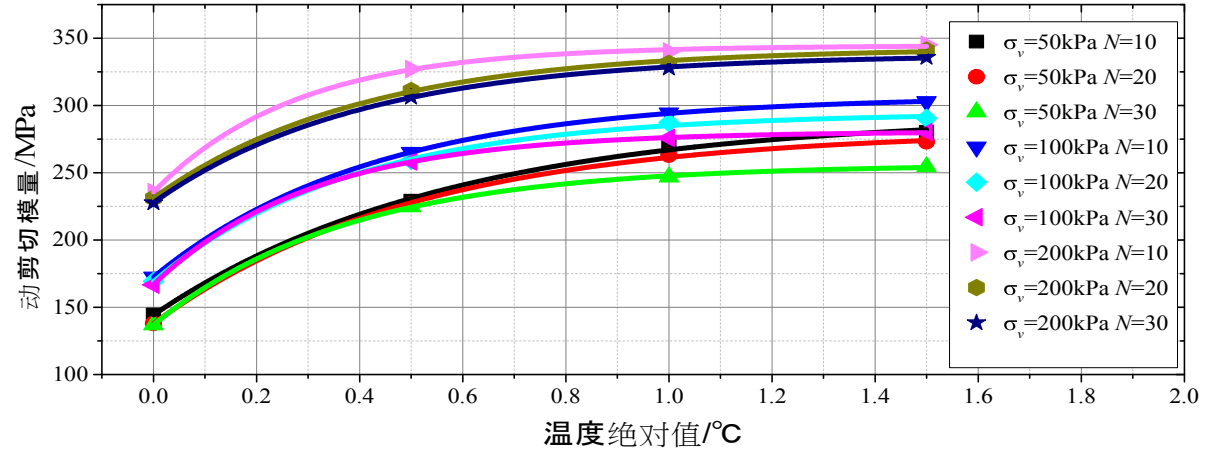


Dynamic modulus — Influenced by Temperature

Temperature controlled
Dynamic triaxial test



Temperature Controlled
Dynamic Direct shear test



$$G_{dmax} = A_1 \cdot \exp(-|T_c|/B_1) + G_{d0}$$



Dynamic modulus — Influenced by **Temperature**

$$G_{\text{dmax}} = A_1 \cdot \exp(-|T_c| / B_1) + G_{\text{d0}}$$



$$\sigma_3 = 100 \text{ kpa}$$

$$N = 30$$

**Temperature controlled
Dynamic triaxial test**

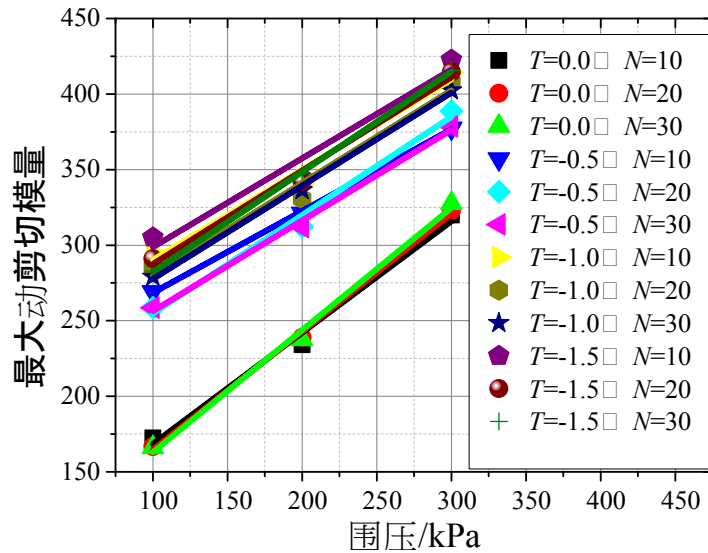
$$G_{\text{dmax}} = -118.303 \exp(-|T_c| / 0.328) + 284.184 \left. \vphantom{G_{\text{dmax}}} \right\}$$
$$R^2 = 0.9901$$

**Temperature Controlled
Dynamic Direct shear test**

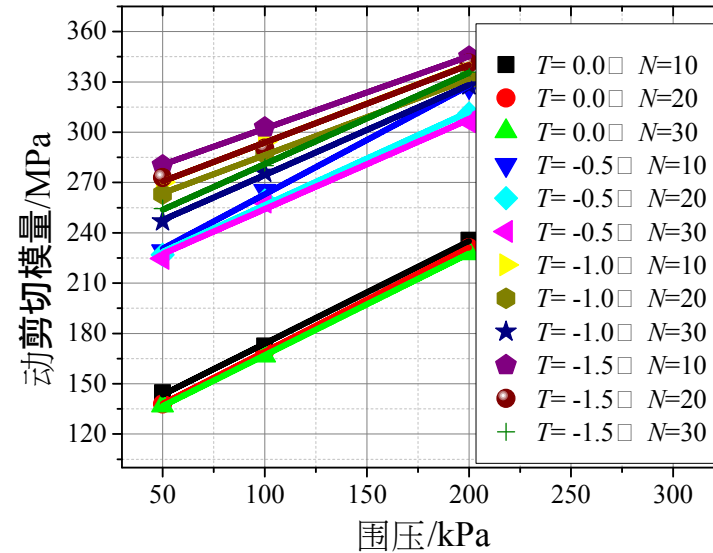
$$G_{\text{dmax}} = -113.873 \exp(-|T_c| / 0.308) + 265.653 \left. \vphantom{G_{\text{dmax}}} \right\}$$
$$R^2 = 0.9974$$



Dynamic modulus — Influenced by **Confining pressure**



Dynamic triaxial test



Direct shear test



$T_c = -1.0^\circ\text{C}$ $N = 20$

$$G_{\text{dmax}} = 218.461 + 0.613\sigma$$

$$G_{\text{dmax}} = 241.053 + 0.453\sigma$$



Dynamic modulus — Influenced by Moisture content

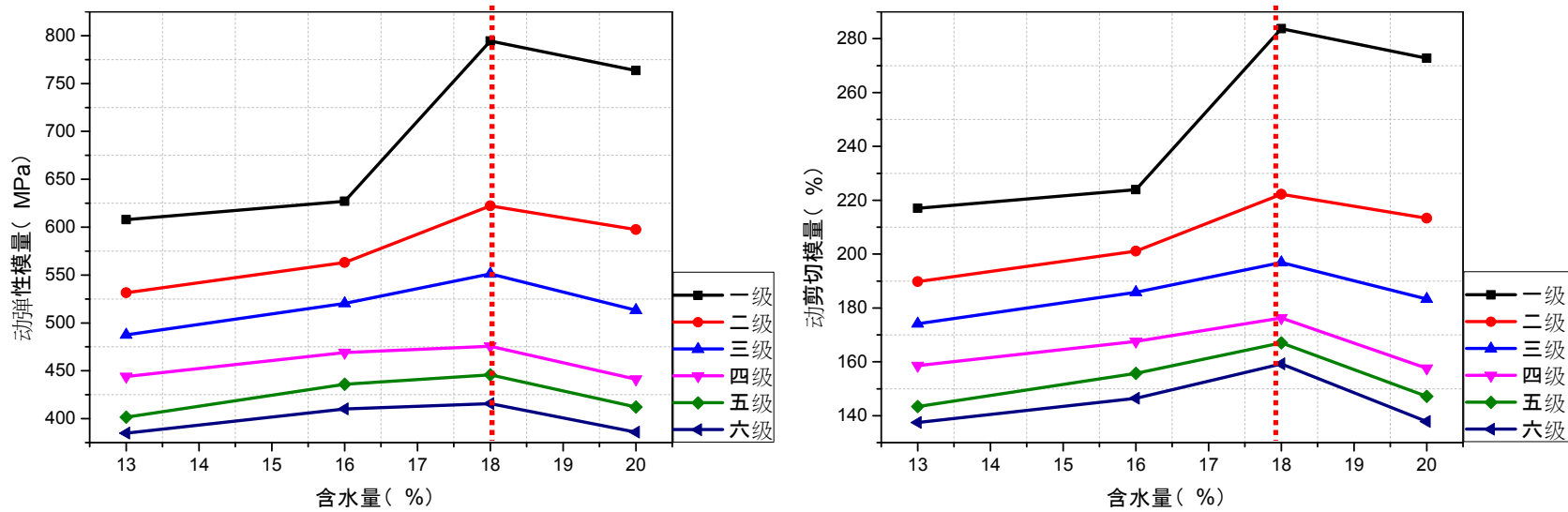


Fig. Relationship between dynamic modulus and different water content

Test parameters	Dynamic tri-axial test	Dynamic direct shear
Temperature(°C)	-1.5	-1.5
Confining pressure(Mpa)	0.5	0.5
Moisture content(%)	13, 16, 18, 20	13, 16, 18, 20
Vibration frequencies(Hz)	1	1



Dynamic modulus — Influenced by Loading Cycles

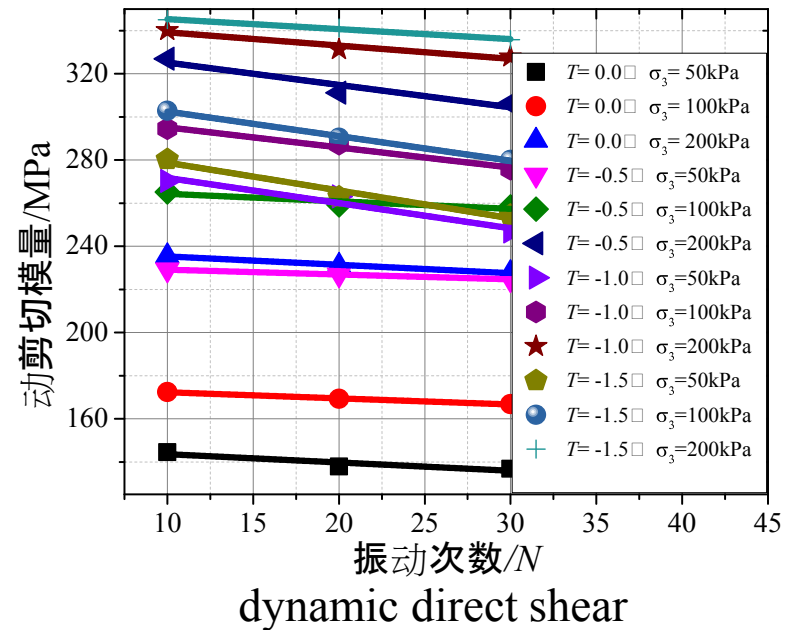
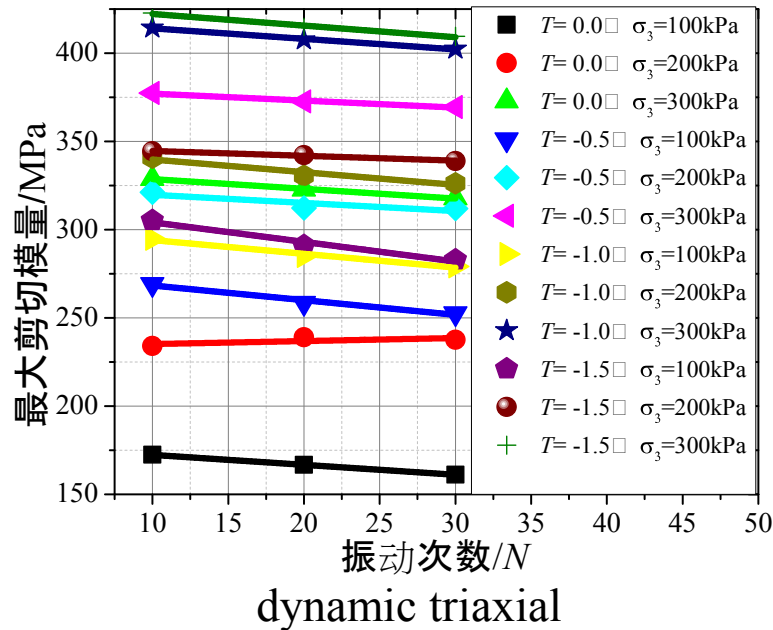


Fig. Reference shear strain vs. vibration times curve

$$G_{dmax} = G_0 + G_1 N$$



Dynamic modulus — Influenced by Frequencies

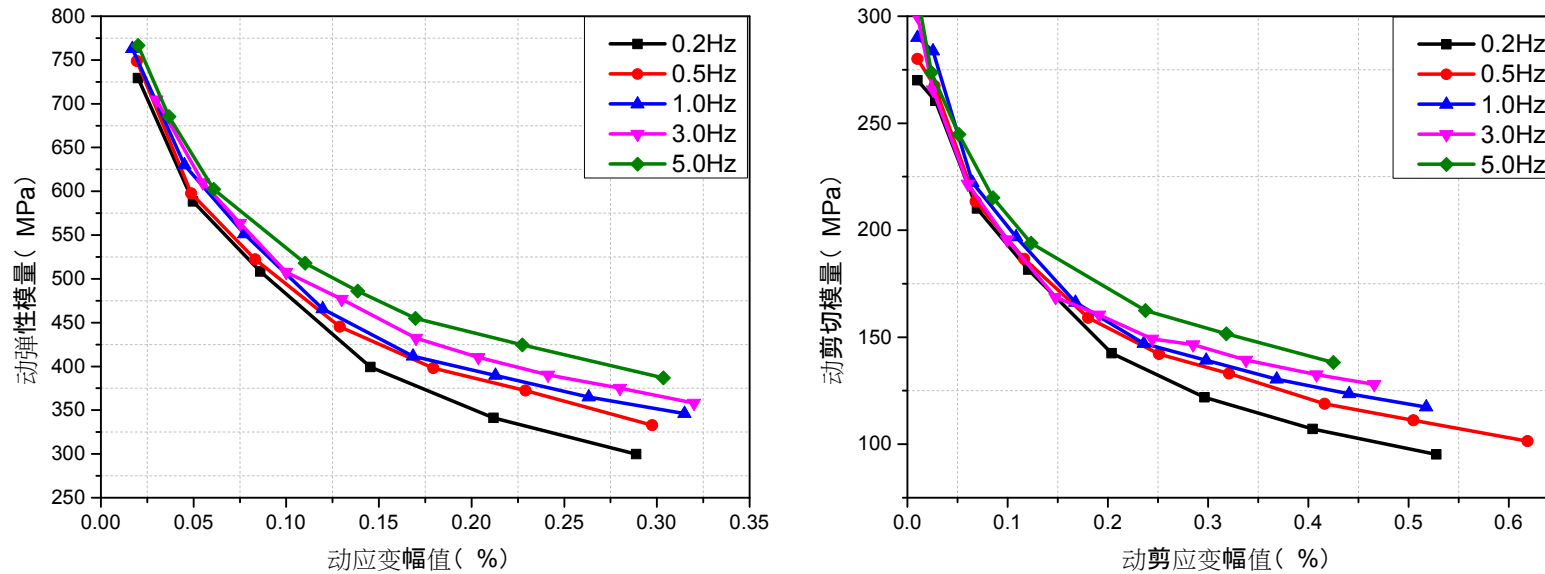


Fig. Relationship between dynamic elastic modulus and dynamic strain amplitude with different vibration frequencies

Test parameters	Dynamic tri-axial test	Dynamic direct shear
Temperature(°C)	-1.5	-1.5
Confining pressure(Mpa)	0.5	0.5
Moisture content(%)	18	18
Vibration frequencies(Hz)	0.2, 0.5, 1.0, 3.0, 5.0	0.2, 0.5, 1.0, 3.0, 5.0



Dynamic modulus — A function of Temperature, Confining pressure and load cycles

$$G_{dmax} = f(T_c, \sigma_3, N)$$

**Temperature Controlled
Dynamic triaxial test**

$$\left. \begin{aligned} G_{dmax} &= 142.21 + 187.42T_c - 63.81T_c^2 \\ &+ 49.46\left(\frac{\sigma_3}{100}\right) - 1.98\left(\frac{\sigma_3}{100}\right)^2 - 6.47\left(\frac{N}{10}\right) \end{aligned} \right\}$$
$$R^2 = 0.9852$$

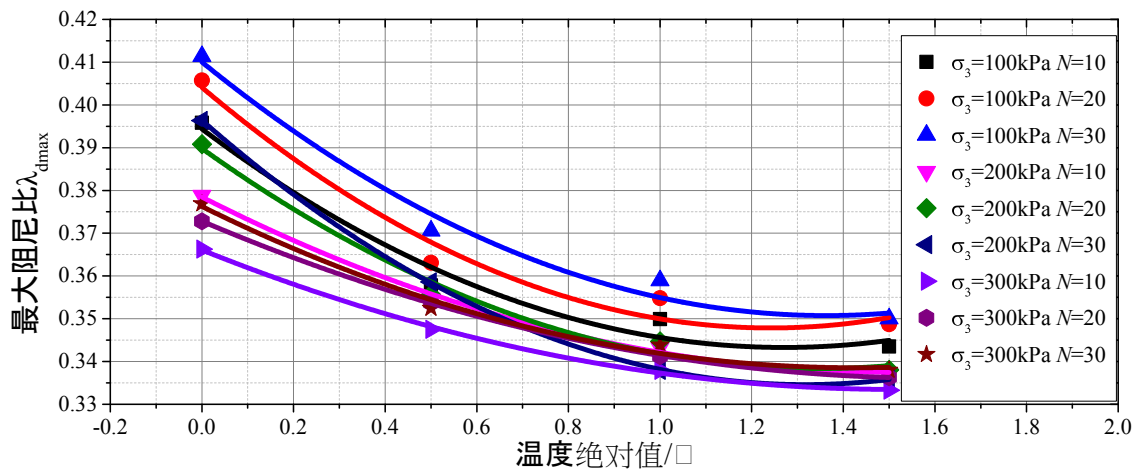
**Temperature Controlled
Dynamic Direct shear test**

$$\left. \begin{aligned} G_{dmax} &= 133.07 + 195.75T_c - 79.95T_c^2 \\ &+ 58.18\left(\frac{\sigma_v}{100}\right) - 1.66\left(\frac{\sigma_v}{100}\right)^2 - 7.31\left(\frac{N}{10}\right) \end{aligned} \right\}$$
$$R^2 = 0.9827$$

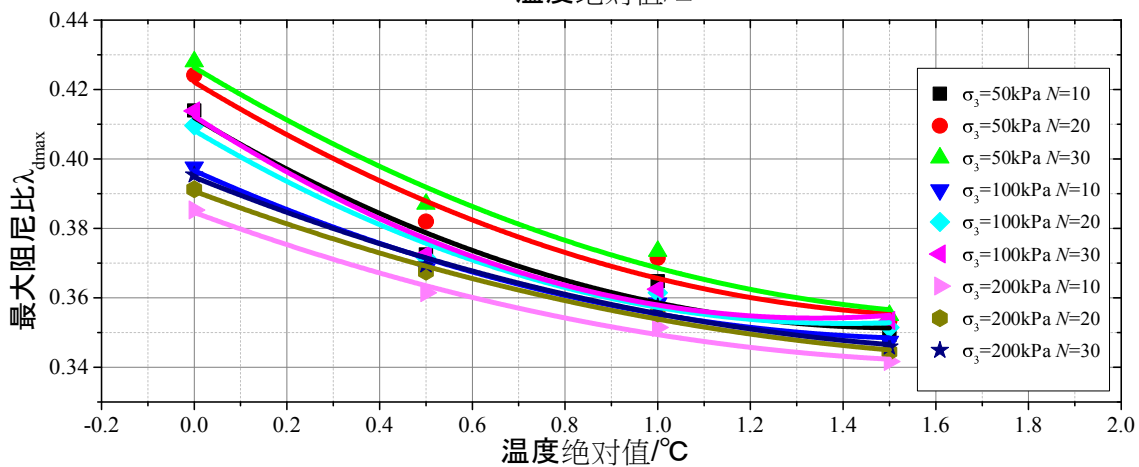


Damping ratio — Temperature

Dynamic triaxial test



Direct shear test



$$\lambda_{dmax} = \lambda_1 + \lambda_2 \cdot |T_c| + \lambda_3 \cdot |T_c|^2$$



Damping ratio — A function of Temperature, Confining pressure and load cycles

$$\lambda_{dmax} = f(T_c, \sigma_3, N)$$

Dynamic triaxial test

$$\lambda_{dmax} = 0.3948 - 0.06074T_c + 0.0174T_c^2 - 0.0089\left(\frac{\sigma_3}{100}\right) + 0.00019\left(\frac{\sigma_3}{100}\right)^2 + 0.00429N$$
$$R^2 = 0.9708$$

Direct shear test

$$\lambda_{dmax} = 0.4156 - 0.06744T_c + 0.02078T_c^2 - 0.00744\left(\frac{\sigma_3}{100}\right) + 0.005667\left(\frac{\sigma_3}{100}\right)^2 + 0.004457N$$
$$R^2 = 0.9838$$

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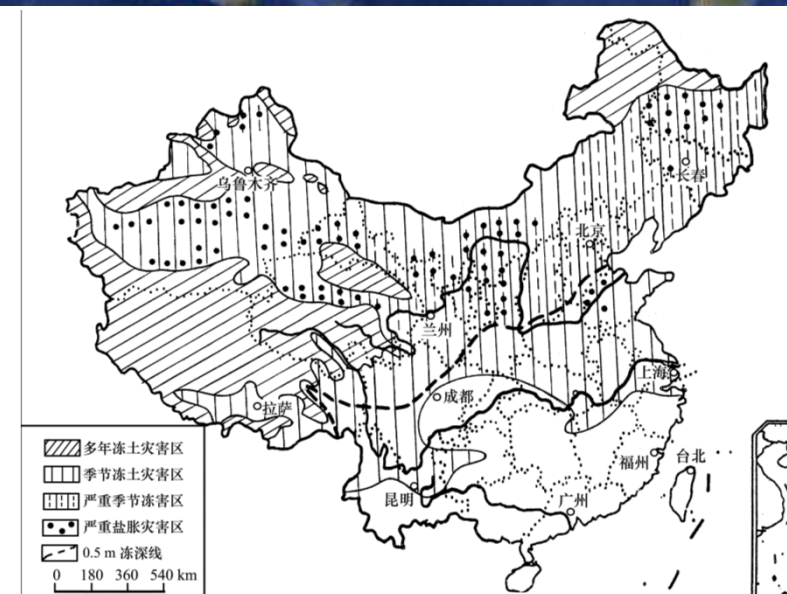
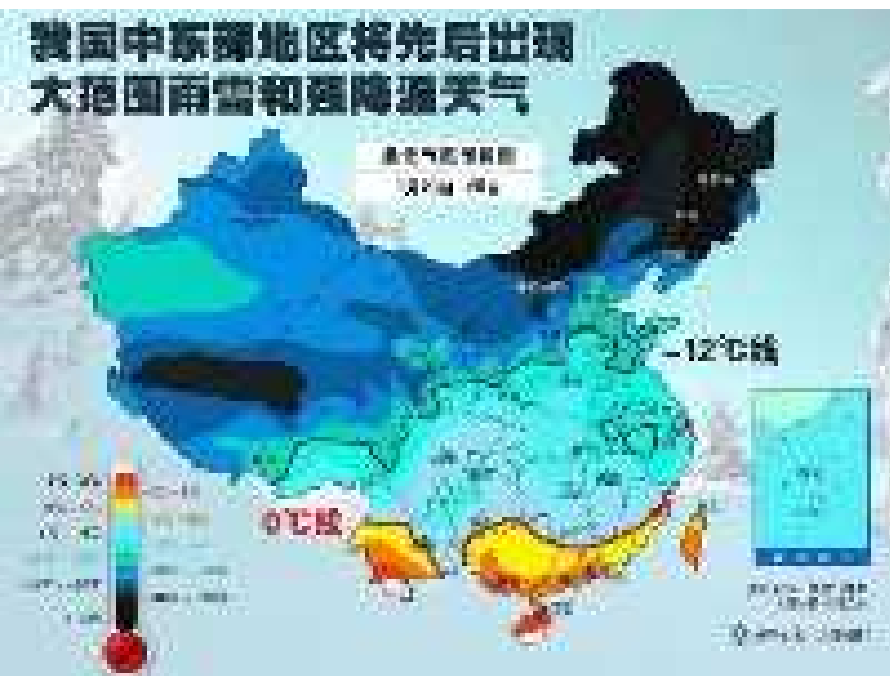
(原北方交通大学)

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Frost Related Problems : Examples

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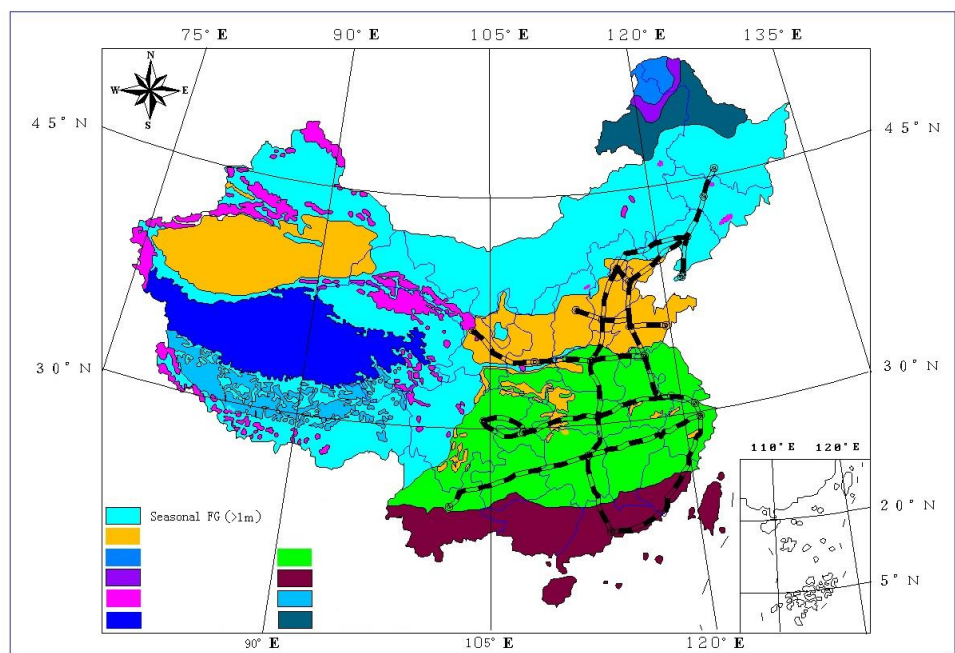
Cold Regions



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Geotechnics

Harbin-Dalian HSR



Chinese frozen soil distribution and HSR plan



Designed Speed: 350KM/h
 Slab Track- No Ballast
 Average air Temp 5.7°C,
 Extrem high 38°C, low -
 36.5°C;
 Freezing Depth 170cm
 (Changchun)

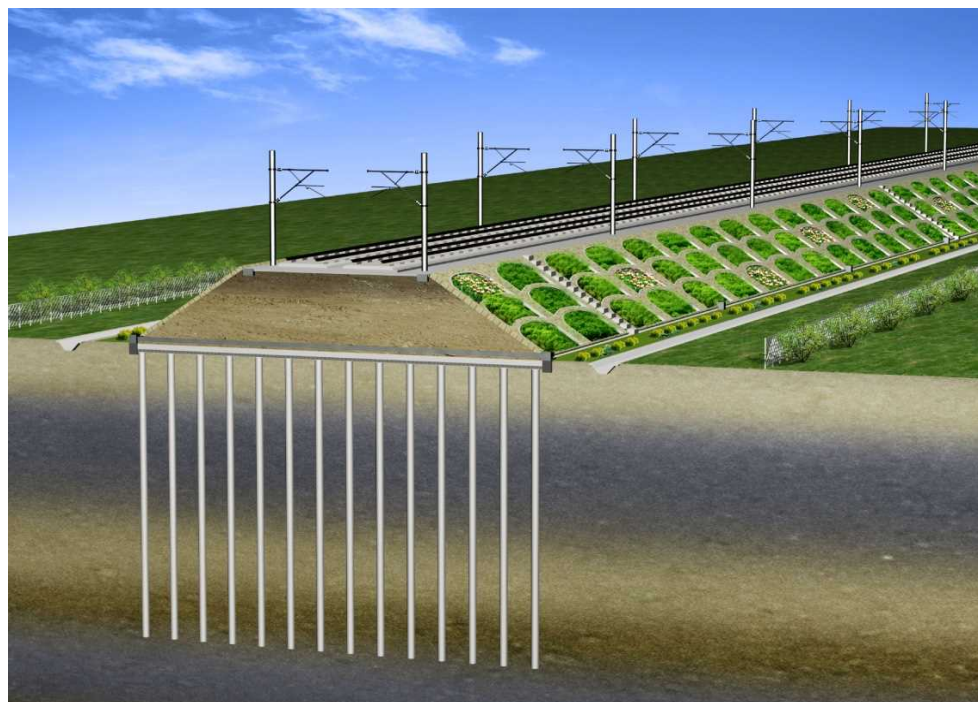
	Length/km	number	proportion
路基roadbed	231.245		25.58%
桥梁bridge	662.765	162	73.32%
隧道tunnel	9.929	8	1.1%

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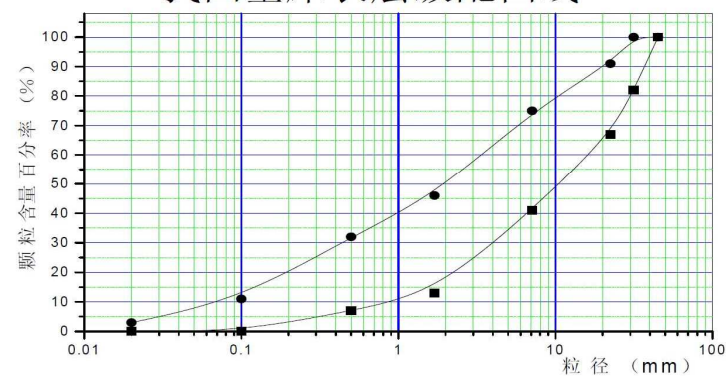


Unfrost susceptible Fills Used
More Detailed Classification of Soil
Frost Susceptibility. 5%, 15%, 30%



客运专线路基技术

我国基床表层级配曲线



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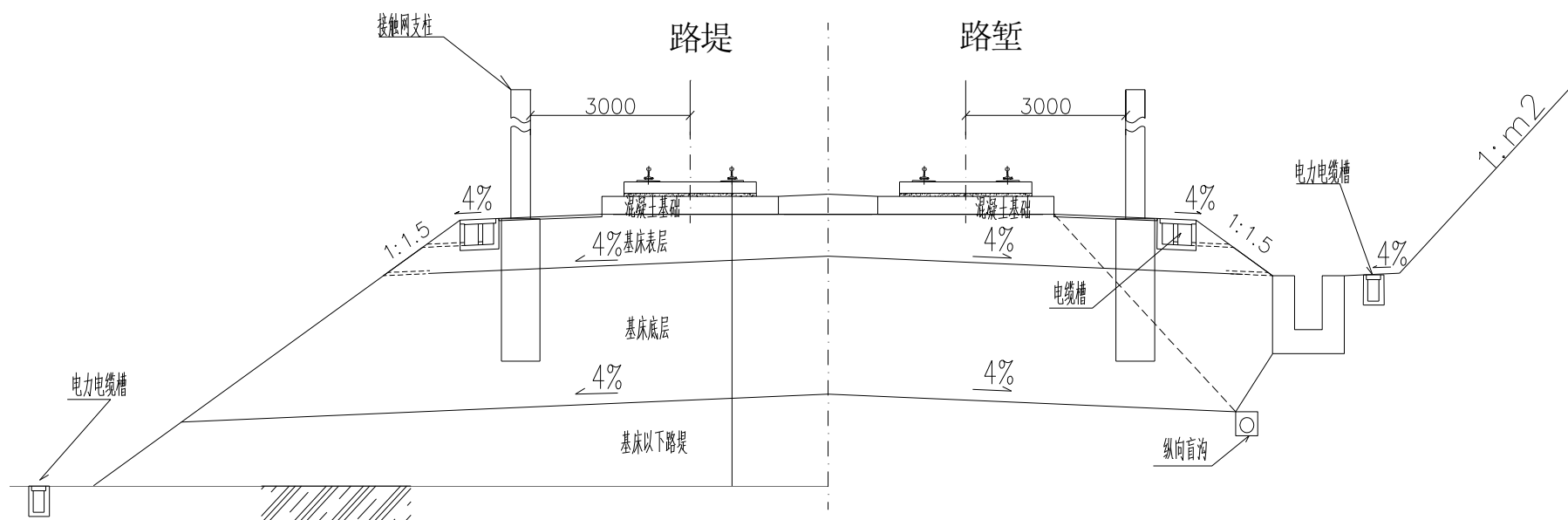
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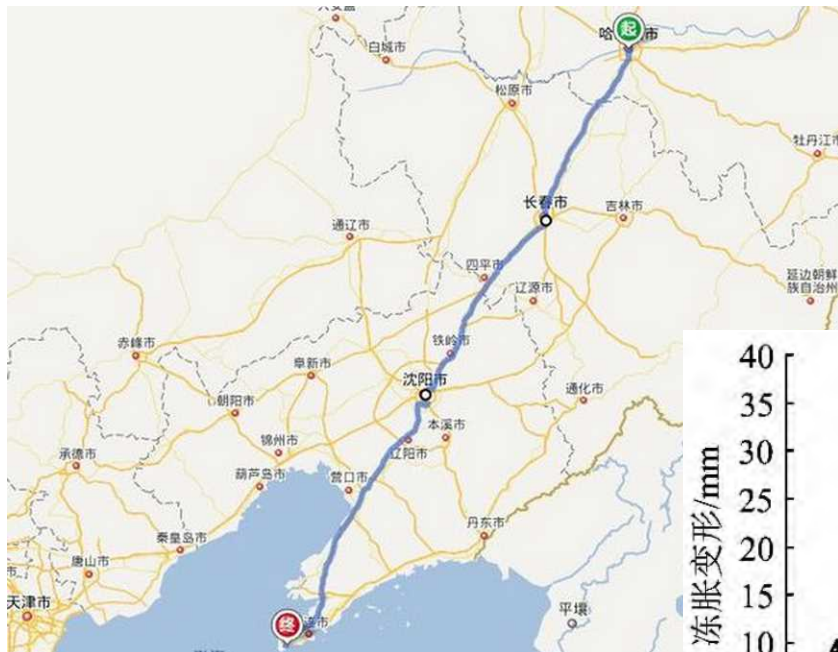
Deformation source:

Subgrade, k , n , $K30$, E_{vd} , E_{v2}

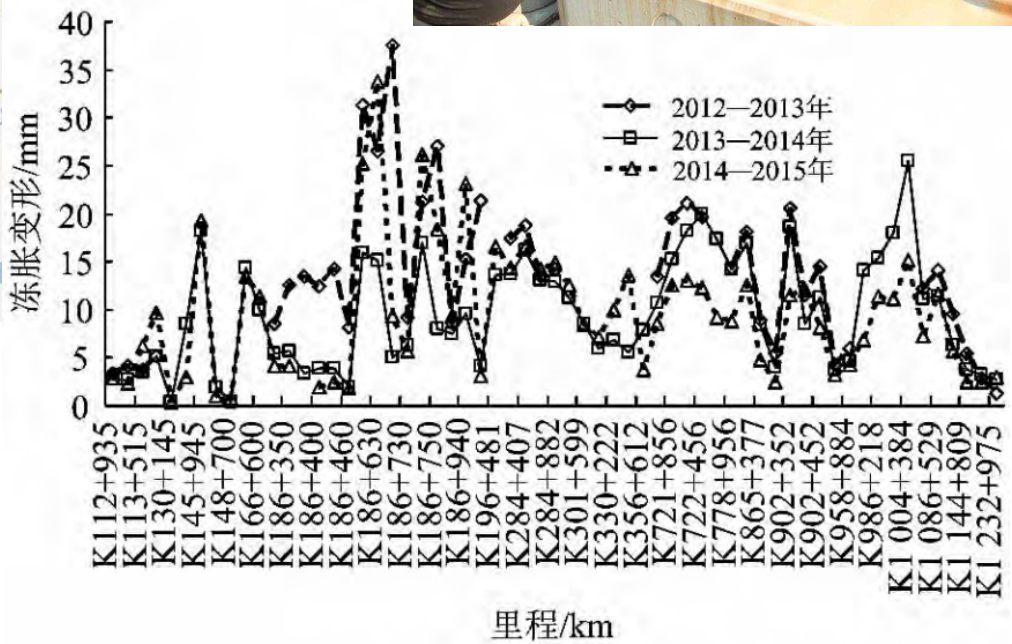
Base : Modification



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Harbin-Dalian high-speed railway



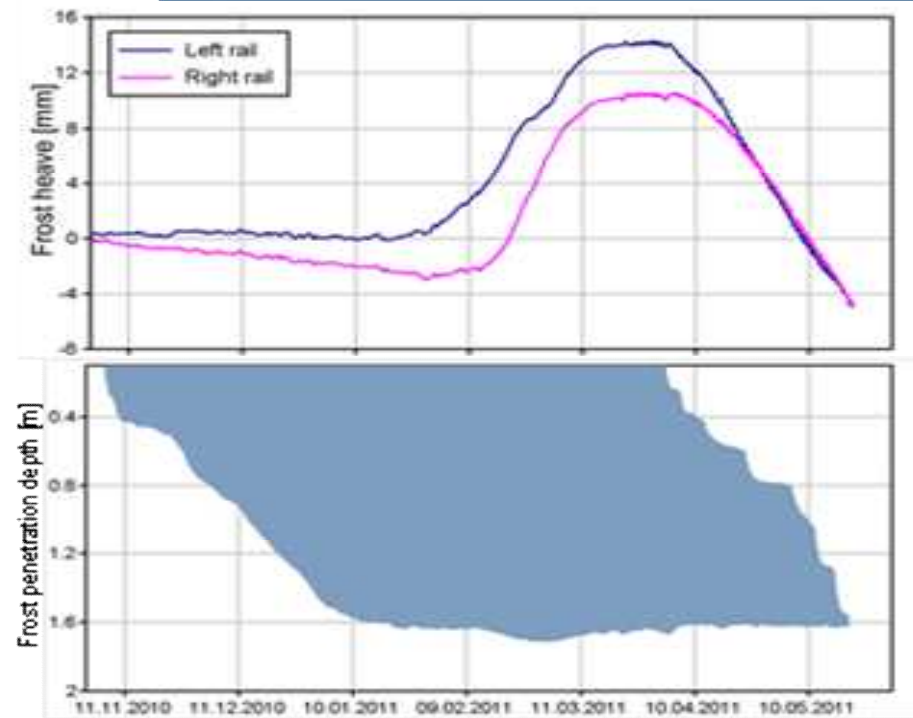
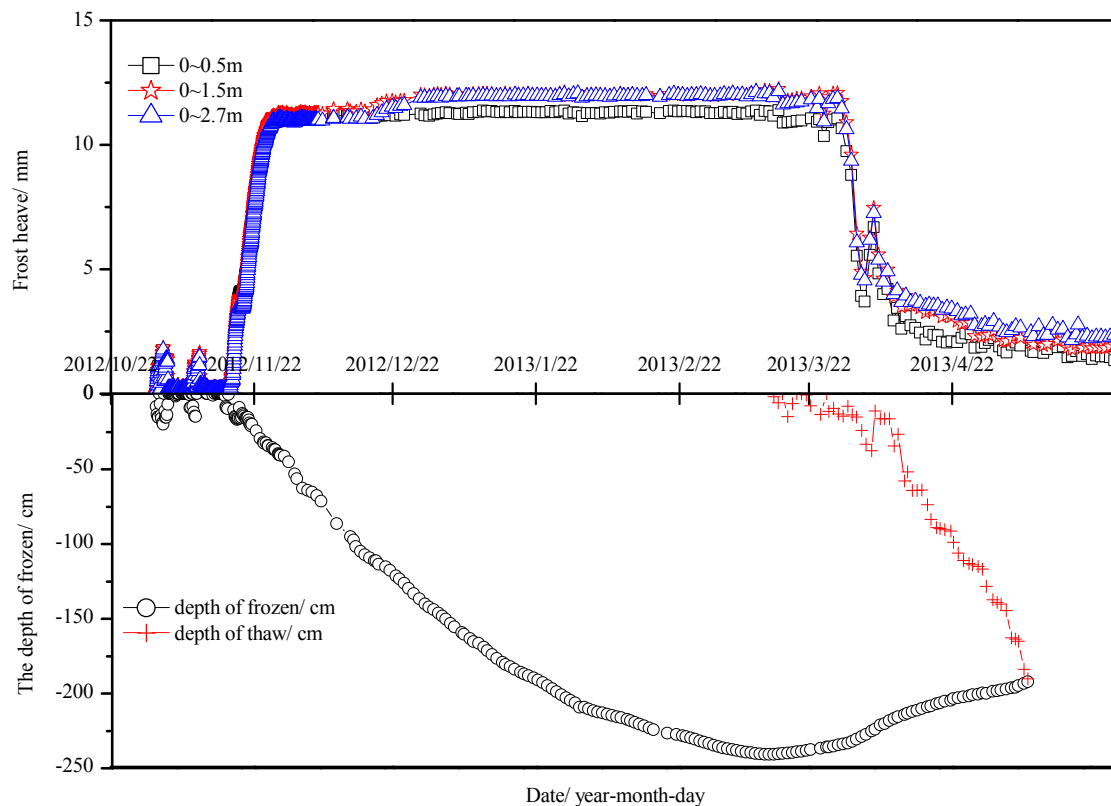
Maximum frost heave deformation

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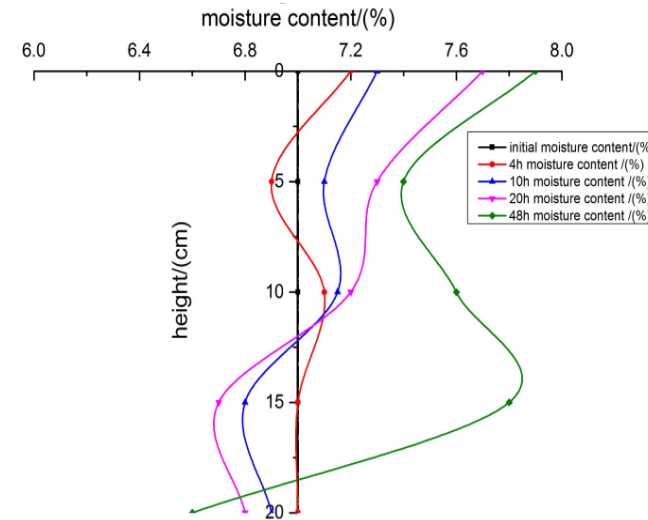


After Normikoula, 2013

After Niu 2014



试验	试验详情				冻胀量 (mm)	冻结深度 (cm)	冻胀率 (%)
	含水率 (%)	细颗粒 (%)	冷端温度 (°C)	压实度			
1	5	3	-5	0, 90	0, 65	9, 56	0, 68
2	5	5	-7	0, 93	1, 14	12, 67	0, 90
3	5	7	-10	0, 97	0, 67	18, 61	0, 36
4	7	3	-7	0, 97	1, 8	13, 15	1, 37
5	7	5	-10	0, 90	1, 83	17, 42	1, 05
6	7	7	-5	0, 93	1, 54	11, 09	1, 39
7	10	3	-10	0, 93	1, 38	17, 25	0, 8
8	10	5	-5	0, 97	1, 87	10, 17	1, 84
9	10	7	-7	0, 90	1, 47	12, 91	1, 14



水分迁移





Summary

- Lime-Cement Modified Soil for HSR
 - Fiber Reinforced Soil has lower thermal conductivity, higher strength, longer durability
 - Dynamic Shearing Box developed
-
- Thanks to National 973 project and NSCF!
 - Thanks to my team members!