

# **Uniaxial compressive strength of hydraulic, graded iron and steel slag base-course material produced at different manufacturers and its increase with curing time**

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## **0. CONTENT**

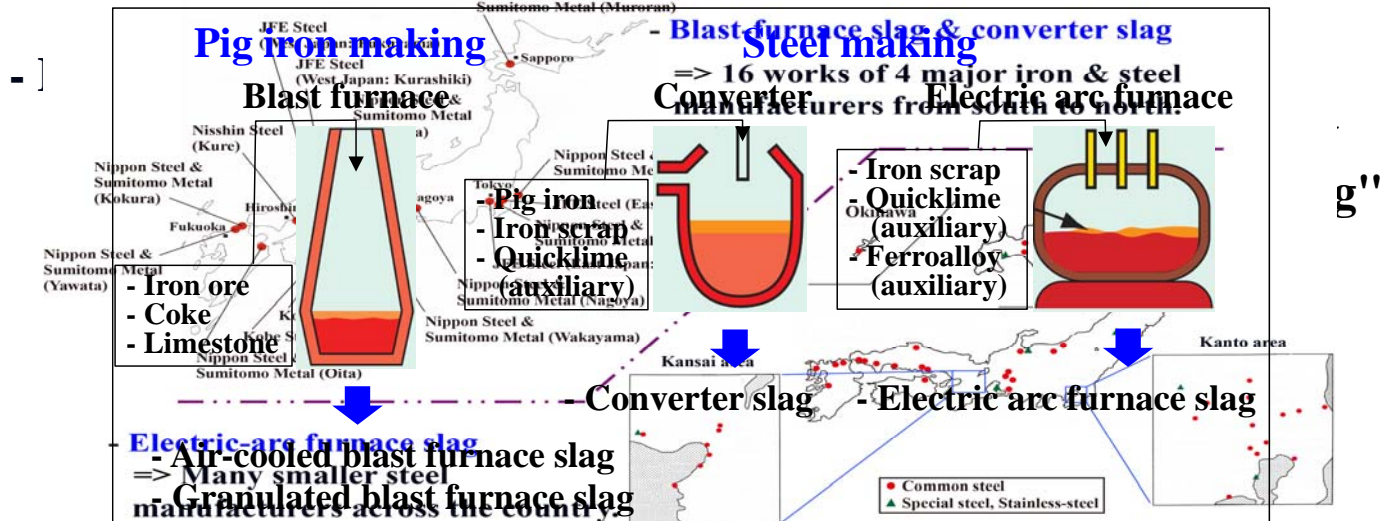
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- 1. Background and Introduction**
- 2. Purpose**
- 3. Test material and Specimen preparation**
- 4. Results and Discussions**
- 5. Conclusions**

# 1. BACKGROUND AND INTRODUCTION

## Iron and steel slag

- Produced during the process of making iron and steel, which is an industrial waste
- Classified into 4 types
  - Blast furnace slag & converter slag at 16 works of major iron and steel manufacturers
  - Electric blast furnace slag & granulated blast-furnace slag
  - Converter slag & electric arc furnace slag



# 1. BACKGROUND AND INTRODUCTION

## Iron and steel slag used in Japanese road construction by JIS (2013)

Item \ Type	Crusher-run iron and steel slag	Graded iron and steel slag	Hydraulic graded iron and steel slag	Crusher-run steel slag	Single-graded steel slag	Notes
Designations	CS-40, CS-30, CS-20	MS-25	HMS-25	CSS-30, CSS-20	SS-20, SS-5	The number indicates the max. grain size.
Usage	Subbase-course	Base-course	Base-course	Hot asphalt-stabilization	Hot asphalt mixtures	
Coloration	No	No coloration	No	-	-	Only for blast-
Uniaxial compressive strength (MPa)	-	-	1.2 or larger (13-day cured)	-	-	
Density in saturated surface-dry	-	-	-	-	2.45 or	

**A steady development of hydraulic nature in HMS !**

- assumed in the Japanese design method of asphalt pavement

- Hydraulic graded iron and steel slag (HMS) consists of blast-furnace slag and steel slag with or without additives.

- Some may not contain the granulated blast-furnace slag or any additives.

*Their mixing ratios are often manufacturers' secrets.*

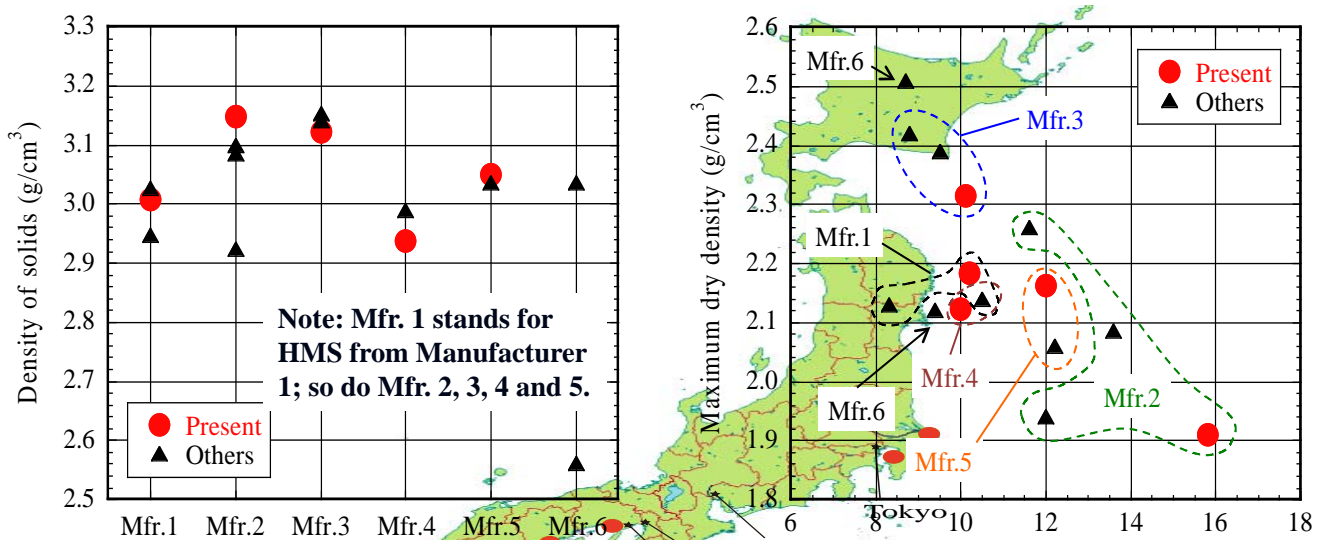
## 2. PURPOSE

- Does "HMS" base-course material from many different manufacturers exhibit similar mechanical characteristics, especially hydraulic nature?
- Had a great opportunity, in cooperation with Nippon Slag Association, of this experimental research program:
  - Mechanical characterization of HMS from **5 different manufacturers**, especially uniaxial compressive strength and resilient modulus.
- To clarify whether or not the material exhibits a similar "hydraulic nature" regardless of its manufacturers for its rational use as base-course.

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## 3. TEST MATERIAL & SPECIMEN PREPARATION

- HMS (hydraulic graded iron and steel slag) base-course material from well-known **5 manufacturers**



=> A difference in the constituents of each HMS & their mixing ratios.

- $\rho_s$  ranges from 2.9 to 3.2 g/cm<sup>3</sup>: Mfr. 2 shows the largest  $\rho_s$ .
- Greater than common soil.

- $\rho_{d,max}$  and  $w_{opt}$  scatter in a wide range.
- Mfr. 3 exhibits largest  $\rho_{d,max}$  with lower  $w_{opt}$
- Mfr. 2 shows smallest  $\rho_{d,max}$  with highest  $w_{opt}$

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### 3. TEST MATERIAL & SPECIMEN PREPARATION

#### - Cylindrical Specimens

- Size: 100 mm in diameter and 200 mm in height (excluding aggregates greater than 20 mm)

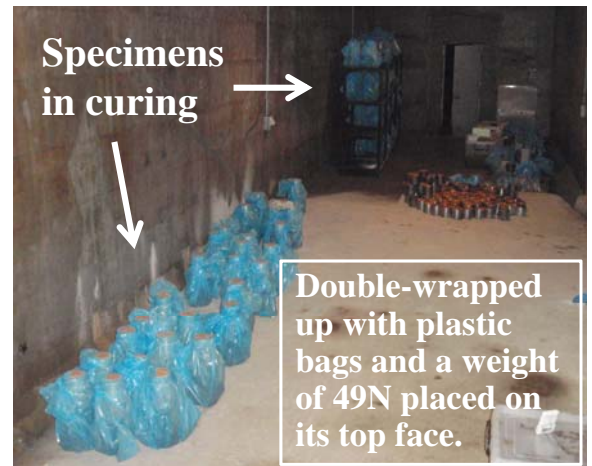
- Degree of compaction: 95%

- A prescribed amount of the material with its  $w_{opt}$  was taken and placed into a steel mould (inner diameter of 100 mm & height of 200 mm) in five stages

- Compacted using a 4.5 kg rammer in such a way that the resulting  $\rho_d$  became 95% of the  $\rho_{d,max}$ .

- Curing of specimens: Stored them at an underground room with a temp. of about 20° C and a humid. of about 60% from 0 to 730 days.

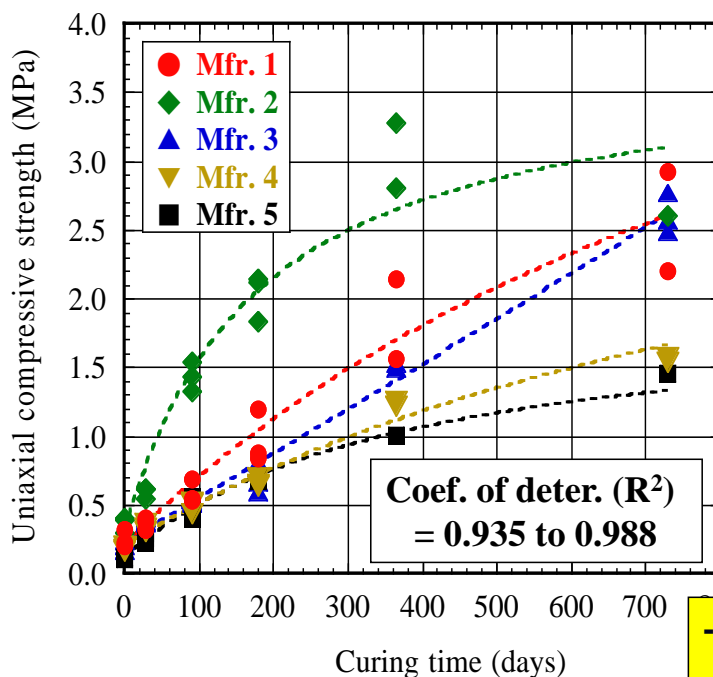
- No. of specimens: 3 pieces/curing time/manufacturer



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### 4. TEST RESULTS AND DISCUSSIONS

#### Uniaxial compressive strength ( $q_u$ ) at each curing time



-  $q_u$  has a wide distribution at each curing time.

-  $q_u$  seems to increase with curing time, regardless of manufacturer.

e.g., Ratio of 730-day cured average  $q_u$  to 28-day cured one are:

7.0 for Mfr. 1,

5.1 for Mfr. 2,

6.8 for Mfr. 3,

4.6 for Mfr. 4,

5.6 for Mfr. 5.

-  $q_u$  with a shorter curing time underestimates its long-term  $q_u$  regardless of manufacturer.

- Increasing tendency of  $q_u$  with time differs among manufacturers.

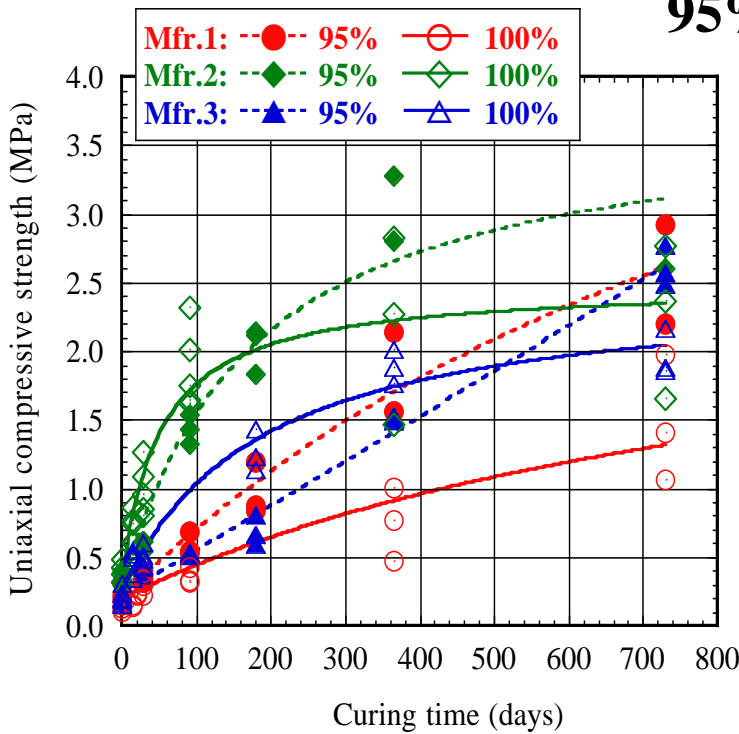
e.g., Mfr. 3 seems to continue to increase further; Mfr. 5 is likely to settle down soon.

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# 4. TEST RESULTS AND DISCUSSIONS

## Uniaxial compressive strength ( $q_u$ )

### 95% vs. 100%-compacted



(With regression curves with the coefficient of determination,  $R^2$  ranging from 0.830 to 0.988)

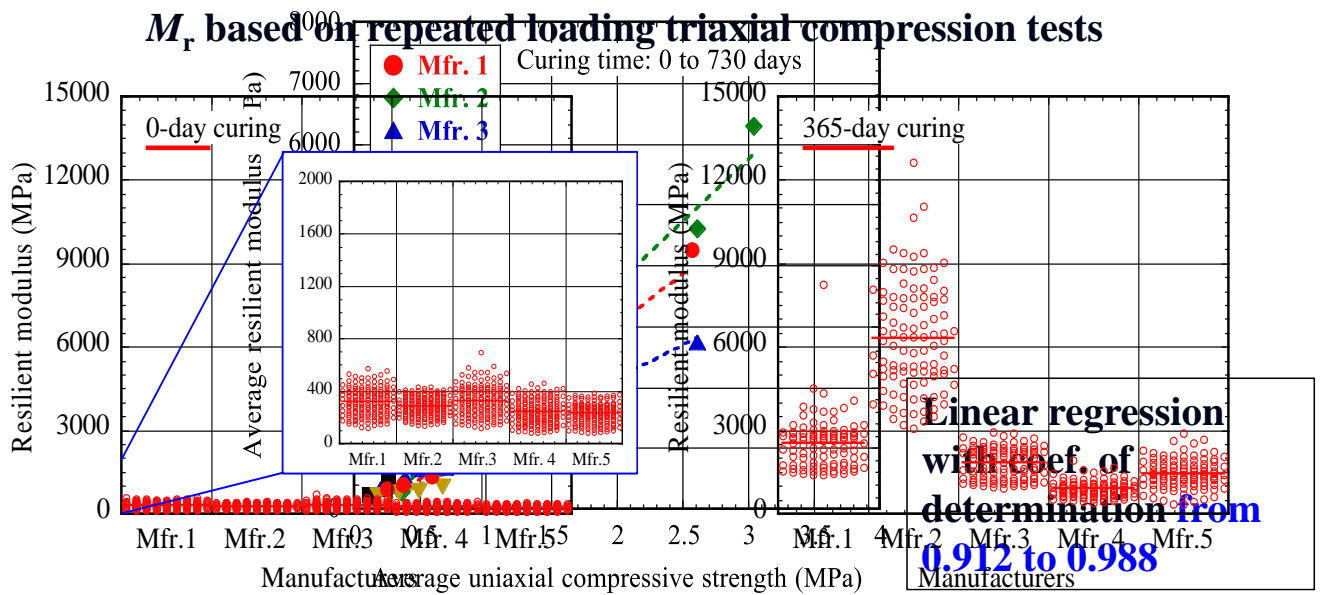
- 100%-compacted  $q_u$  also shows scattering at each curing time.
- 95%-compacted  $q_u$  is not necessarily smaller than 100%-compacted one.
- => **The variable development of hydraulic nature overwhelms the expected influence of compaction efforts on the strength.**

- Increasing tendency of  $q_u$  with time differs even in the same manufacturer's HMS.
- => **Development of hydraulic nature may be different, depending on when it comes, even if the HMS comes from the same manufacturer.**

# 4. TEST RESULTS AND DISCUSSIONS

## Uniaxial compressive strength ( $q_u$ ) vs. Resilient modulus

In Average for each curing time for each manufacturer ( $M_r$ )



- A strong correlation between average  $q_u$  and average  $M_r$  exists.
- => Can estimate average  $M_r$  from average  $q_u$  for each manufacturer.
- For a given average  $q_u$ ,  $M_r$  differs among manufacturers.

## 5. CONCLUSIONS

From this study, the followings can be pointed out as conclusions.

- There are large variations in the compaction properties ( $w_{opt}$  and  $\rho_{max}$ ) among the five types of HMS.
- $q_u$  for the five types of HMS was distributed widely at each curing time.
- A tendency of  $q_u$  to increase with curing time also differed among the five types of HMS.
- This variable development of hydraulic nature blurred the effect of compaction efforts on the strength.
- $M_r$  also differed among the five types of HMS but there existed a strong linear correlation between the mean  $q_u$  and the mean  $M_r$  for each of them.

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## 5. CONCLUSIONS

A possible consequence from this study may be the following:

- When two base-course are constructed using HMS, they could exhibit a different durability or service life, even if the thickness and compaction degree of the base-course are the same between them.

> It would be difficult to determine rationally the thickness of HMS base-course to meet a targeted service life.

> One would have no choice but to adopt a conservative thickness, referring to the existing pavement structures with HMS base-course.

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