

FRP Anchorage Systems for the Strengthening of Infill Masonry **Structures**

120

2.5 5.0 7.5 10.0 12.5 15.0 17.5

kPa)



Lab. of Engineering Systems for Maintenance system



_C1

-S1_G_0

-S2 P O

-S3_G_SR

-S4 P SR

-S5 G FA

-S6_P_FA

-S7-G-EB

-S8-G-SK

Comparison of Results

Deflection at Mid point (cm)

Figure 12: Comparison of Load - Deflection behavior

FAILURE MODES



Figure 15: Flexural Failure of Control Specimen (Left) Figure 16: FRP Rupture Failure of S3-G-SR Specimen (Center) Figure 17: Displaced Shape of S4-P-SR Specimen (Right) -No Failure



Specimen (Left)

Figure 18: Debonding at top interface up to fiber anchors of S5-G-FA Figure 19: Debonding at top interface up to fiber anchors of S6-P-FA Specimen (Right)



Figure 20: Top fiber anchor pull out (left) and Bottom fiber anchor rupture (right) of S6-P-FA Specimen

SUMMARY OF TEST RESULTS

Specimen ID	FRP Type	Anchorage Type	Elastic limit (kPa)	Max Load (kPa)	Max Displ (cm)	Failure Mode
C1	-	-	3.5	15.5	3.6	FB
S1-G-0	GFRP	Overlap	28.3	36.1	2.2	DB
S2-P-0	PET		19.3	29.0	3.8	DB
S3-G-SR	GFRP	Shear	28.3	112.3	6.0	FR
S4-P-SR	PET	Restraint	33.1	124.6	16.2	NF
S5-G-FB	GFRP	Fiber Bolt	11.7	60.7	5.4	AR&AP
S6-P-FB	PET		36.5	50.4	12.2	AR&AP
S7-G-EB	GFRP	Embedded Bar	47.6	68.3	5.4	AP
SB-G-SK	GFRP	CFRP Shear	39.3	56.1	4.0	AP
S9-P-SK	PET	Кву	16.5	38.3	3.3	AP
S10-G-NSM	Grancrete	Near Surface	17.9	25.0	2.5	AP
S11-E-NSM	Epoxy	Mounted	16.5	36.6	3.1	AP

ABSTRACT

A previous study conducted at North Carolina State University on the strengthening of infill masonry walls with FRP clearly indicated that the type of anchorage system has a strong influence on the overall performance of the FRP strengthening system. This study will explore the performance of several innovative FRP anchorage systems for strengthening of masonry infill walls. A new type of FRP with high fracturing strain, PET, is proposed for the experimental program in which the FRP is anchored to the supporting members using four different types of anchorage: overlap, mechanical anchorage, wrapping around an embedded FRP bar, and FRP anchor bolts. The primary objective of this study is to explore the performance of innovative FRP anchorage systems for strengthening of infill masonry walls. Previous studies have shown that FRP strengthening of masonry can lead to a substantial increase in load carrying capacity when proper anchorage of the FRP to supporting elements is provided. In cases where inadequate anchorage is used, the mode of failure can shift from a ductile flexural failure to a brittle and premature shear sliding failure. This study intends to explore different anchorage systems to determine which are effective in preventing or delaying the shear sliding mode of failure and to quantify the effectiveness in terms of increased load carrying capacity and ductility.

FRP ANCHORAGE TYPES

sheets



"shear restraint" (SR), consists of steel plates bolted to the RC caps. The plates were clamped over the FRP sheet to provide mechanical anchorage and extend two inches beyond the masonry/RC cap interface to resist sliding shear along this interface.





"fiber bolt" (FB), consists of a bundle of fibers embedded perpendicular to the face of the RC cap and flaved outward at the surface to resist pullout of the FRP

Figure 2: FRP Reinforcement with Fiber Bolts anchor



"embedded bar" (EB), consists of wrapping the FRP sheets around an FRP bar embedded near in the surface of the RC cap and running parallel to the masonry/RC cap interface

Figure 3: FRP Reinforcement with Embedded Bar anchor



"shear keys" (SK), consists of short near surface mounted CFRP strips embedded perpendicular to the masonry/RC cap. These are intended to resist sliding shear along the interface. The FRP sheet will then be placed with the "overlap" configuration above these shear keys.

Figure 4: FRP Reinforcement with CFRP Shear Key anchor



"Near Surface Mounted " (NSM), consists of short surface mounted CFRP strand sheet embedded perpendicular to the masonry/RC cap. These are intended to resist sliding shear along the interface and resist flexural failure.

Figure 5: Reinforcement with Near Surface Mounted Bar anchor



Test Specimen and set up



Figure 8: Typical cyclic loading sequence from Airbag



Figure 11: Location of Load Cells (Right)



Figure 14: Comparison of Measured Strain profile in FRP Sheet

5000

Strain (Micro strain)

←S1_G_0 ←S2_P_0 ←S3_G_SR ←S4_P_SR ←S5_G_FA ←S6_P_FA ←S7-G-EB ←S8-G-SK

10000

15000

20000

25000

NC STATE UNIVERSIT

0

-10000

-5000

Experiment of this study was conducted at