



Estimation Method on Deterioration of Marine Concrete Structures Due to Chloride Attack

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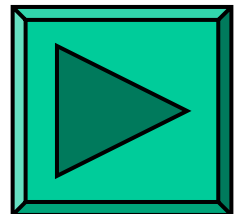
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2014.4.25

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- **Outline of deterioration process of marine concrete structure**
- **Examination of durability for marine concrete structure in durability design**
- **Simulation model of corrosion of reinforcement in concrete**
- **Evaluation of structural performance of concrete structure deteriorated due to corrosion of reinforcement**

Outline of Deterioration Process





















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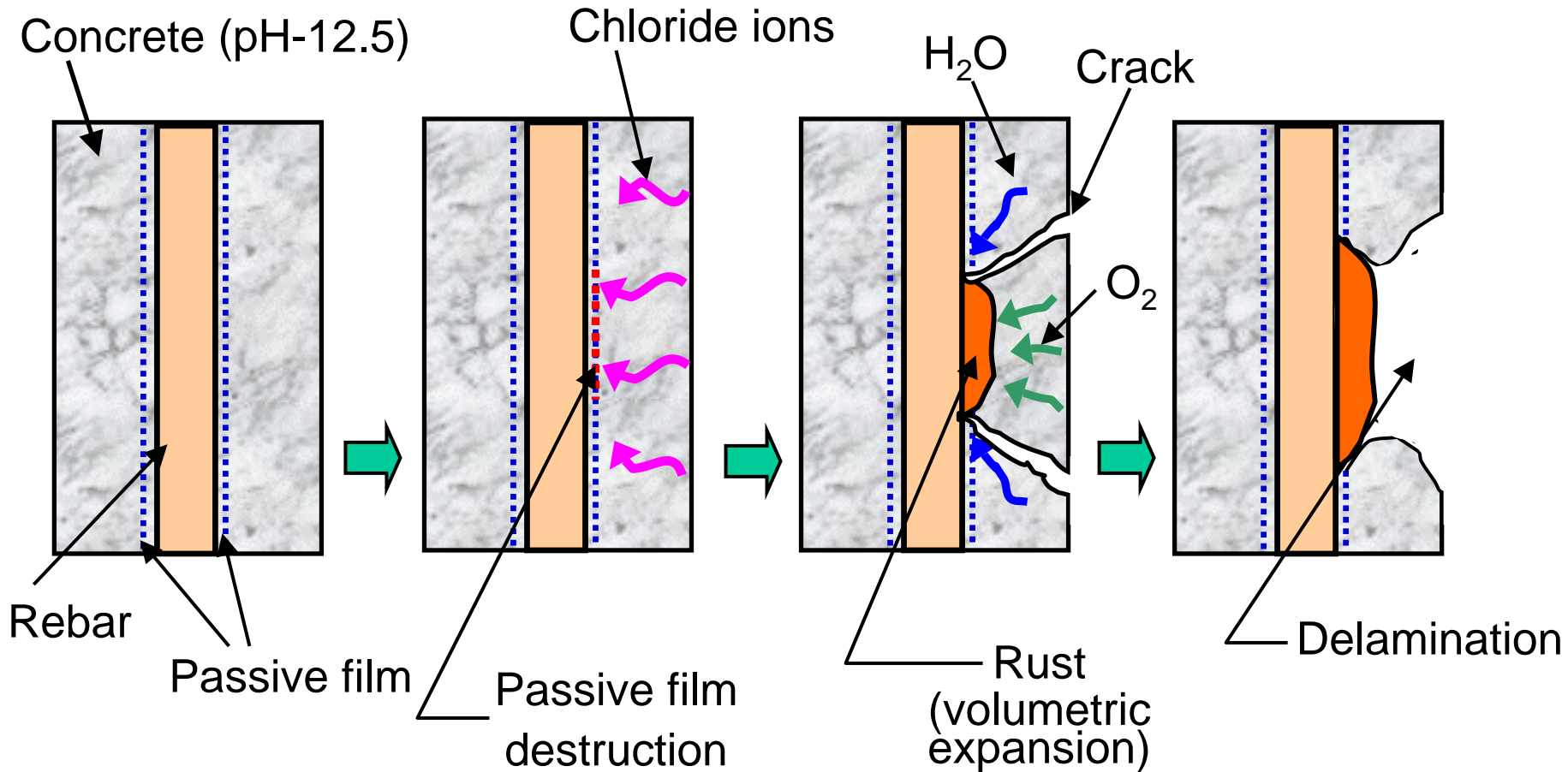
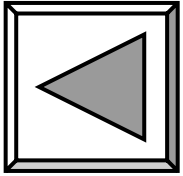






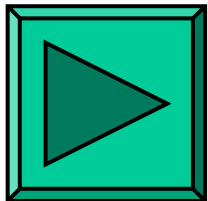
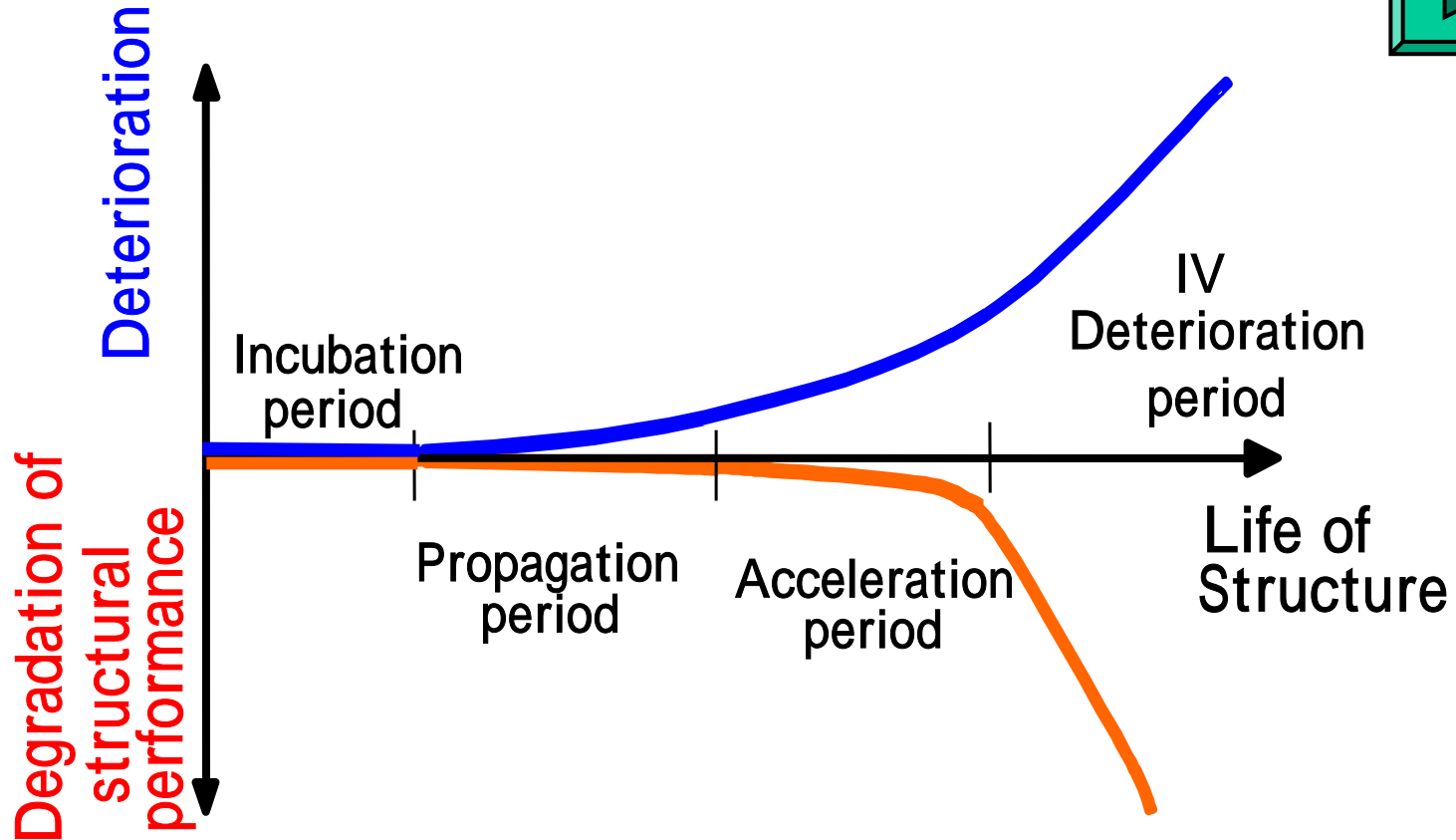
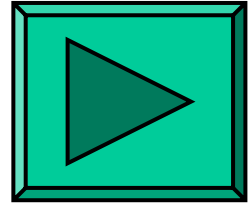


Deterioration process on marine concrete structures



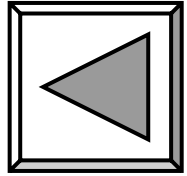
Chloride-induced deterioration process

Deterioration process on marine concrete structures



Chloride-induced deterioration process

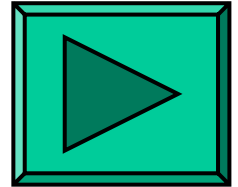
Deterioration process on marine concrete structures



Definition of stages in the deterioration process and primary factors characterizing each stage

Stage No.	Definition of period	Primary factors characterizing the deterioration
I	Period of chloride penetration until the chloride concentration around rebars up to the threshold value	<ul style="list-style-type: none">• Chloride diffusion rate• Cover thickness
II	Period of the corrosion progress on rebar until concrete cracks due to the corrosion appear	<ul style="list-style-type: none">• Rebar corrosion rate• Resistivity against cracking of concrete
III	Period of the corrosion progress on rebar after appearance of concrete cracks	<ul style="list-style-type: none">• Rebar corrosion rate
IV	Period of degradation of structural performance induced by rebar corrosion and concrete cracks	<ul style="list-style-type: none">• Width of cracks due to rebar corrosion

Deterioration process on marine concrete structures



Marine environment

Chloride penetration into concrete

Passive film on reinforcement is lost

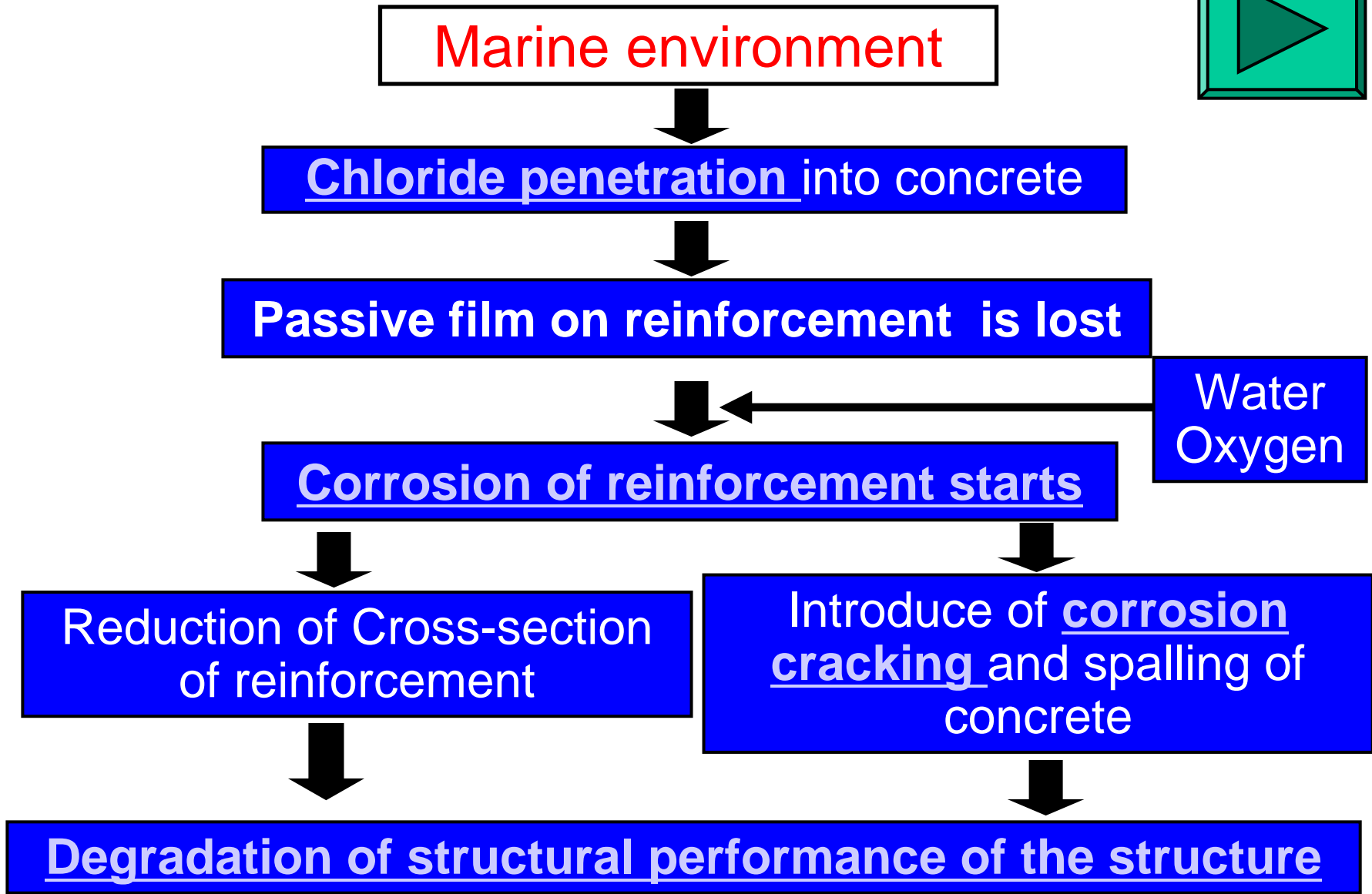
Water
Oxygen

Corrosion of reinforcement starts

Reduction of Cross-section
of reinforcement

Introduce of corrosion
cracking and spalling of
concrete

Degradation of structural performance of the structure



Deterioration process on marine concrete structures

Penetration of chloride into concrete

In sea water, Splash zone, Marine atmospheric Zone

Penetration of Cl⁻ via pores to the interior of concrete

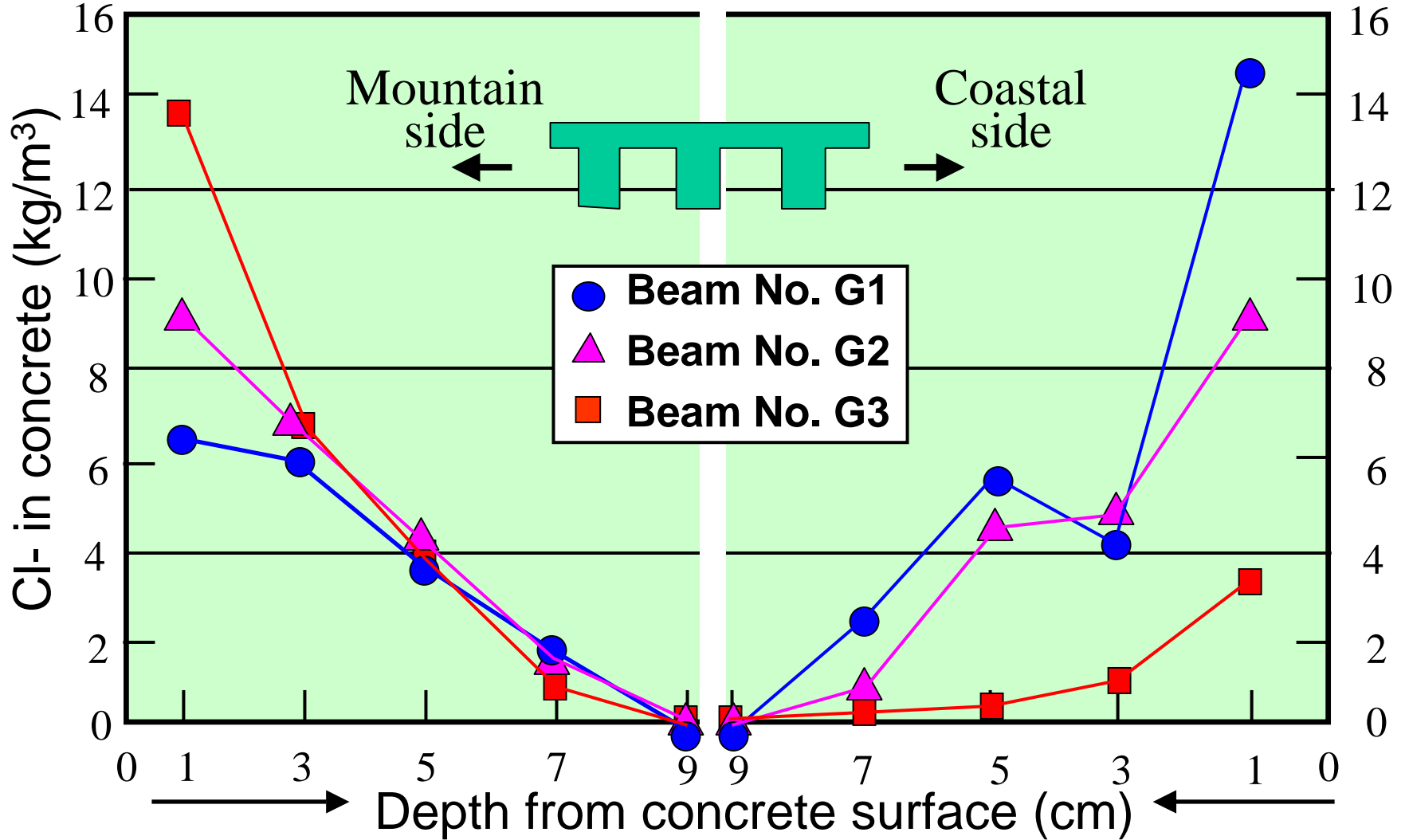
Cement hydrate binds some of Cl⁻ chemically

Fredel's salt (C₃A·CaCl₂·nH₂O)

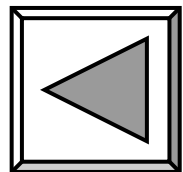
Only the free chloride diffuses into concrete

When critical concentration of free Cl⁻ accumulates on reinforcement surface, corrosion starts on it

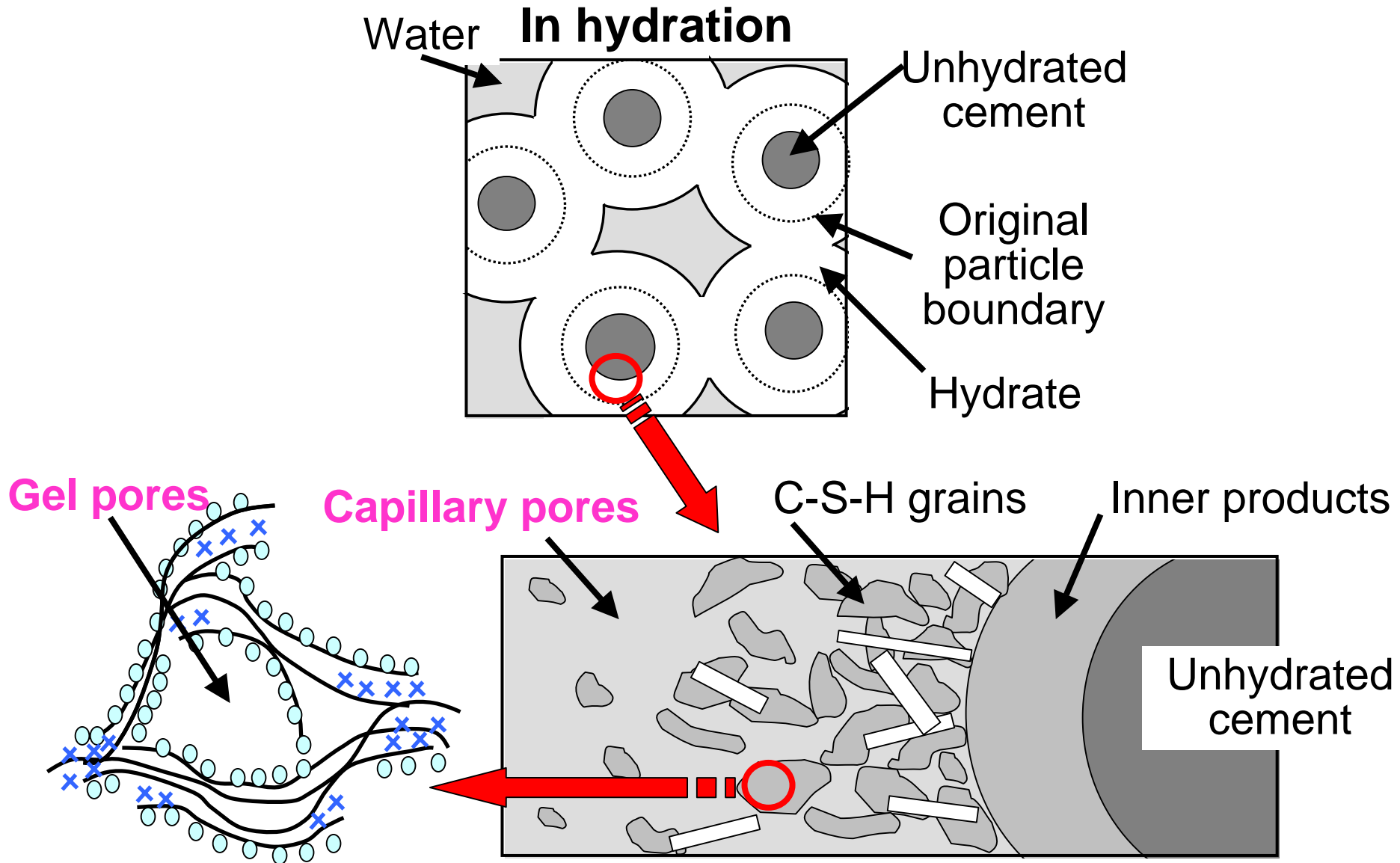
Example of chloride penetration profile into concrete



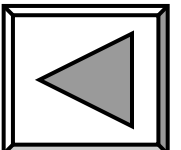
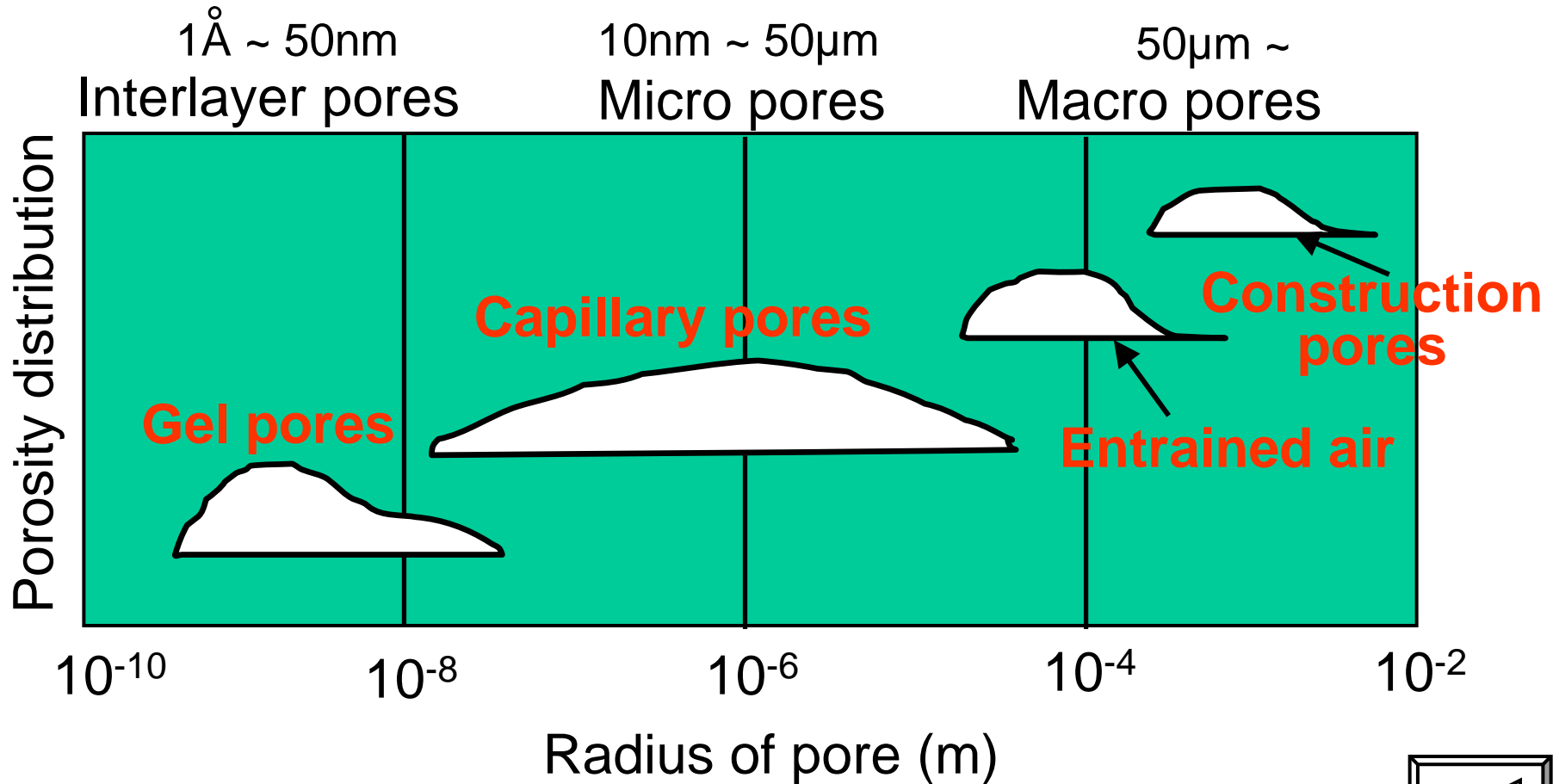
Chloride distribution profiles in concrete bridge beams in coastal zone after 17 years of service



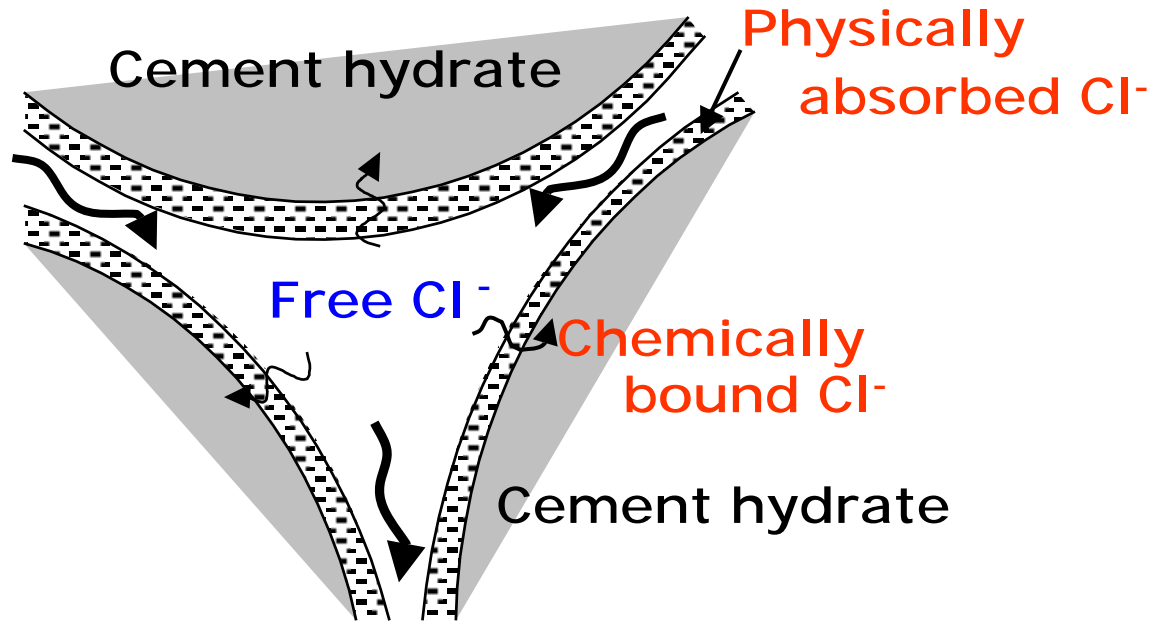
Microstructure of Cement paste



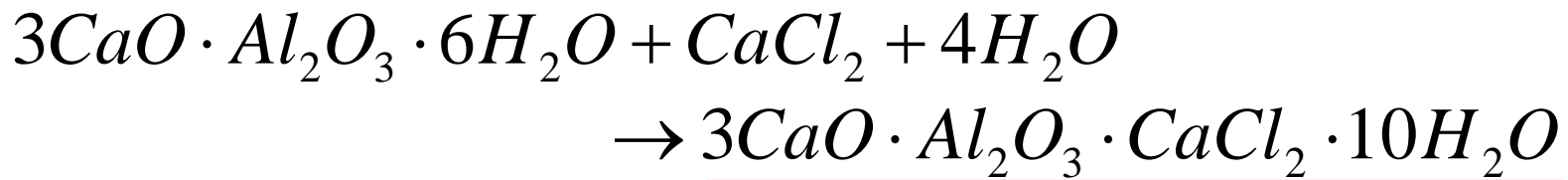
Schematic representation of porosity classification in concrete



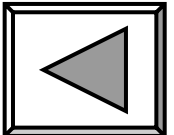
Binding of chloride ions into cement hydrate



Chemical binding equation



Fredell's salt

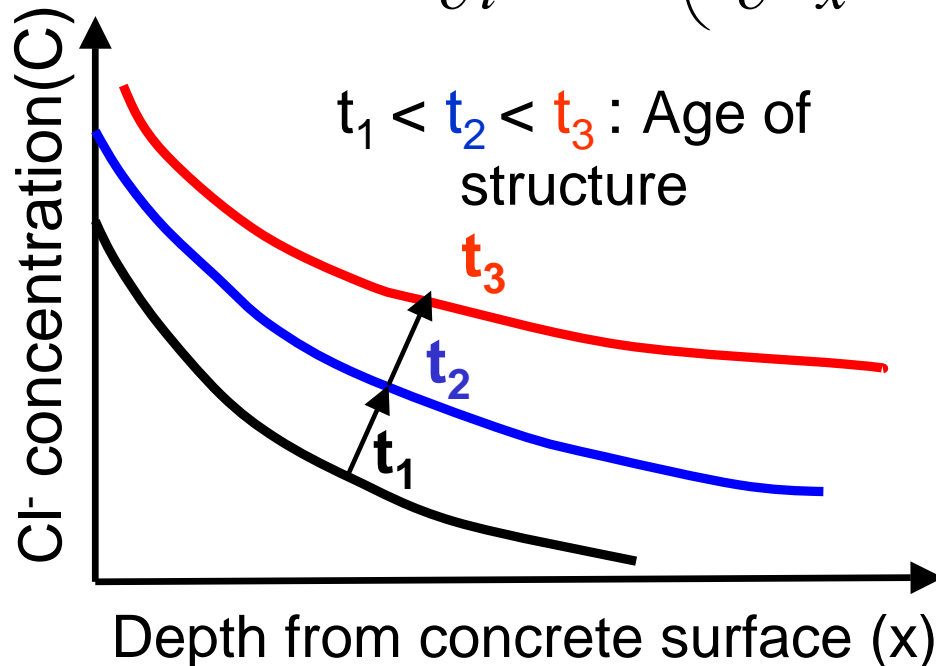


Deterioration process on marine concrete structures

Penetration of chloride into concrete

Diffusion equation (Modified Fick's second law)

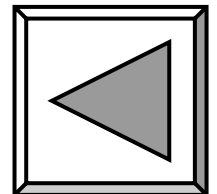
$$\frac{\partial C}{\partial t} = D \left(\frac{\partial^2 C}{\partial x^2} + \frac{\partial^2 C}{\partial y^2} + \frac{\partial^2 C}{\partial z^2} \right) - K \cdot C$$



C: Concentration of Cl⁻ at depth (x,y,z) after t

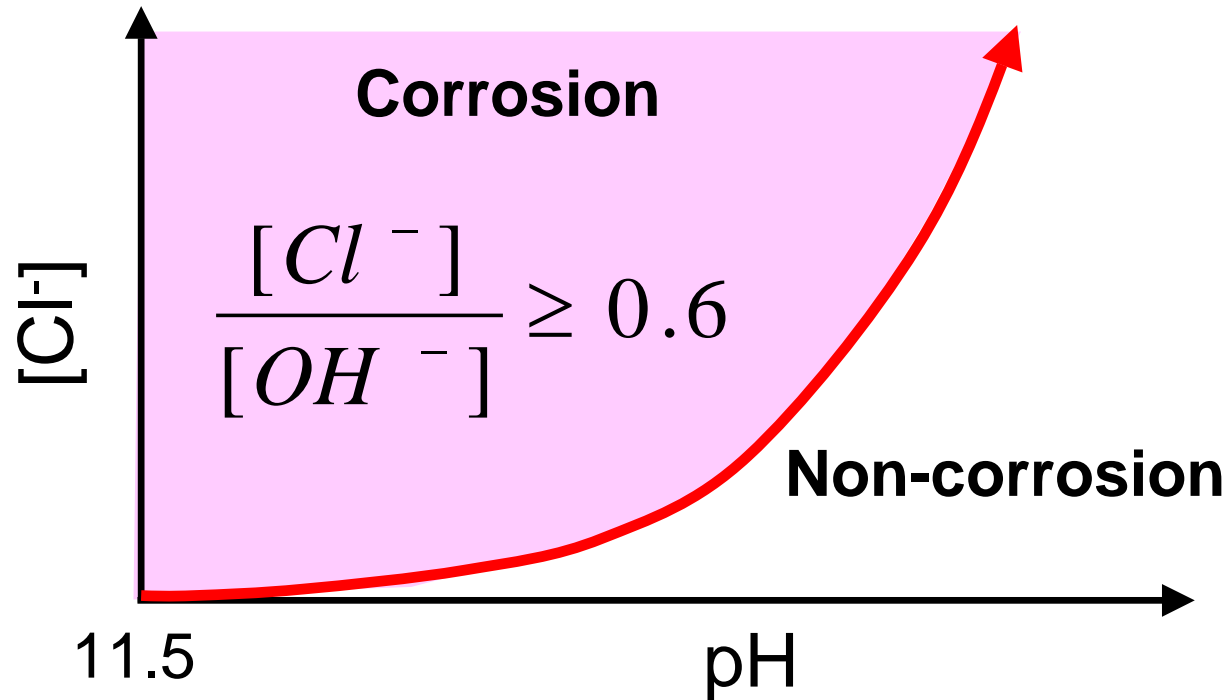
D: Diffusion coefficient

K: Cl⁻ binding coefficient



Deterioration process on marine concrete structures

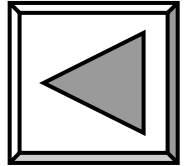
Critical chloride content



Effect of Chloride concentration and pH
on initiation of corrosion

Deterioration process on marine concrete structures

Critical chloride content



In case of ordinary reinforcing bar in concrete

0.05% Cl⁻ related to the weight of Concrete

||

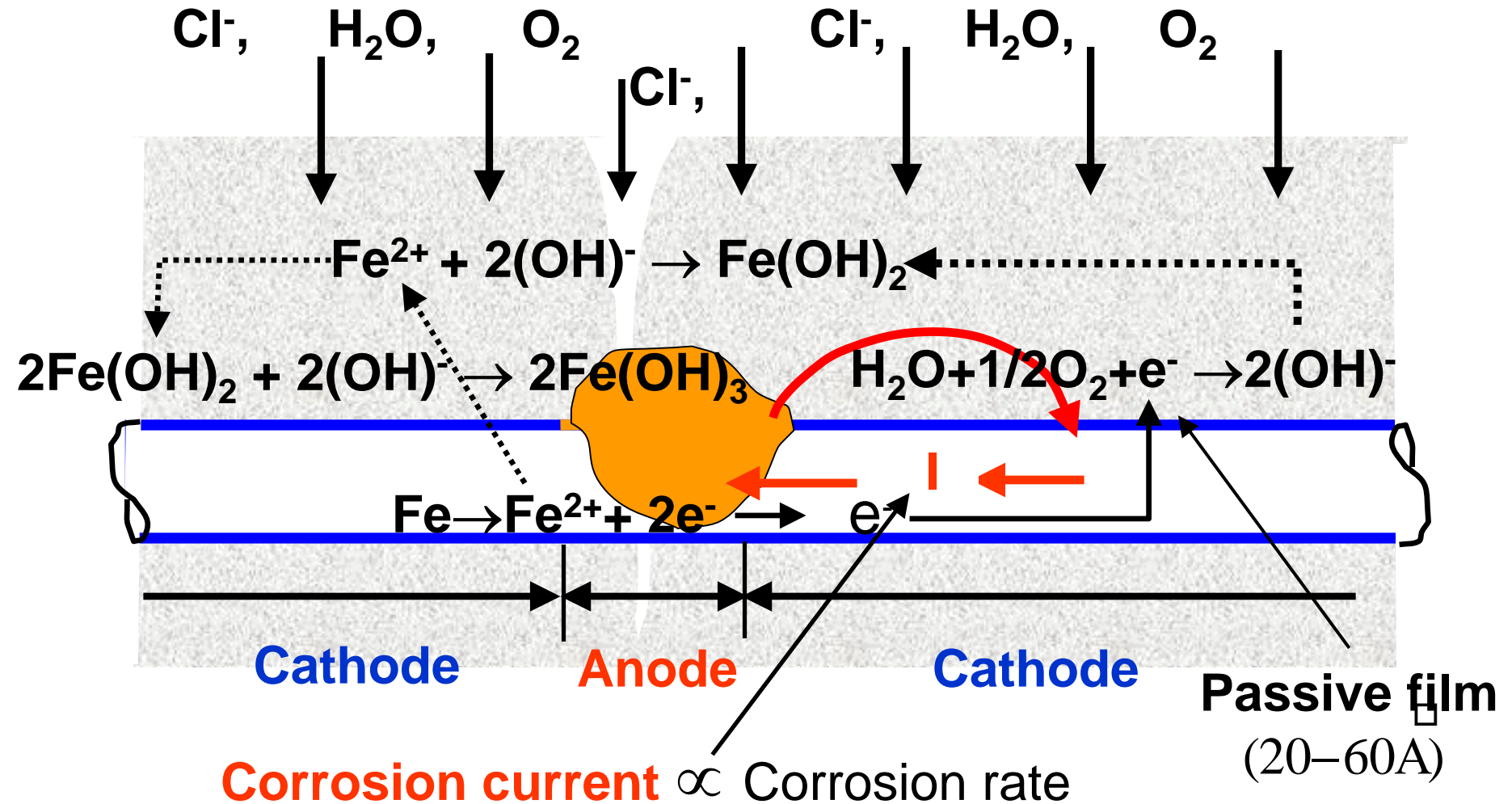
0.4% Cl⁻ related to the cement weight

or

1.2 kg/m³ of Cl⁻ per unit concrete volume

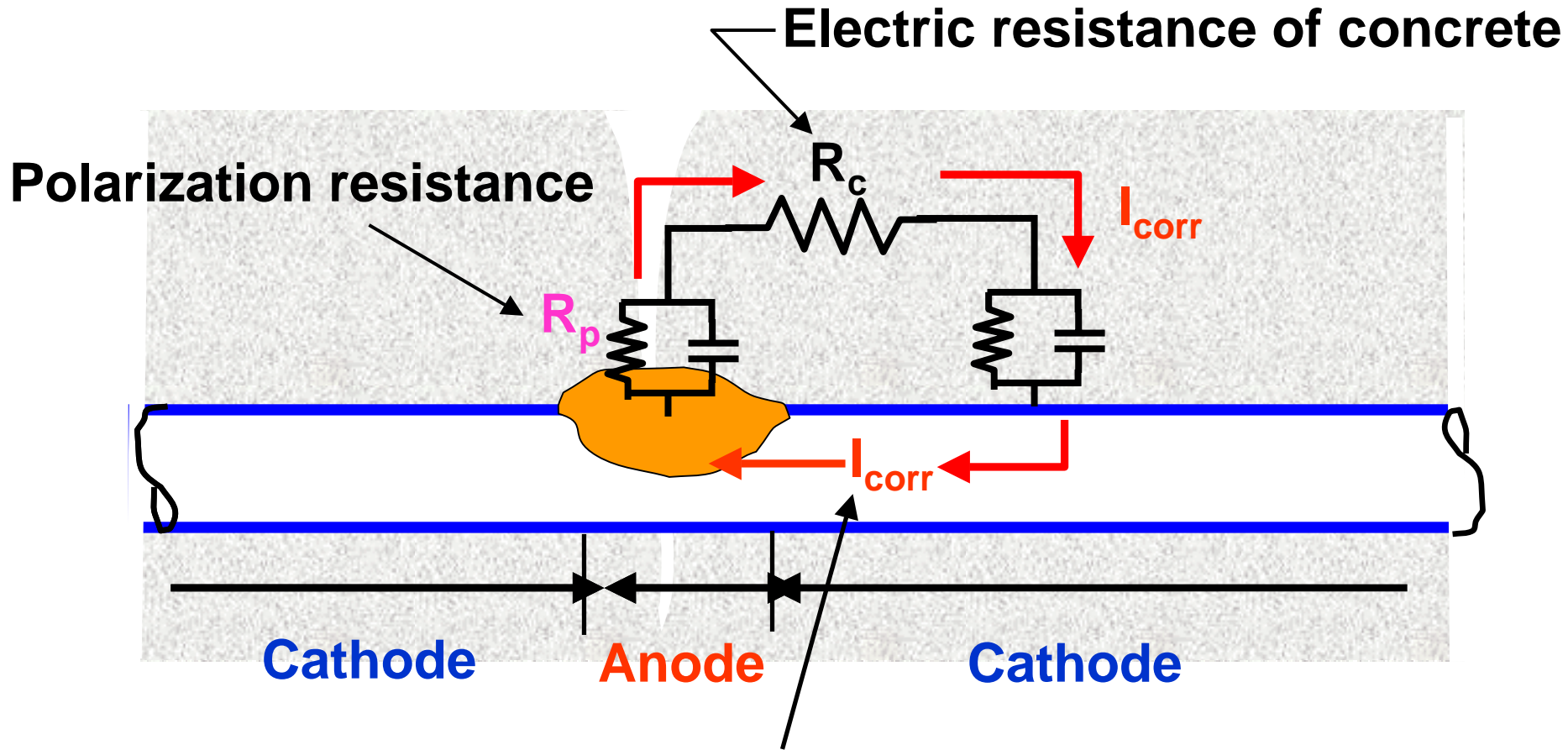
Deterioration process on marine concrete structures

Corrosion process on reinforcement



Deterioration process on marine concrete structures

Corrosion process on reinforcement



Corrosion current \propto Corrosion rate \propto $1/R_p$

Deterioration process on marine concrete structures

Corrosion process on reinforcement

Corrosion weight loss of reinforcement (W)

Corrosion current: I_{corr}

$$I_{corr} = k \cdot \frac{1}{R_p}$$

R_p : Polarization resistance

k : Constant (25~50mV)

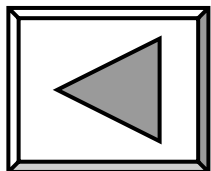
Corrosion Weight loss: W

$$W = \frac{[Fe]}{n \cdot F} \cdot I_{corr} \cdot t$$

$[Fe]$: Atomic weight (55.84 g)

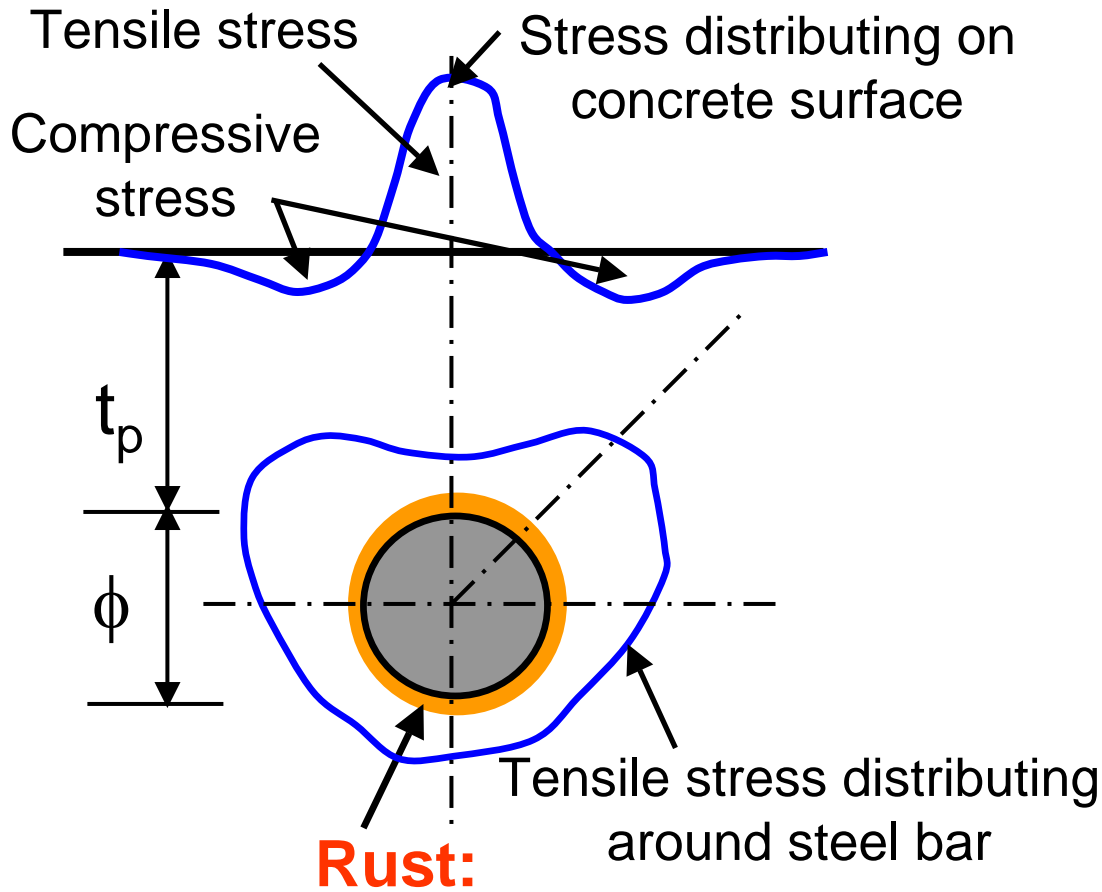
n : Atomic value (Fe : $n=2$)

F : Faraday's Constant (96,500 A/sec)

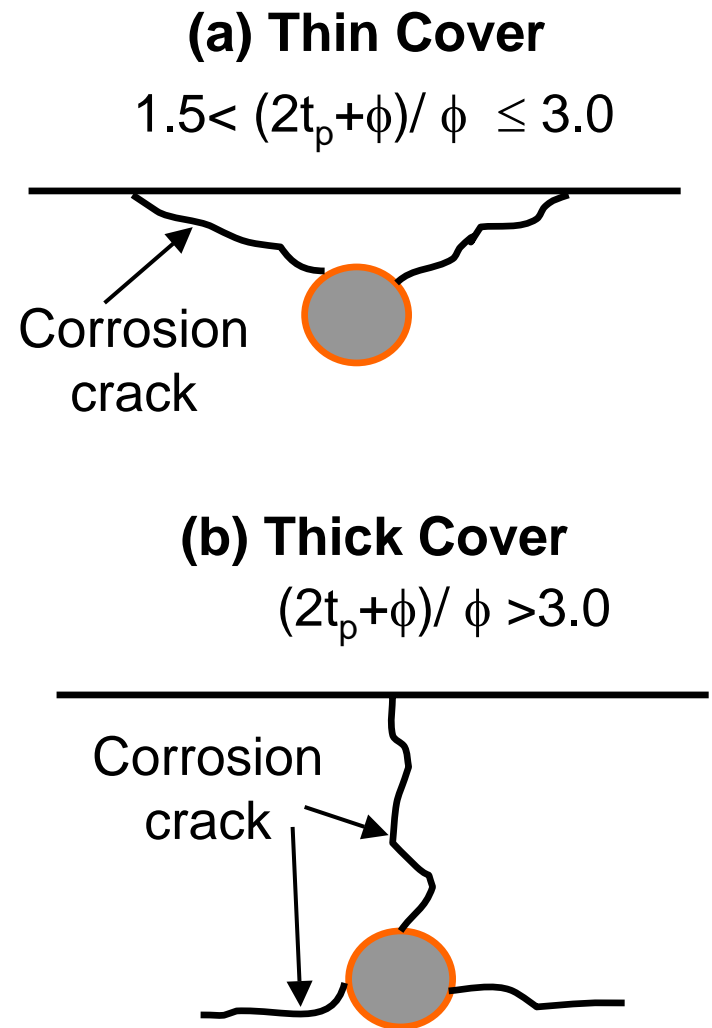


Deterioration process on marine concrete structures

Corrosion crack on concrete

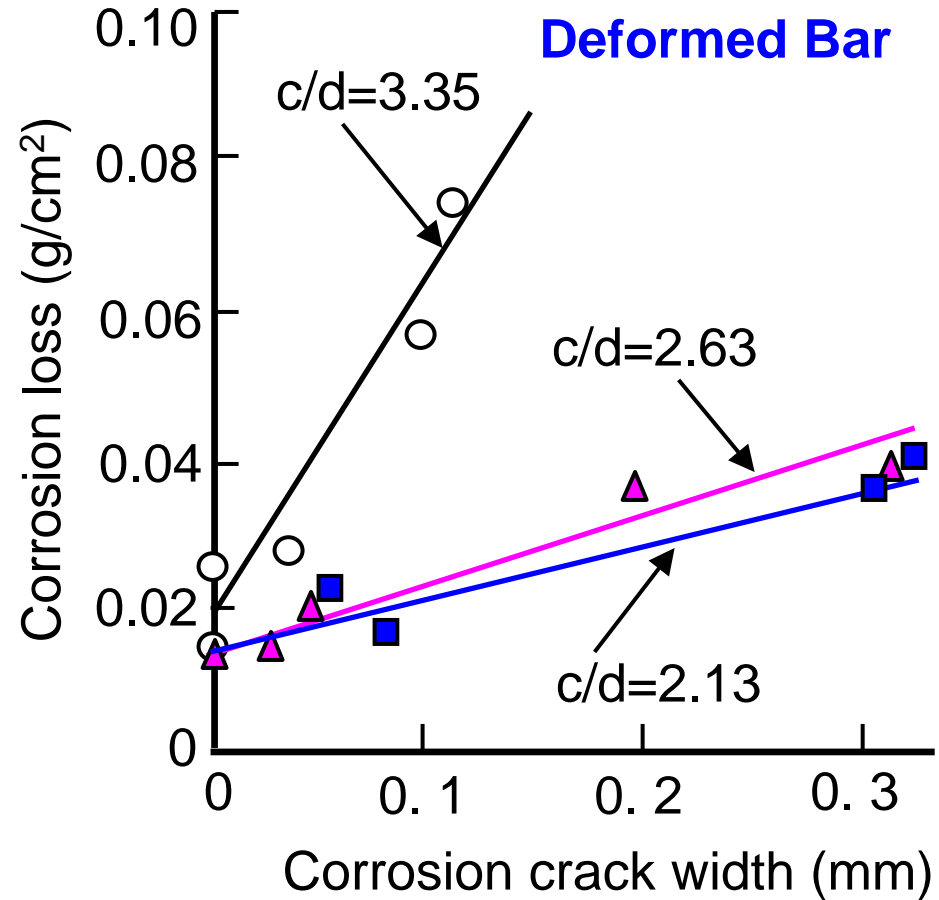
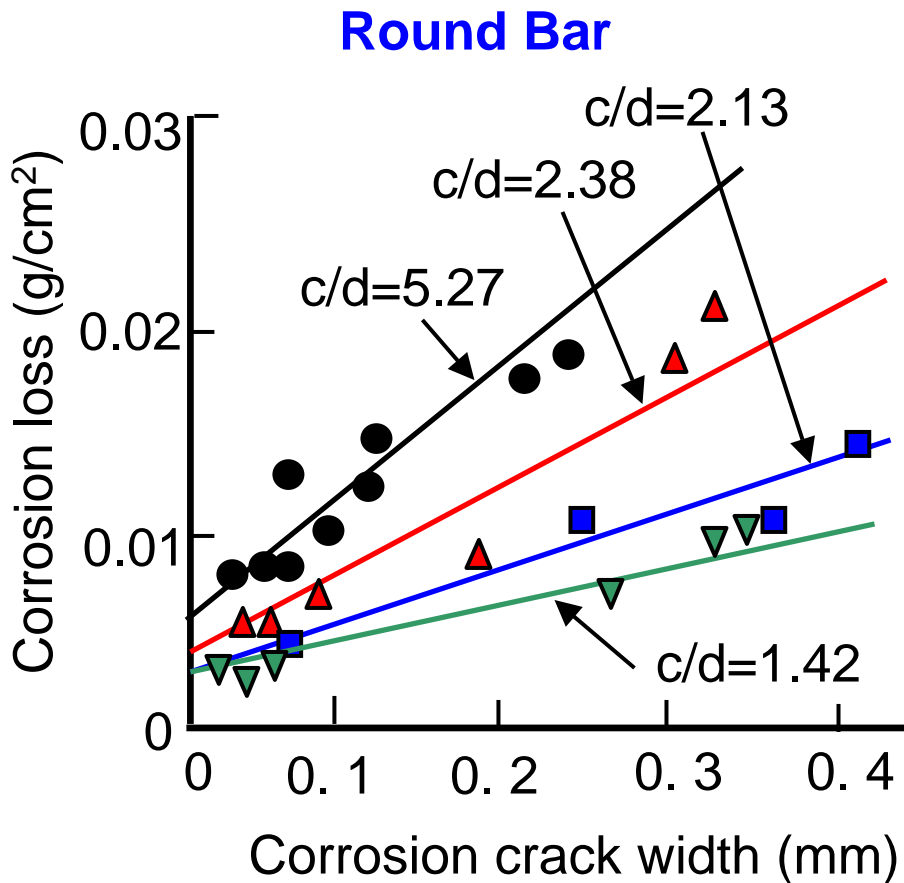


this volume is two to four times of the steel's one



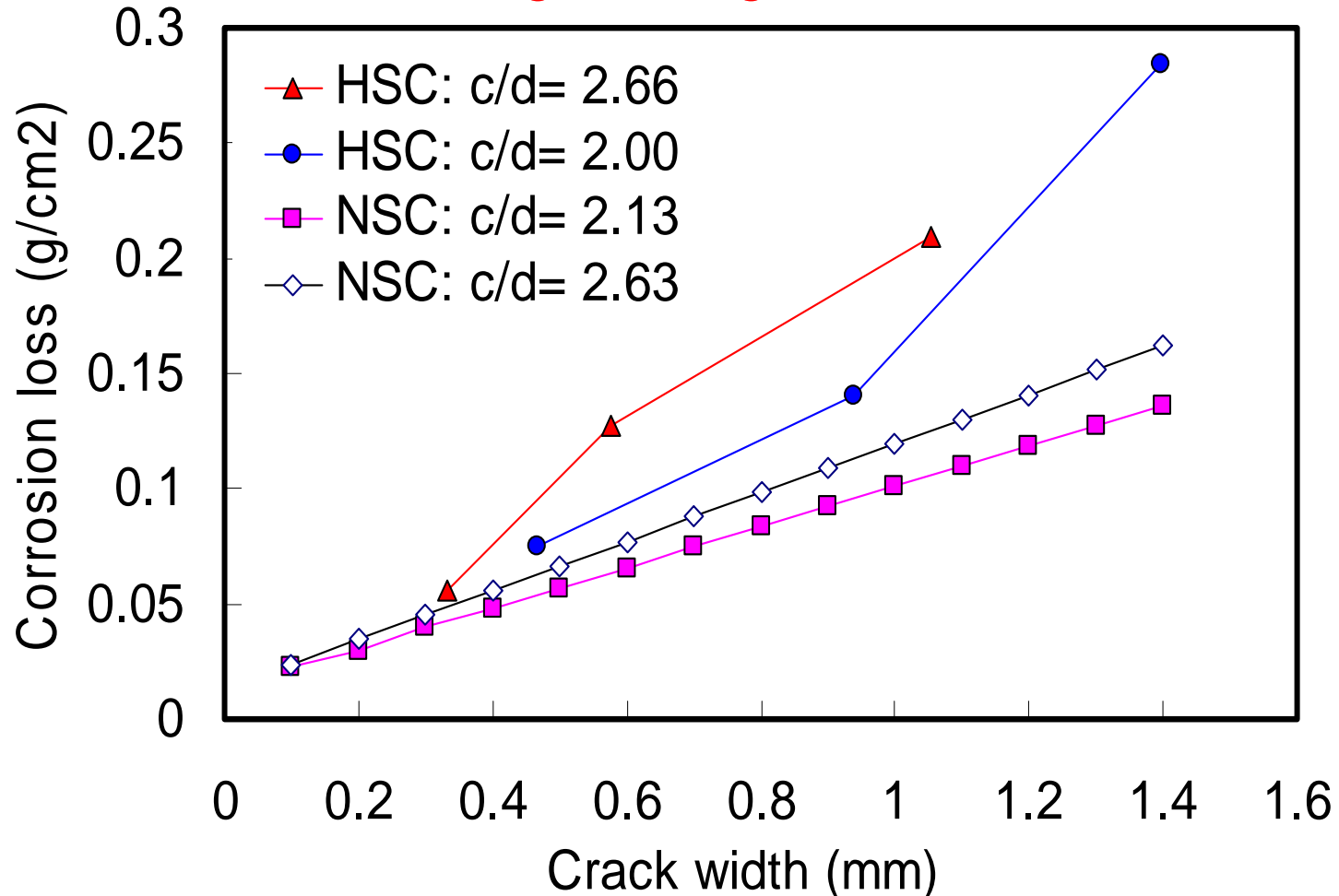
Deterioration process on marine concrete structures

Relationship between corrosion amount and corrosion crack on concrete



c/d: Cover thickness/diameter of rebar

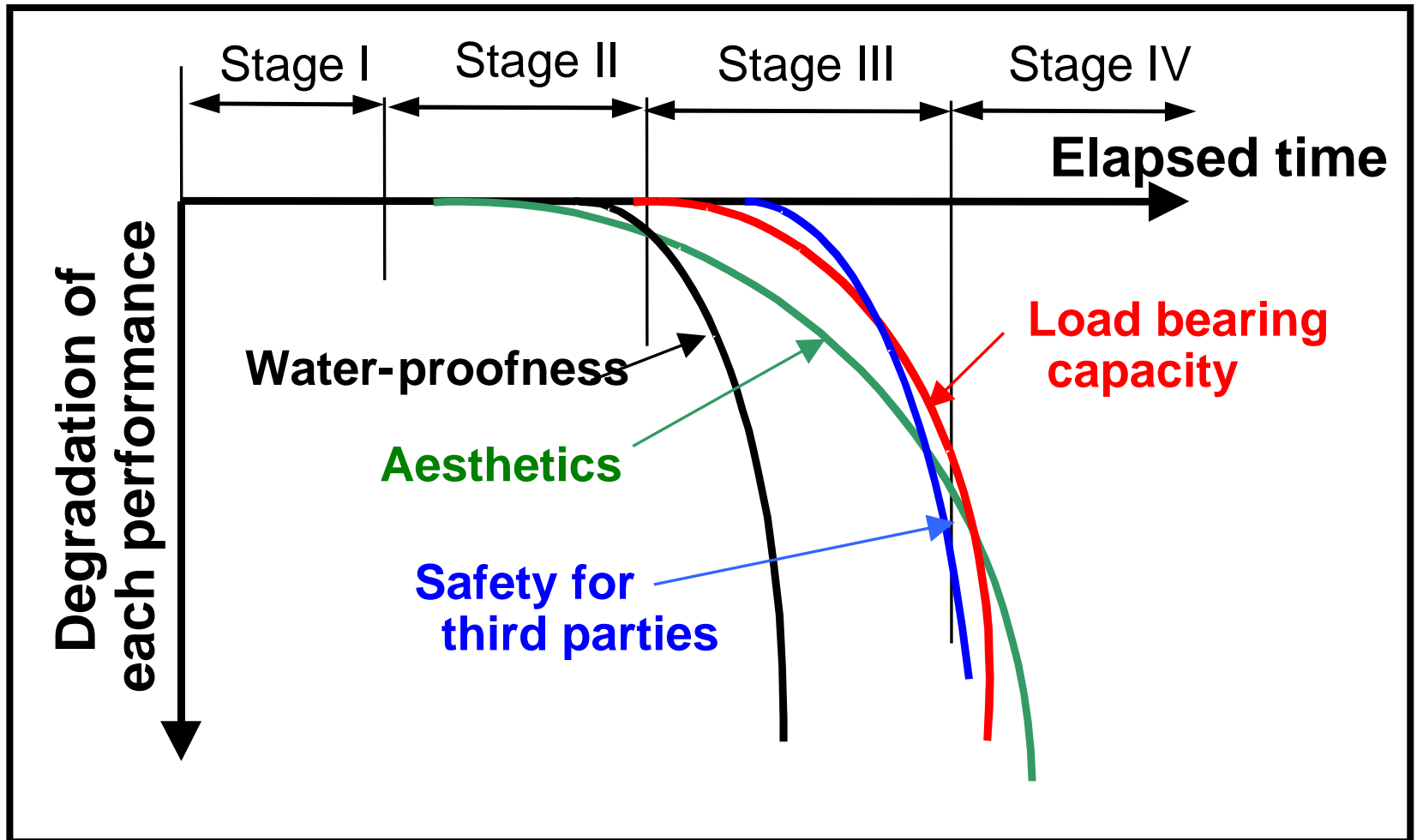
Relationship between corrosion amount and corrosion crack on high strength concrete



- ✓ High strength concrete have smaller crack width opening than normal strength concrete for same corrosion loss
- ✓ Concrete strength also influences on the crack width opening

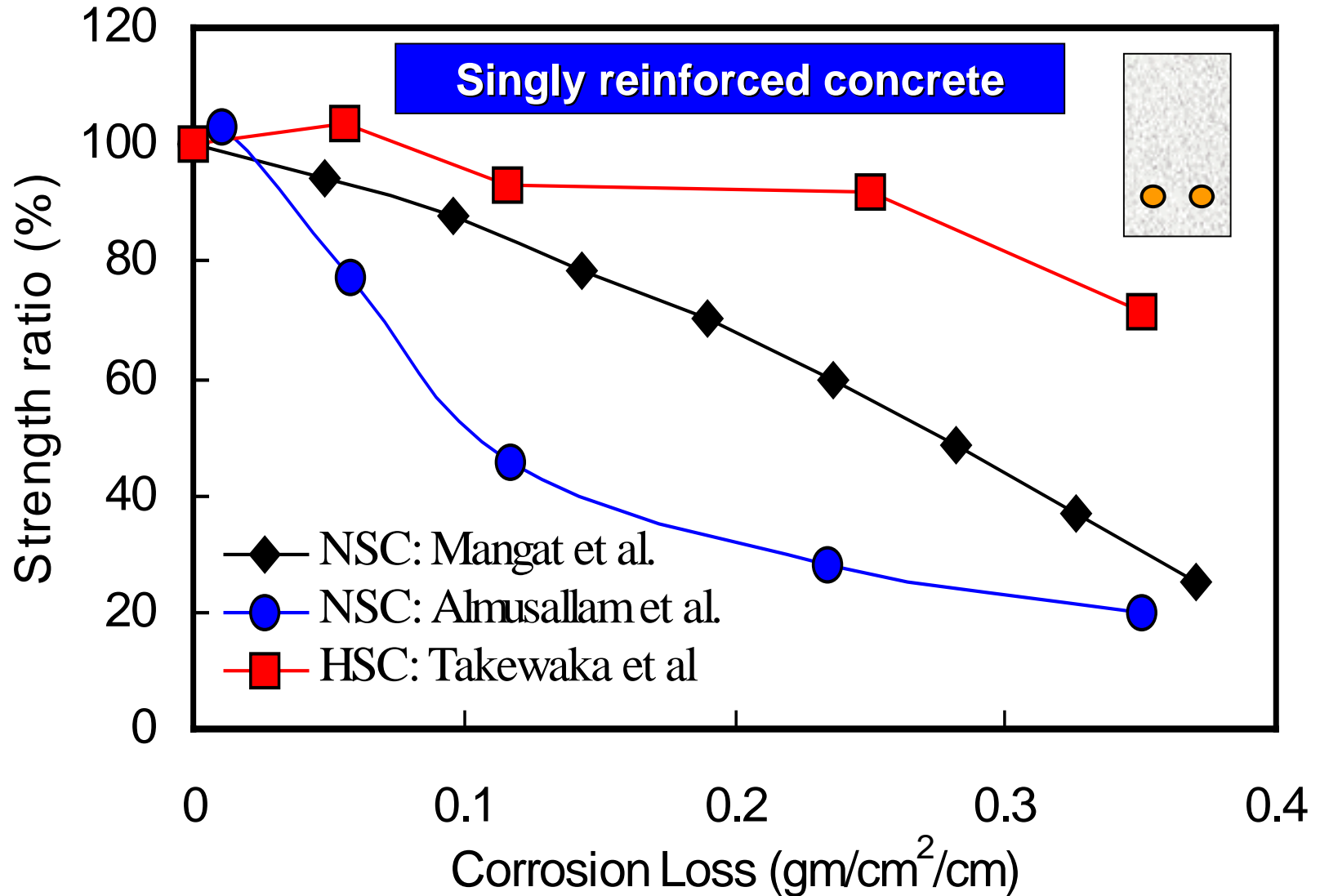
Deterioration process on marine concrete structures

Conceptual figure of degradation process of performance on structure



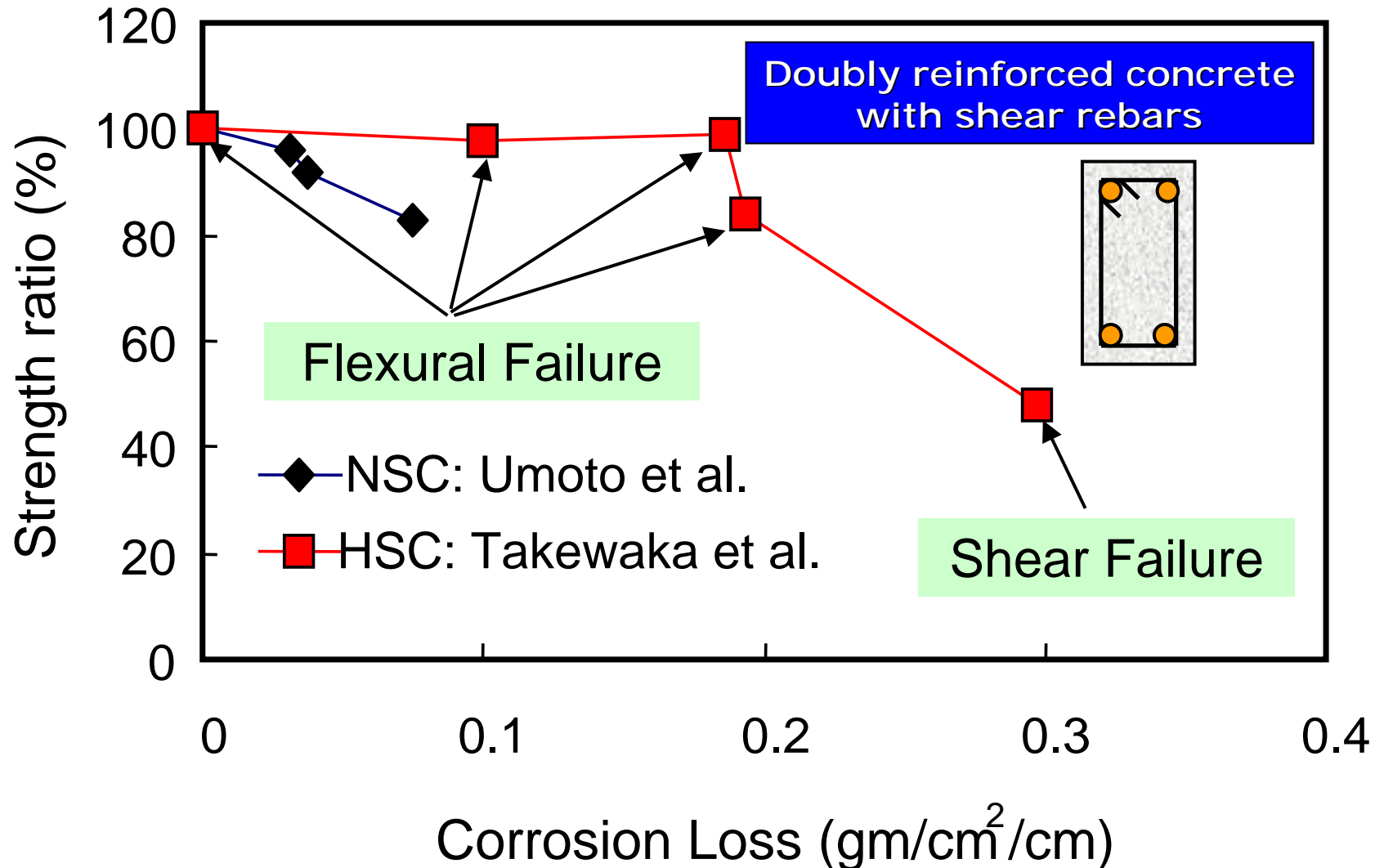
Example of performance degradation on RC beam due to rebar corrosion

Experiment result for loss in load-bearing capacity



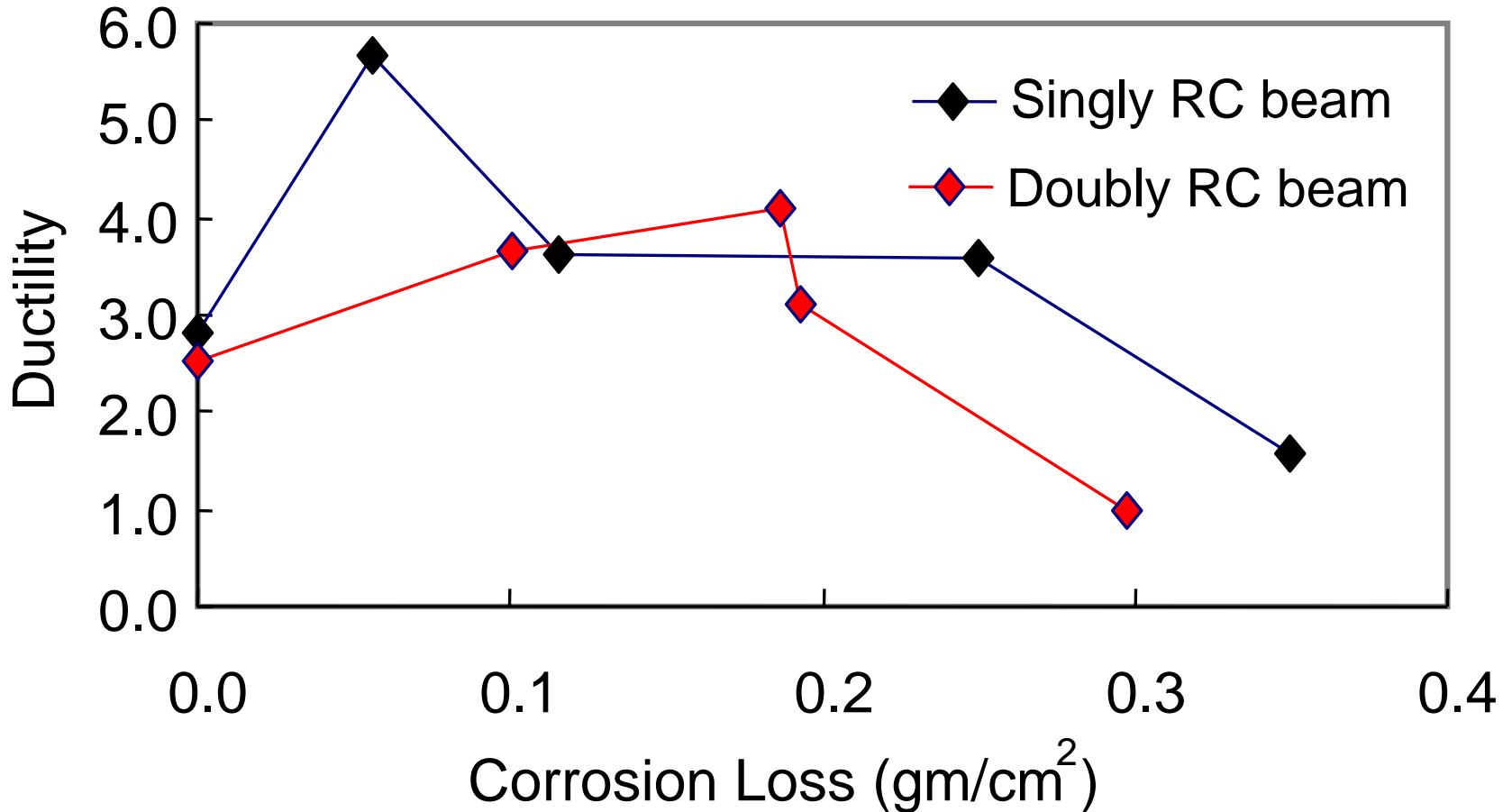
Example of performance degradation on RC beam due to rebar corrosion

Experiment result for loss in load-bearing capacity



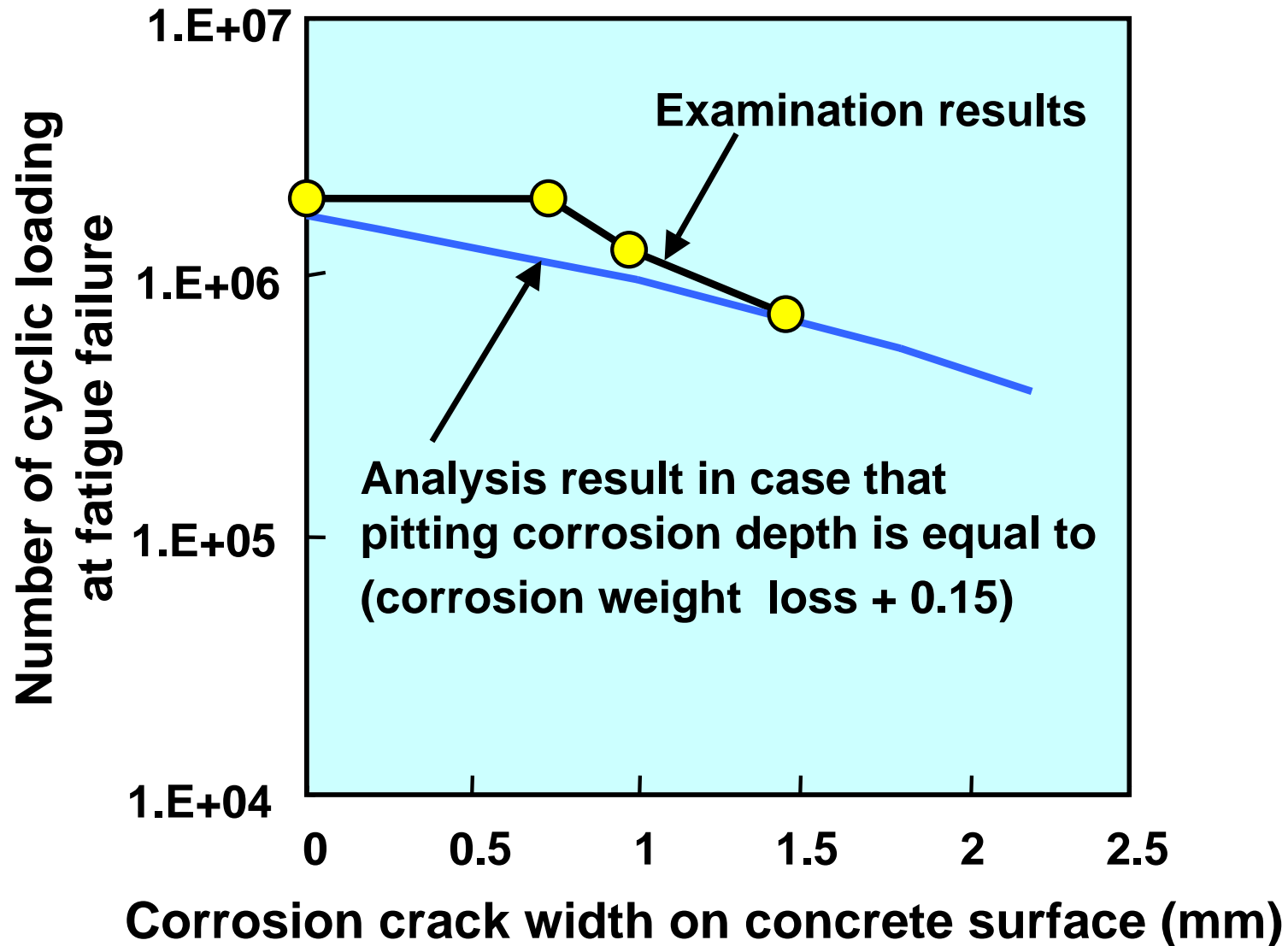
Example of performance degradation on RC beam due to rebar corrosion

Experiment result for loss in ductility of RC beam

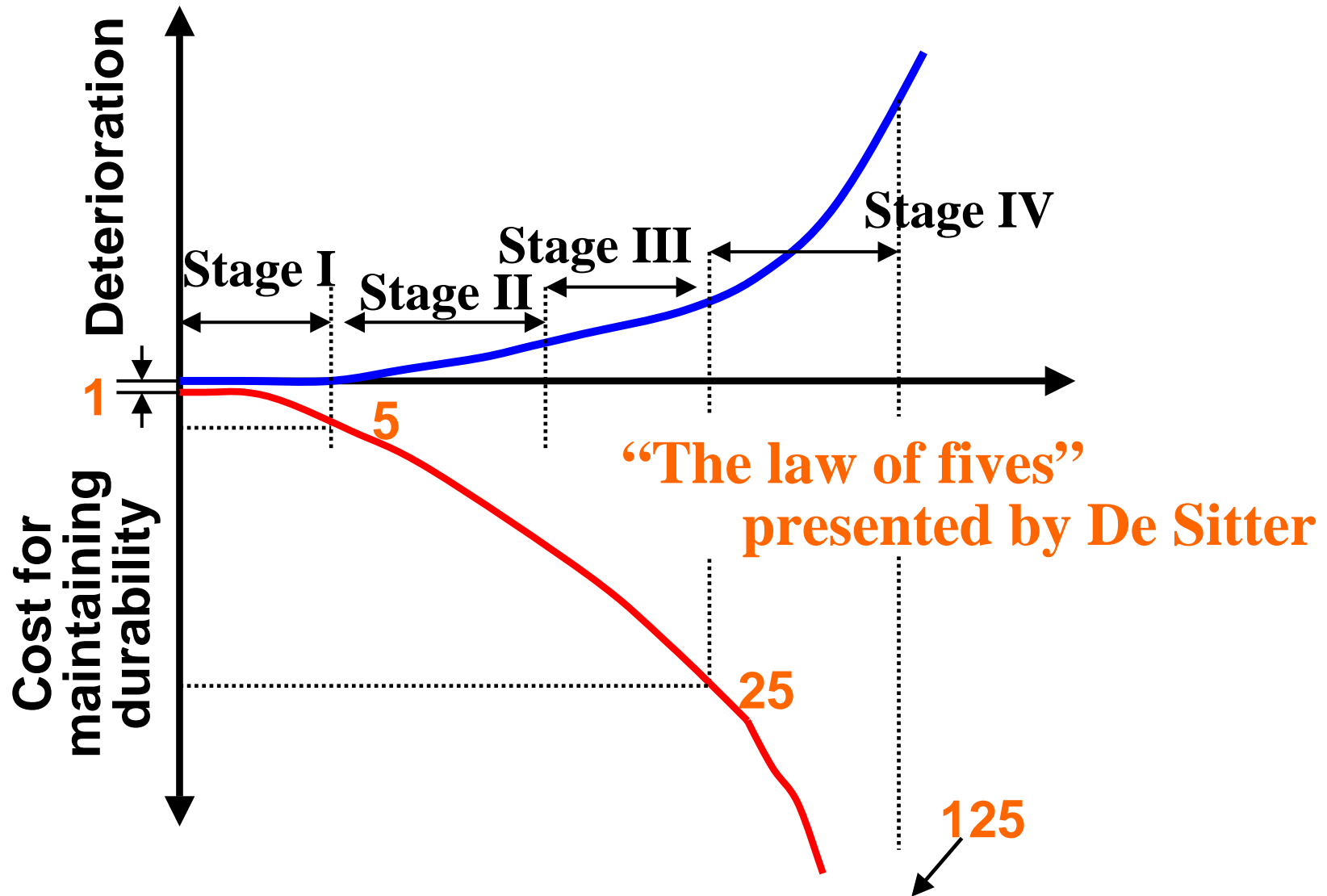


Example of performance degradation on RC beam due to rebar corrosion

Analytical result for loss in fatigue property



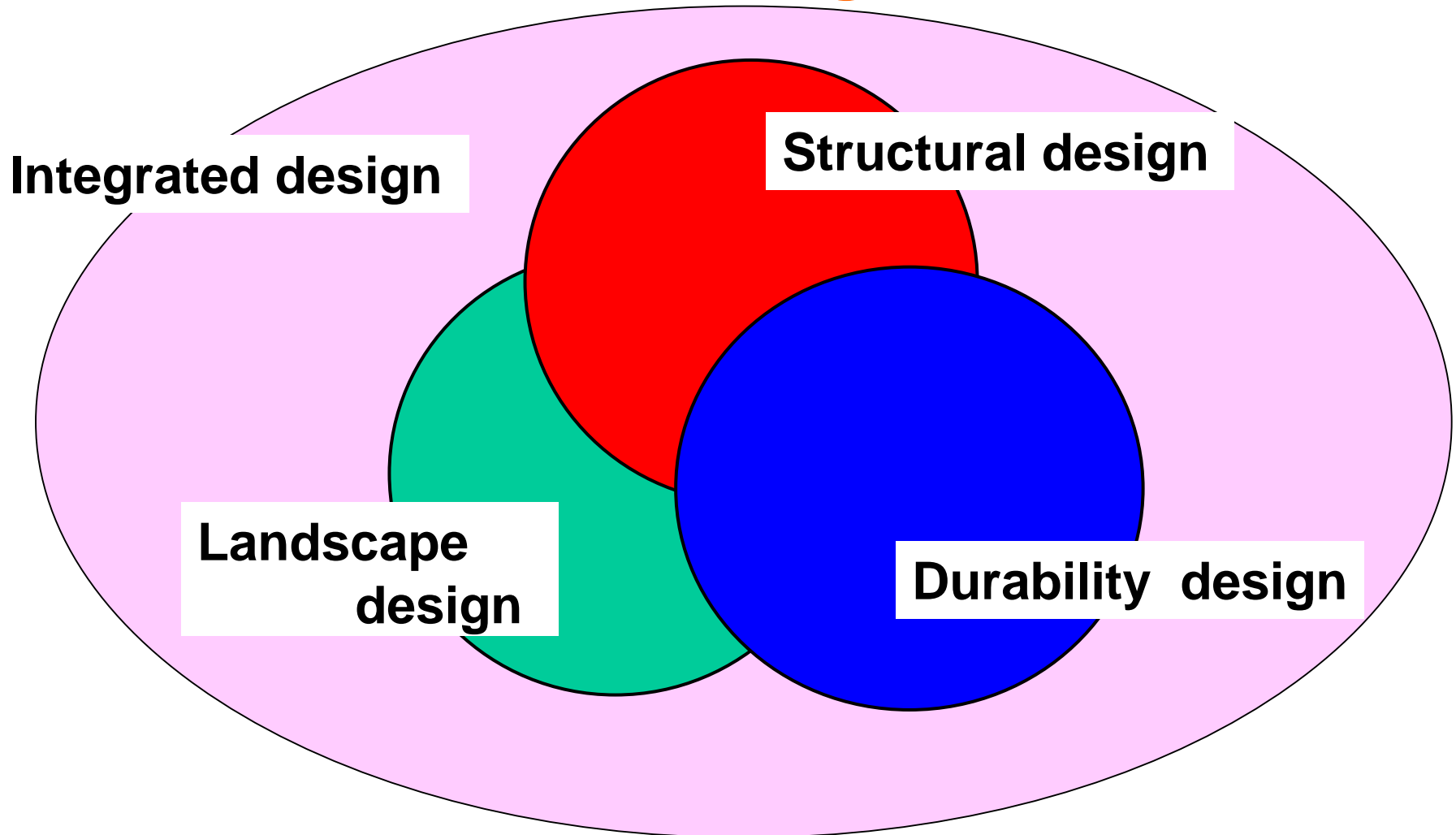
Extra Costs for maintaining durability of structure during the service life



**Examination
in
Durability Design**

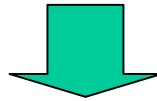
Schematic of design for structure

Performance-based design

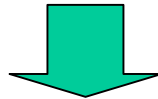


What is “ Durability of structure”

Qualitative performance



Resistance against deteriorating actions from surrounding environment

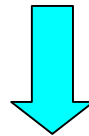


To keep the all of required performances on structure to their levels more than the required ones during the service life

Durability design

Design carried out to ensure that the structure can maintain its required performance (functions) during the service life under environmental actions

defined by Asian concrete model code



Evaluation of long-term-performance

Examination of durability

General principle

All required performances for structure, such as serviceability, restorability and safety under actions in normal use, wind action and seismic action, shall be examined respectively in regard of **their long-term performances in the service life**.

Examination of durability

Examples of durability-limit-state

Durability-limit-state A: All performances maintain the initial conditions.

Durability-limit-state B: Though some material used in structure deteriorates, negligible decay in any performance of structure occurs.

Durability-limit-state C: Though some structural performance deteriorates, function of structure keep in the required condition and the damages are repairable.

Examination of durability

Class A

No deterioration of both structure performance and material.

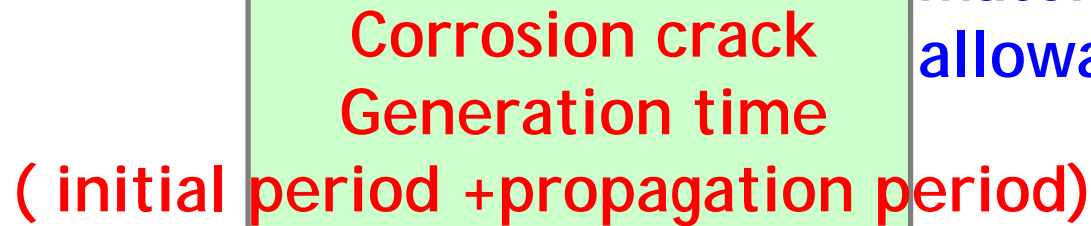
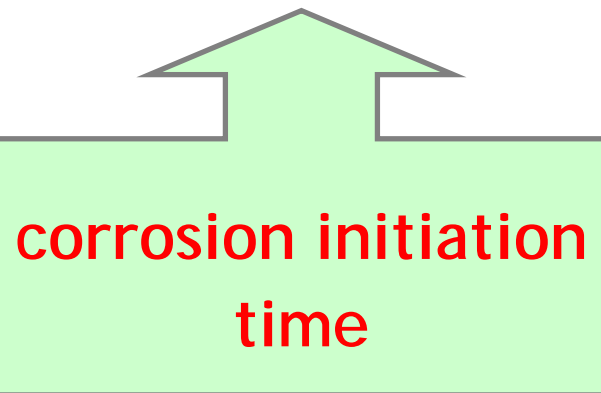
Durability Limit state

Class B

Some deterioration on material, No deterioration of structure performance.

Class C

Deterioration can occur on both performance of structure and material within allowable range .



Examination of durability

Durability-limit-state for marine concrete structures

Durability-limit-state A:

- All performances maintain the initial condition

$$t_d \leq t_{cr}$$

t_d : Design service life of marine concrete structure

t_{cr} : Duration until reinforcement starts to corrode



t_{cr} is seemed to be the duration until concentration of Cl⁻ accumulating on reinforcement surface reaches a critical value for starting corrosion

Examination of durability

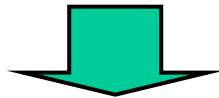
Evaluation method in durability-limit-state A

$$\gamma \cdot \frac{C_{(c, Td)}}{C_{lim}} \leq 1.0$$

$C_{(c, Td)}$: Chloride content at reinforcement position during service life of structure

C_{lim} : Critical chloride content

γ : Safety factor



This concept was Introduced in **1999 version of JSCE standard specification for design of concrete structure** as the verification method of durability of concrete structure

$$C_{(c, T_d)}$$

Simplified Fick's second law

$$\frac{\partial C}{\partial t} = D \frac{\partial^2 C}{\partial x^2}$$

C: Concentration of Cl⁻ at depth x after t

D: Diffusion coefficient



Theoretical analysis

- In sea water or tidal zone**

$$C_{(c, T_d)} = C_0 \left[1 - \operatorname{erf} \left(\frac{c}{2\sqrt{D \cdot T_d}} \right) \right]$$

here,

$$\operatorname{erf}(s) = \frac{2}{\sqrt{\pi}} \int_0^s e^{-\eta^2} d\eta$$

- In splash zone or atmospheric zone**

$$C_{(c, T_d)} = 2W \left[\sqrt{\frac{T_d}{\pi D}} \cdot \exp\left(\frac{c^2}{4DT_d}\right) - \frac{c^2}{2D} \left[1 - \operatorname{erf} \left(\frac{c}{2\sqrt{D \cdot T_d}} \right) \right] \right]$$

C₀ : Chloride content on concrete surface

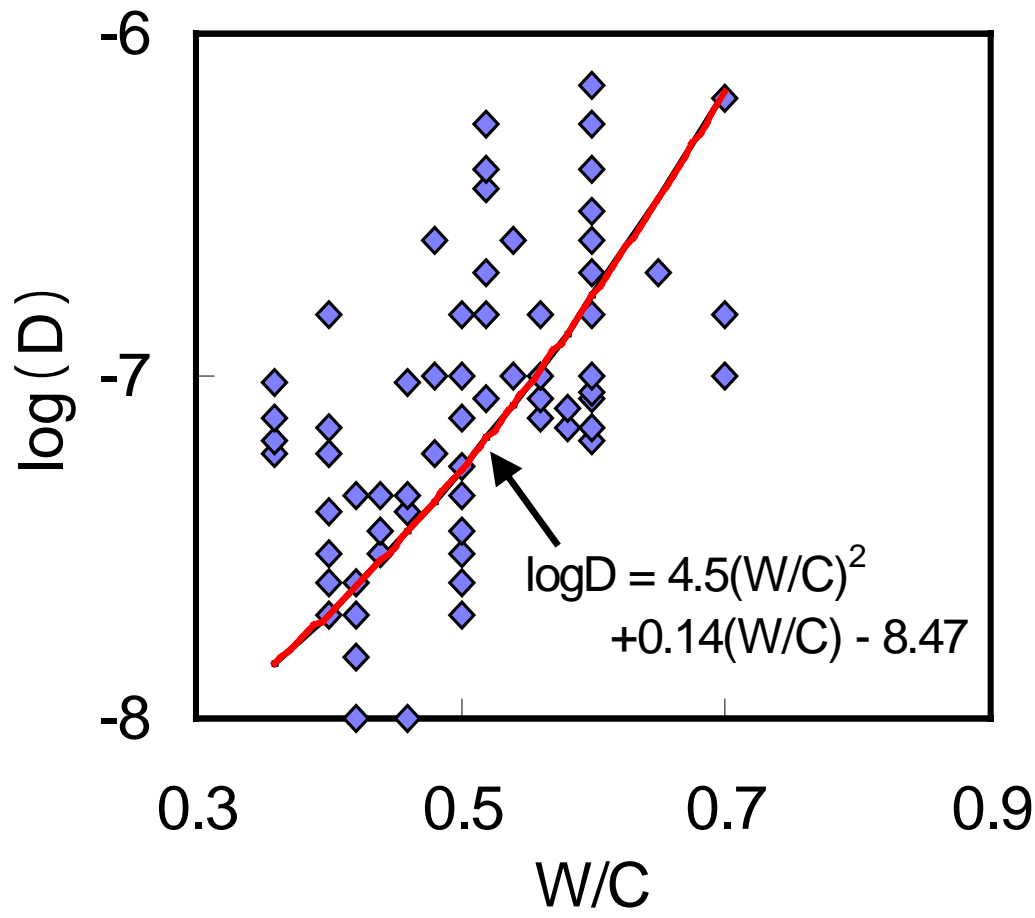
D : Chloride diffusion coefficient of concrete

T_d : Design service life

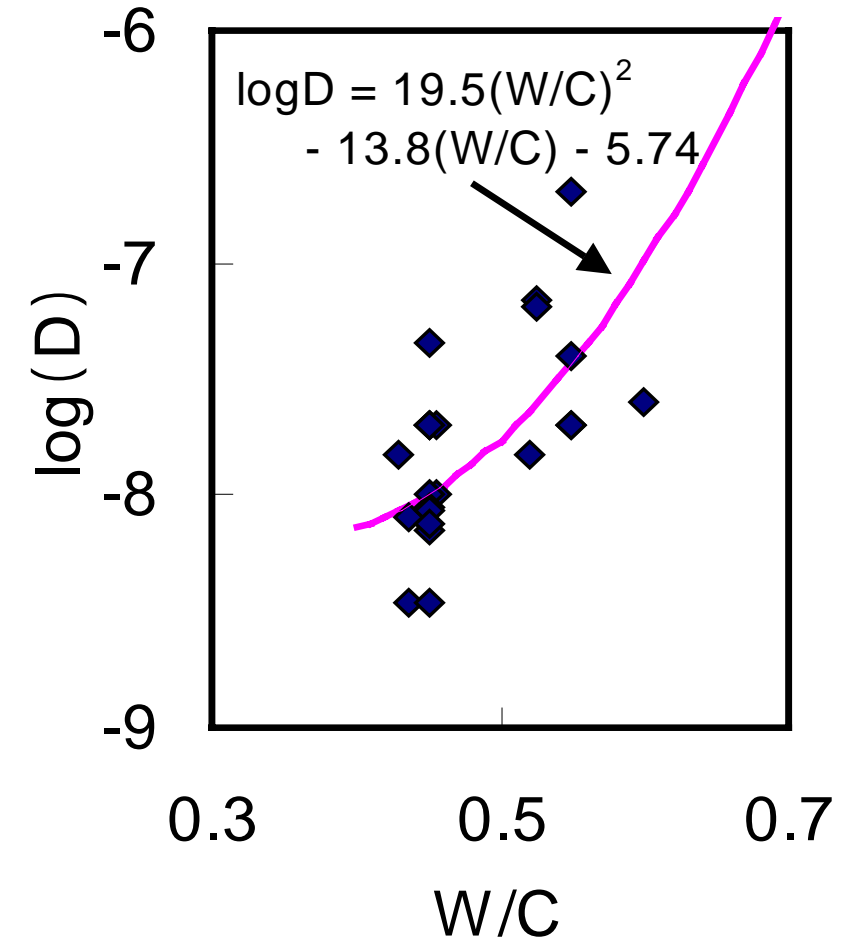
c : Minimum cover thickness

W : Accumulated chloride amount on concrete surface during unit time

Relationship between chloride diffusion coefficient and W/C of concrete



(a) In case of OPC



(b) In case of BFSC

Durability-limit-state for marine concrete structures

Durability-limit-state B:

- Though some material used in structure deteriorate, negligible decay in any performance of structure occurs

$$t_d \leq t_{cr} + t_{ck}$$

t_d : Design service life of marine concrete structure

t_{cr} : Duration until reinforcement start to corrode

t_{ck} : Period of corrosion progress on reinforcement from start of corrosion until occurrence of corrosion crack on concrete

$$t_d = t_{cr} + t_{ck}$$

t_{cr} : Duration until reinforcement start to corrode

$$t_{cr} = \frac{c^2}{4D_d \cdot [erf^{-1}(1 - C_d / C_0)]^2}$$

t_{ck} : Period of corrosion progress on reinforcement from start of corrosion until corrosion crack occurs on concrete

$$t_{ck} = \frac{1.7\alpha_N(1 + \alpha_\phi \cdot c)^{0.85} \cdot c \cdot \left[\frac{1}{(W/C)} - 1 \right] \cdot \alpha_C}{E_h \cdot \beta_t}$$

$$t_{ck} = \frac{1.7\alpha_N(1+\alpha_\phi \cdot c)^{0.85} \cdot c \cdot \left[\frac{1}{(W/C)} - 1 \right] \cdot \alpha_C}{E_h \cdot \beta_t}$$

c : Concrete cover

W/C : Water to cement ratio

α_N : Factor for strength of concrete: = 0.5/(W/C)

α_ϕ : Factor for diameter of rebar(ϕ): = 2/ ϕ

E_h : Factor for environment: = 1.5 (in sea water)

2.5 (tidal zone)

3.5 (splash zone, coast line)

2.0 (others)

β_t : Factor for average temperature: = 0.7 (under 10°C)

1.0 (10 ~ 20°C)

1.3 (over 20°C)

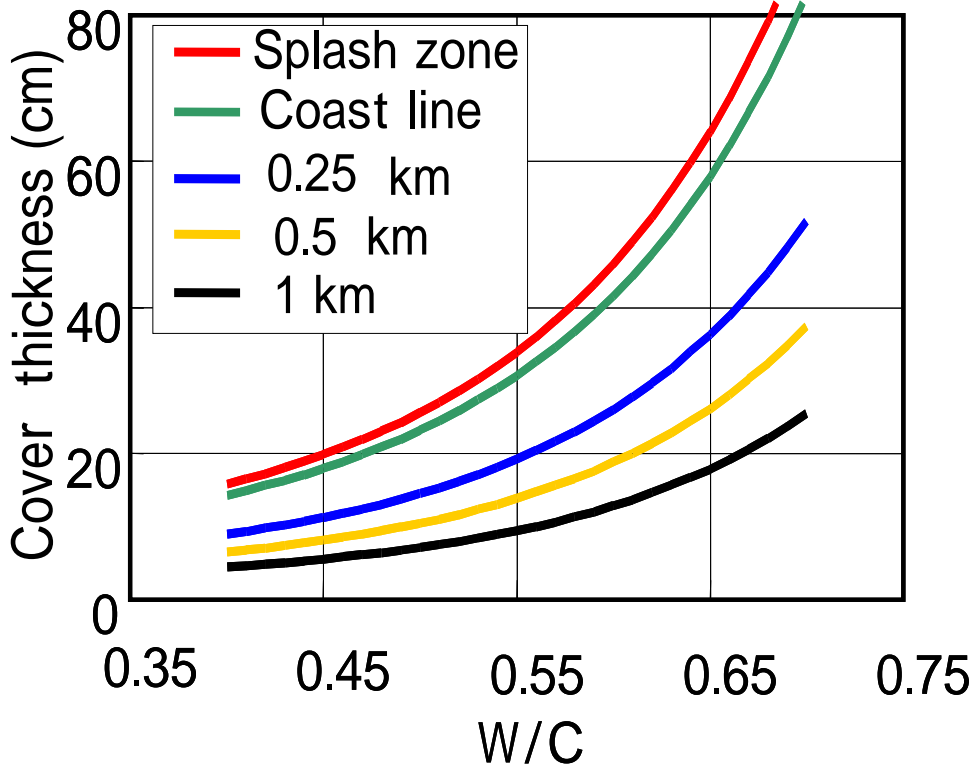
α_C : Factor for type of cement: = 1.0 (OPC)

1.25 (BFSC)

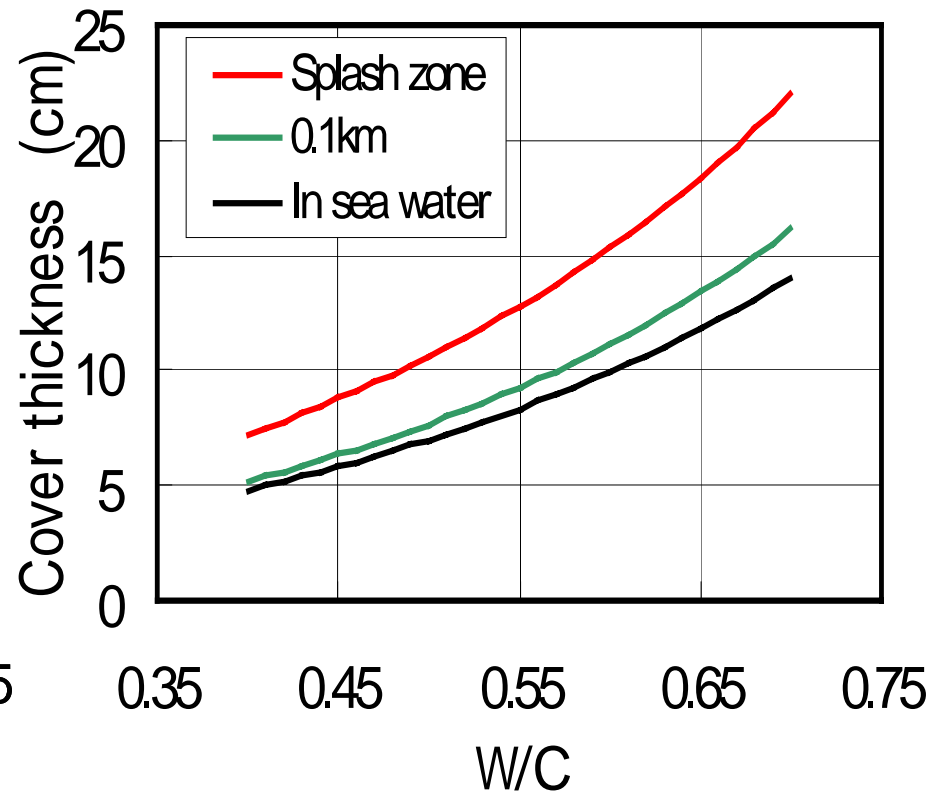
Relationship between minimum cover thickness and maximum W/C required for durability

Design condition
OPC, Design service life: 50 years

Durability-Limit-state A



Durability-Limit-state B

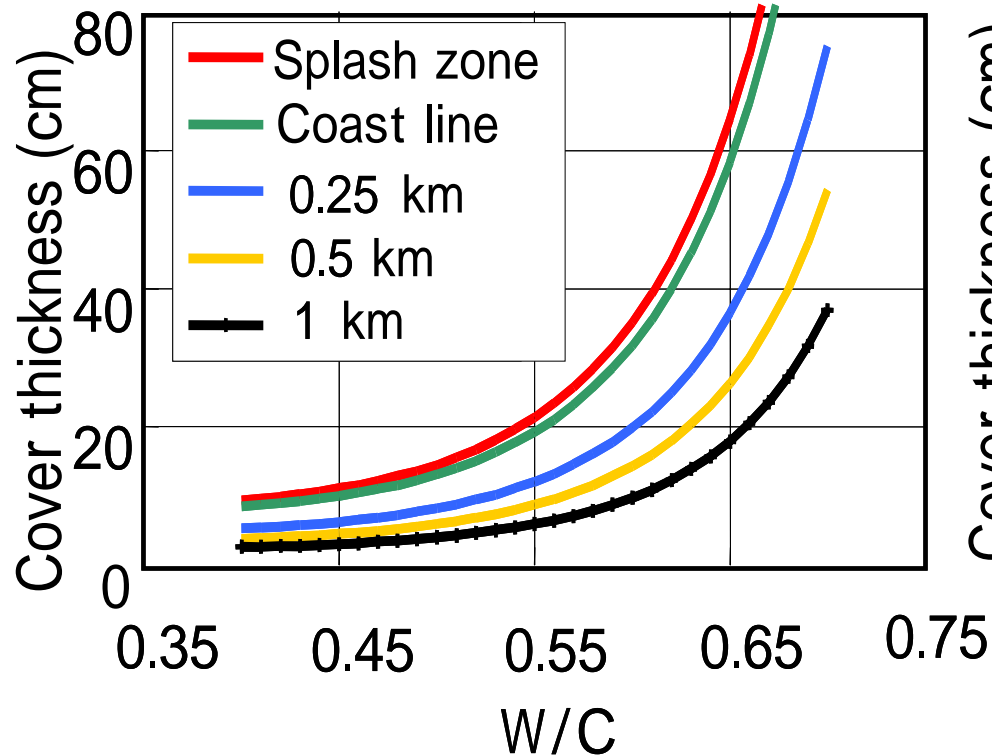


Relationship between minimum cover thickness and maximum W/C required for durability

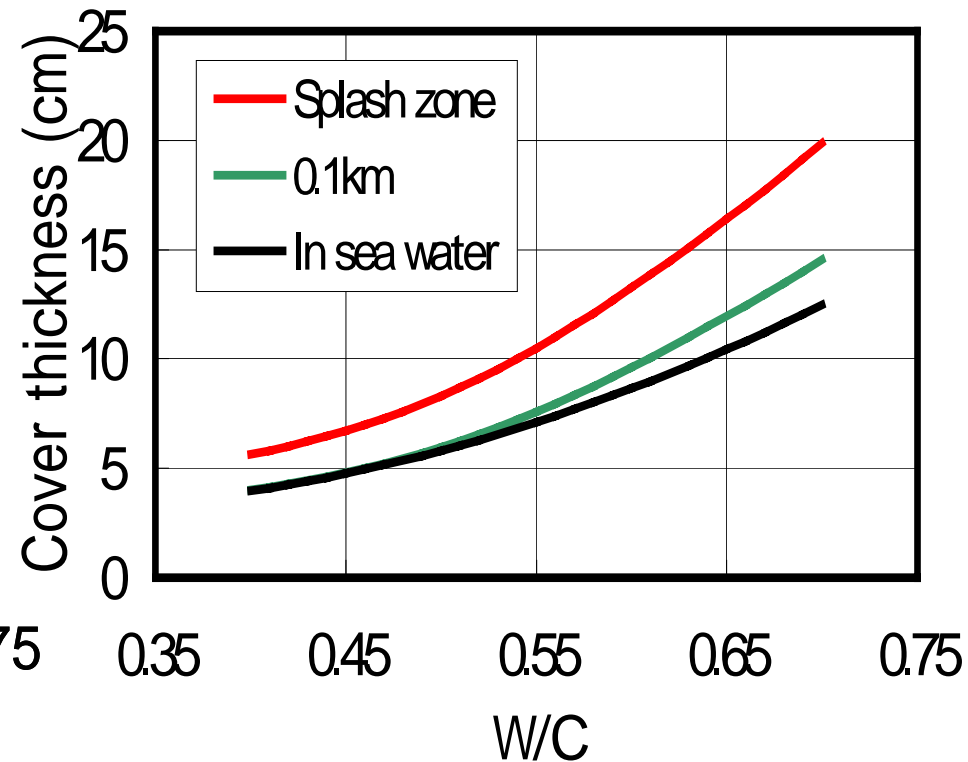
Design condition

Blast furnace slag: 50%, Design service life: 50 years

Durability-Limit-state A



Durability-Limit-state B



Computer Simulation Model

Simulation model for deterioration of concrete structure in marine environment

To evaluate more directly the durability in actual condition by using deterioration simulating model

Simulation model

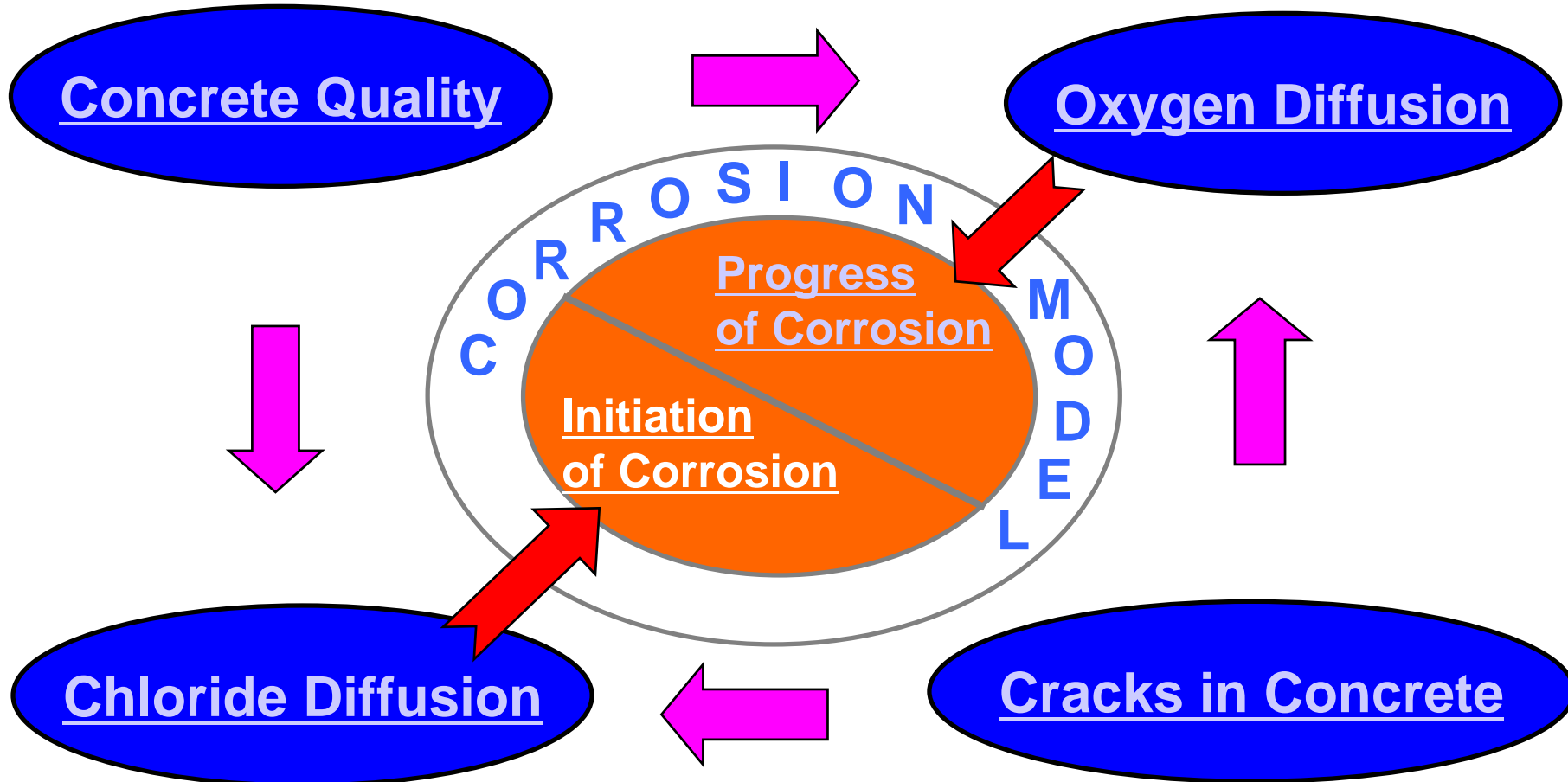
- Concrete model considering scatter of quality
- Penetration model of chloride and oxygen
- Corrosion model of reinforcement

Estimation

- Progress of corrosion of reinforcement
- Period of corrosion crack generation

Simulation model for deterioration of concrete structure in marine environment

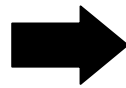
Framework of Corrosion Simulation model



Outline of the concrete model

2 dimensional reinforced concrete model

**Pore distribution
in concrete**



Circular-pore distribution

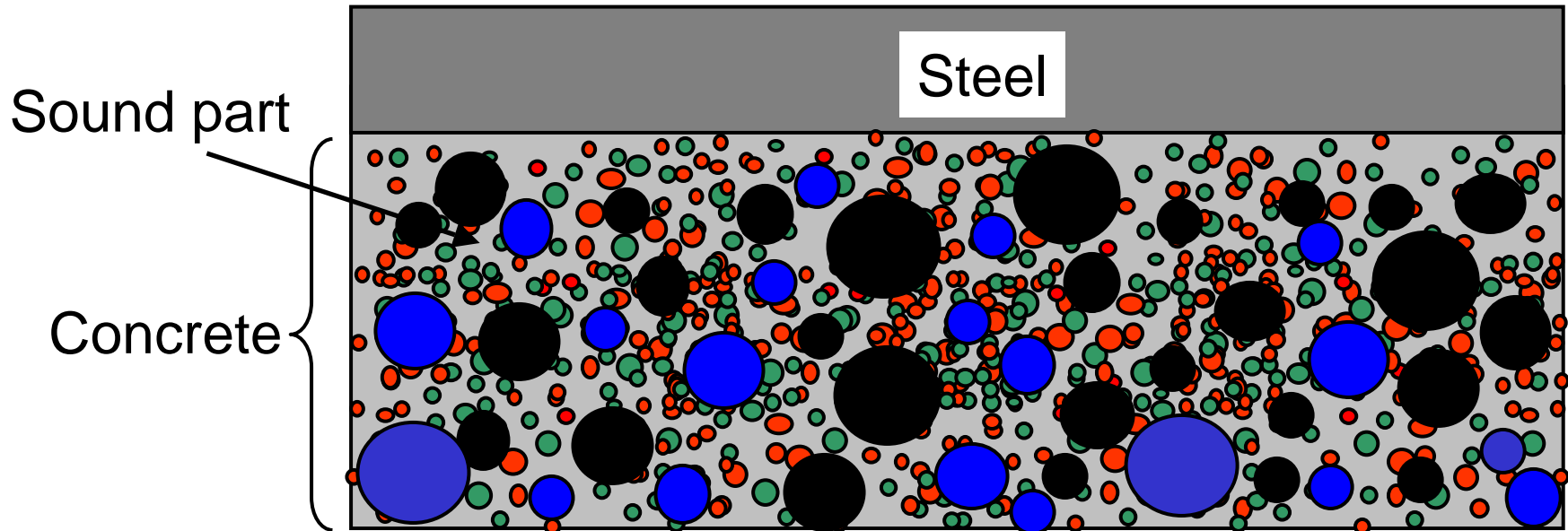
- Randomly located
- Considering W/C and RH

**Aggregate distribution
in concrete**

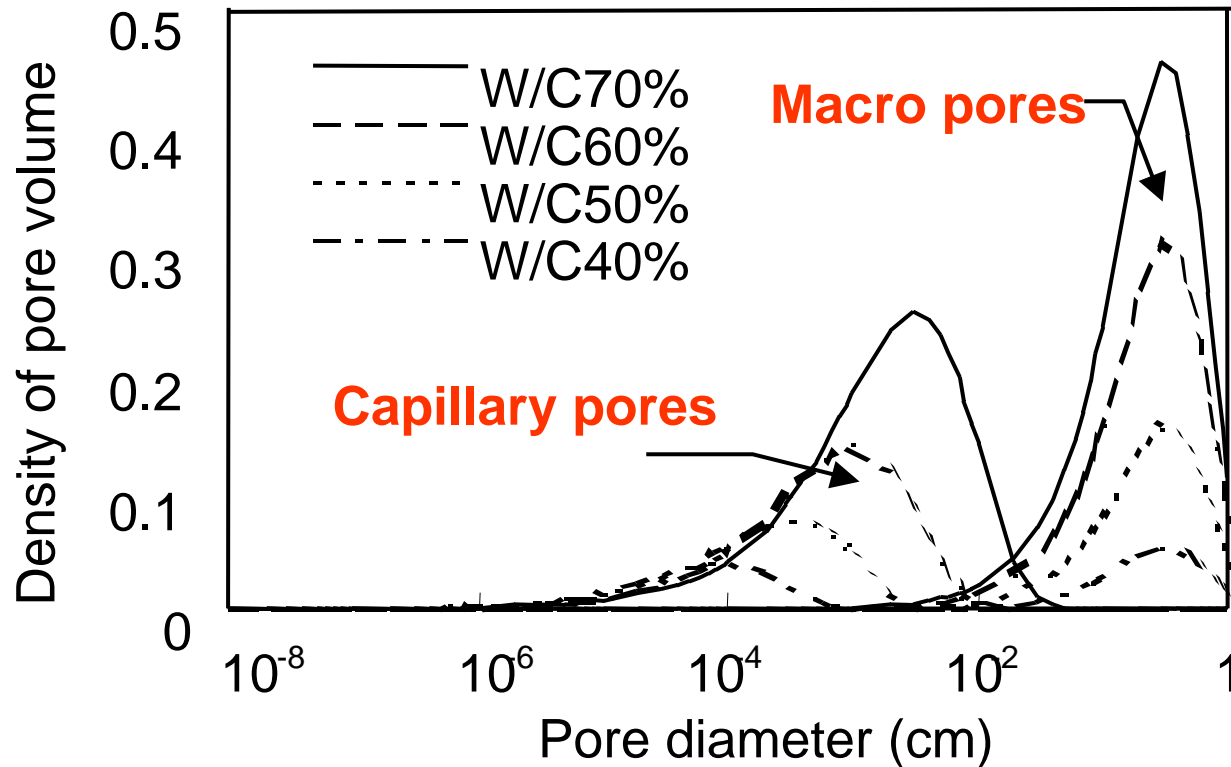


Circular-Aggregate distribution

- Randomly located
- Considering ITZ



Modified pore distribution



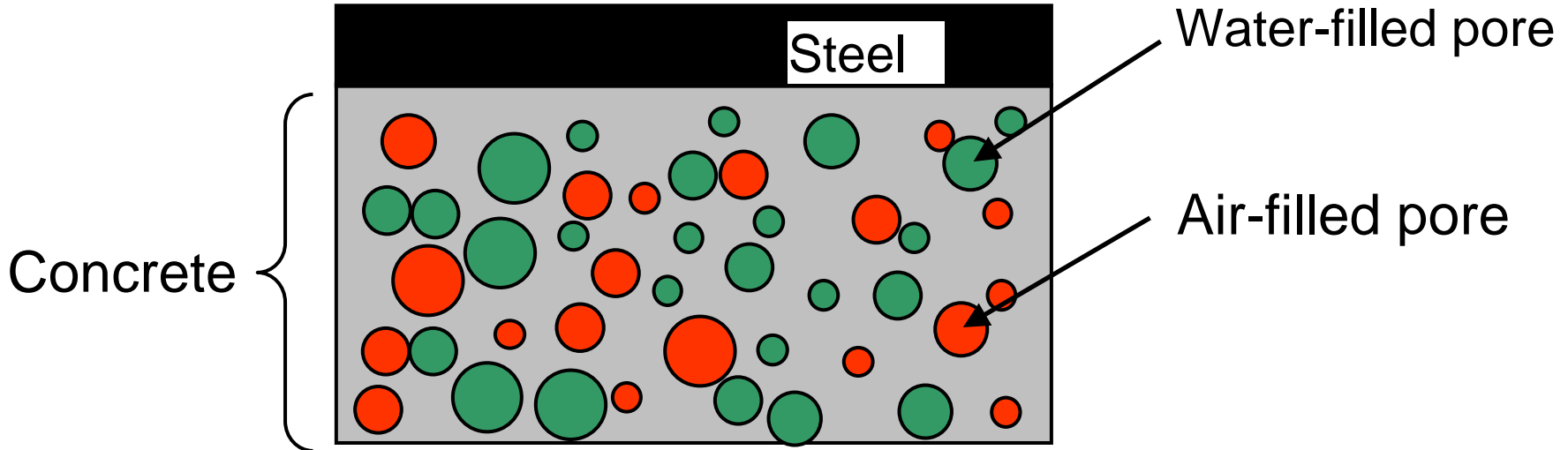
(by Shimomura et al)

$$V'(r) = V'(r_0) \cdot B \cdot C \cdot r^{C-1} \cdot \exp(-Br^C)$$

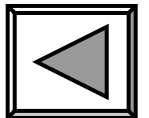
$V'(r)$: Density of pore volume

B, C : Parameters depending on W/C

Modified relative humidity

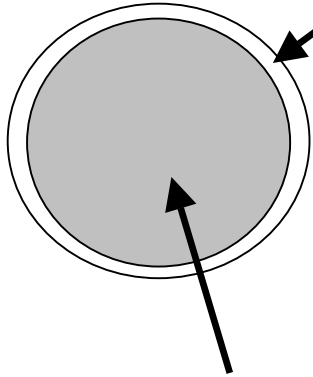


$$\text{Relative humidity} = \frac{\text{Water-filled pore volume}}{\text{Total pore volume}}$$



Model of aggregate

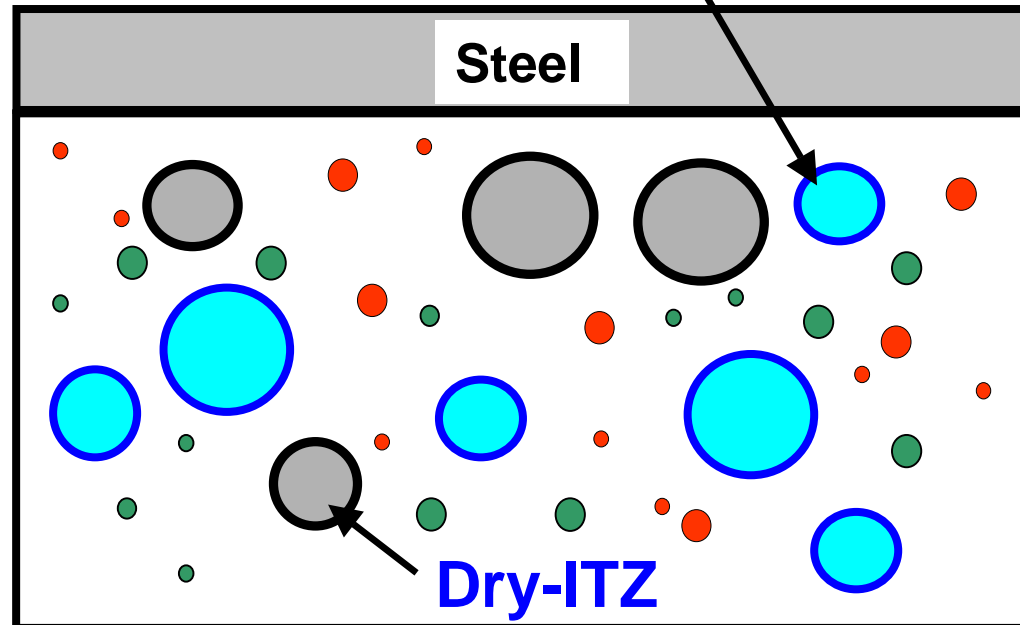
Interfacial transition zone (**ITZ**)



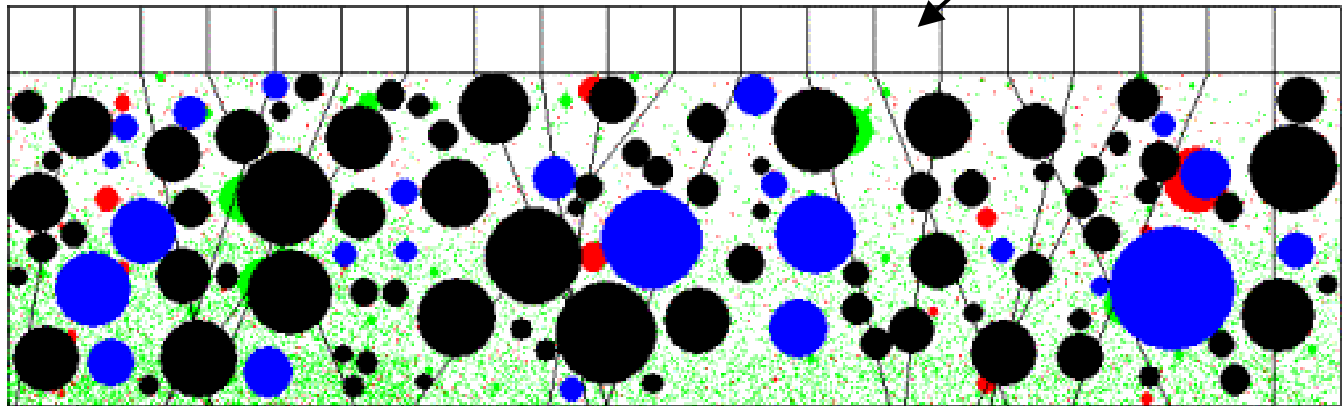
The zone with several micrometers thickness lying between aggregates and hardened cement paste matrix, which has higher porosity than the bulk cement paste

Coarse Aggregate

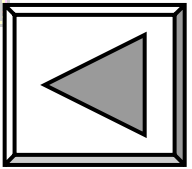
Concrete



Steel



- Wet-aggregate
- Water- filled pore
- Dry-aggregate
- Air- filled pore



Specification of a route on which chlorides reach rebar in minimum diffusion time

For each section (1cm)



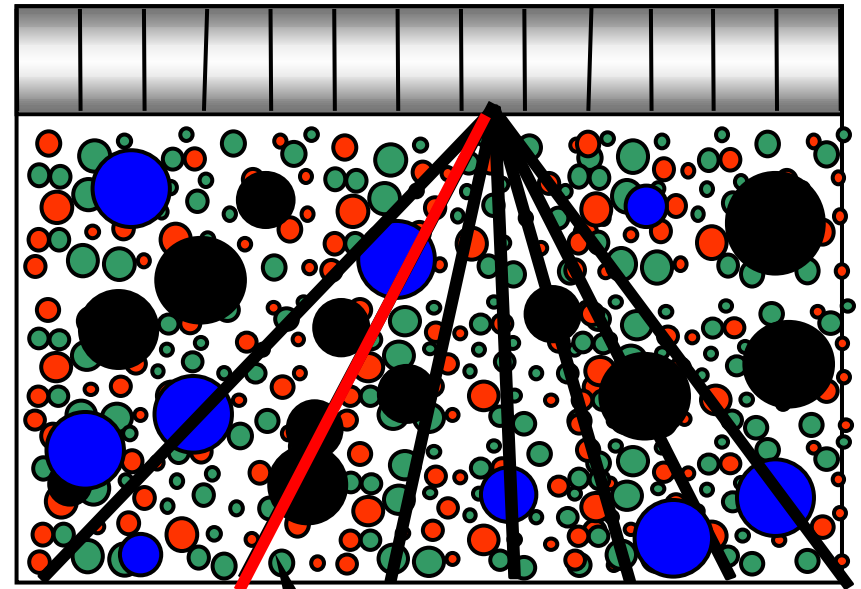
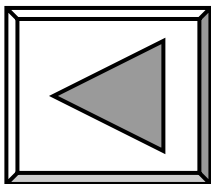
Many diffusion route



Minimum diffusion time

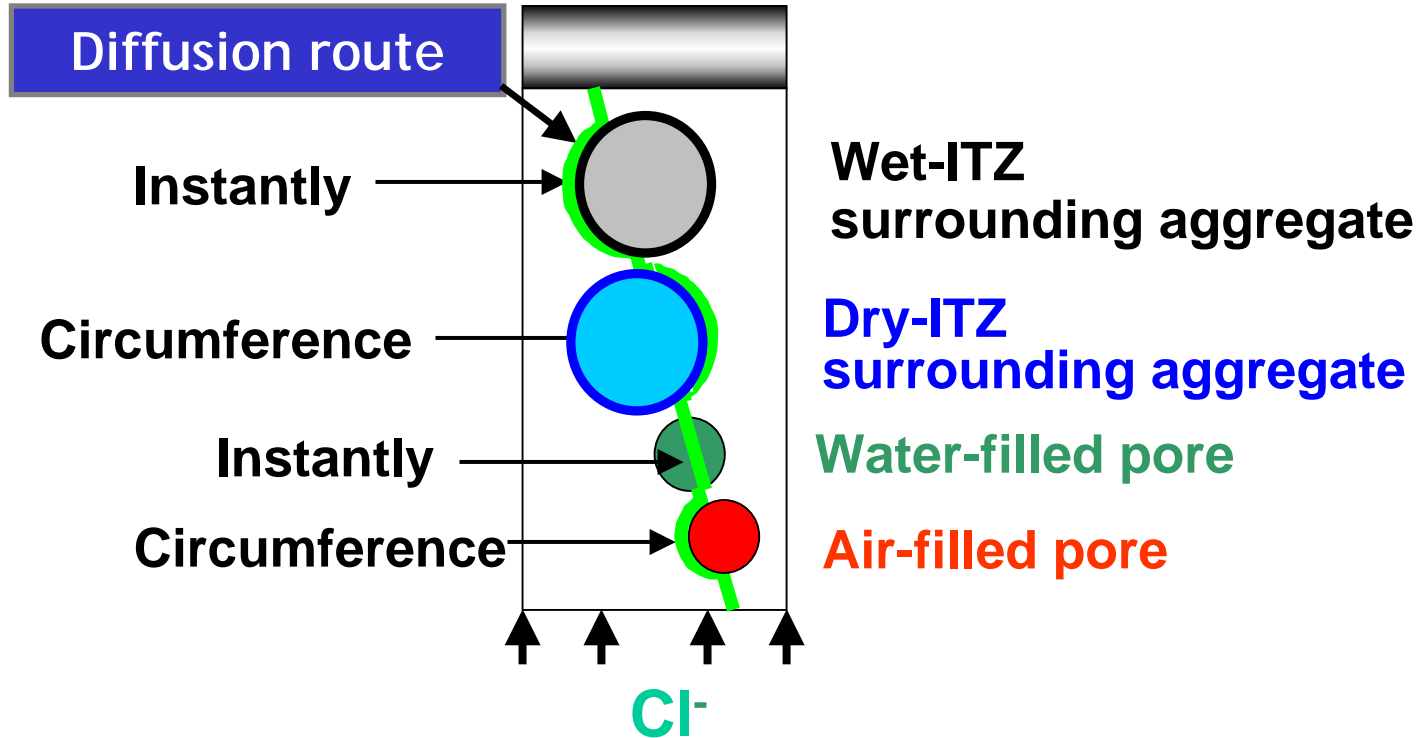


One specific route



Minimum diffusion route

Chloride Penetration Model



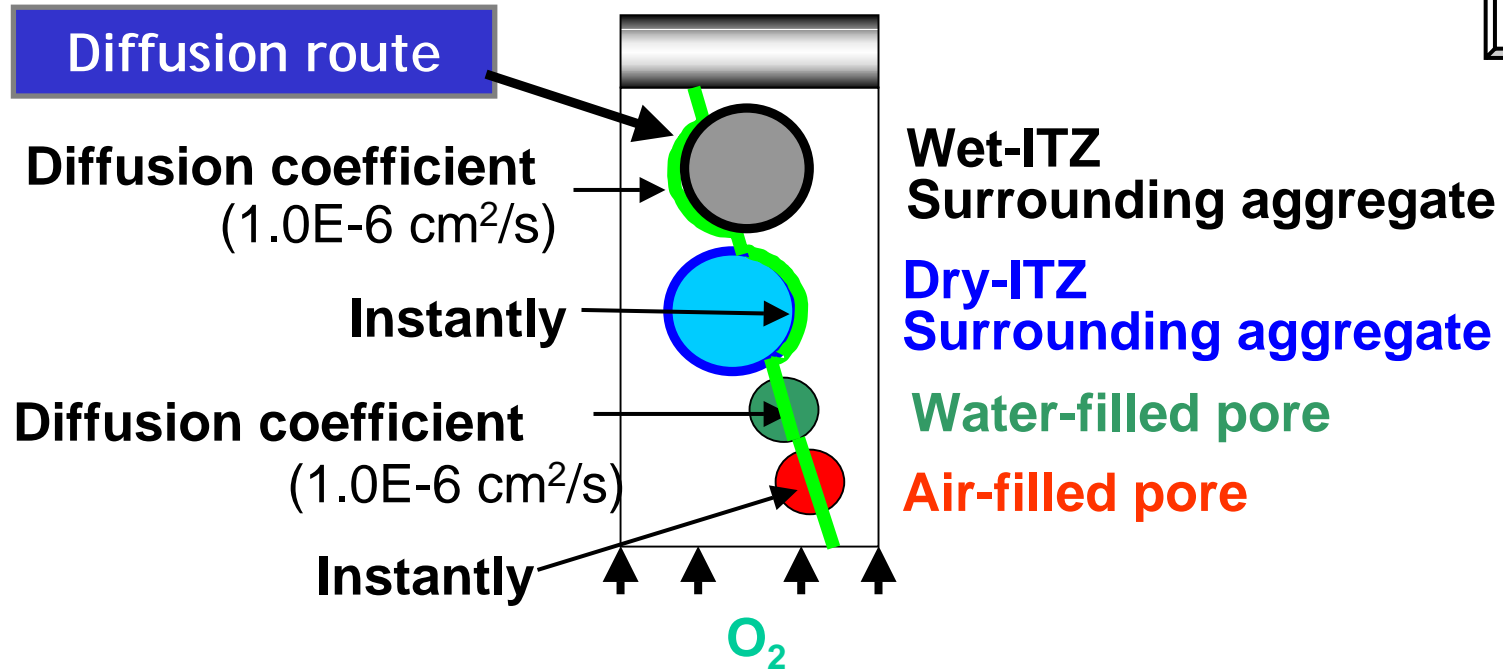
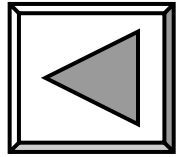
Diffusion of **Free chloride** described by
Modified Fick's 2nd law

$$\frac{\partial C_f}{\partial t} = D \frac{\partial^2 C_f}{\partial x^2} - KC_f$$

C_f : free chloride concentration

K : combined coefficient

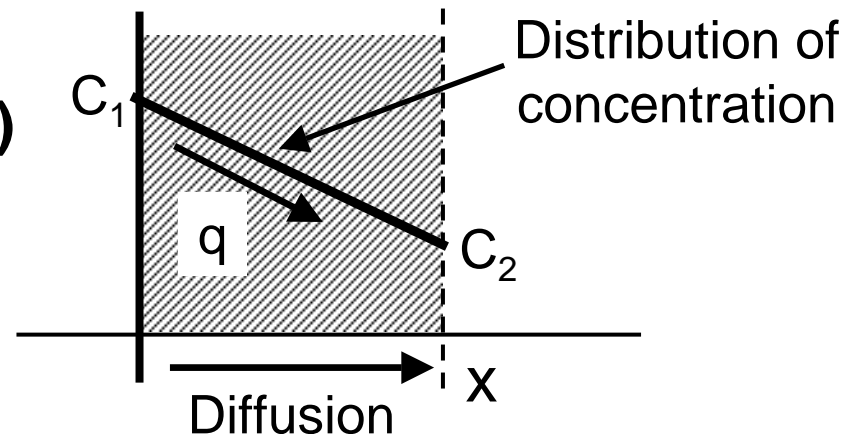
Oxygen Penetration Model



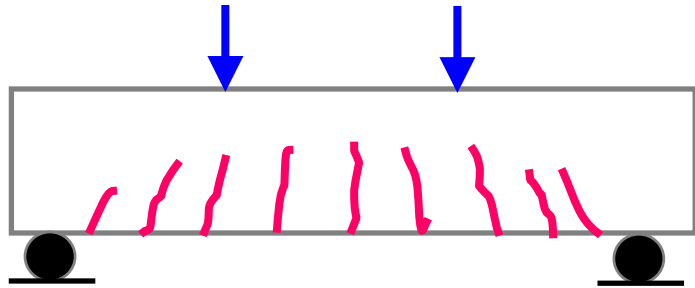
Diffusion of oxygen described by stationary state condition

$$q = D \frac{dC}{dx} \quad (\text{Fick's first law})$$

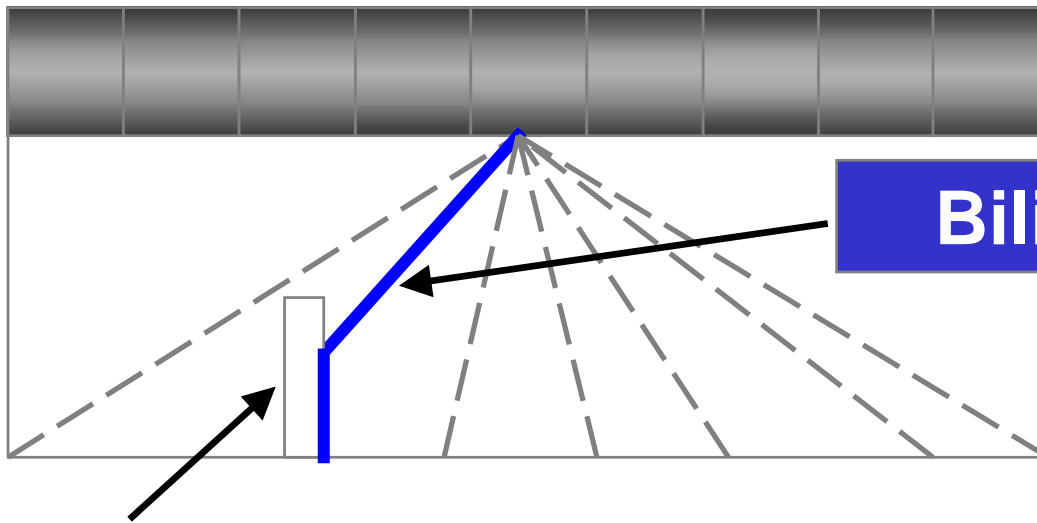
q : Flow rate of substance
 C: concentration of substance
 D: Diffusion coefficient



Cracked concrete Model



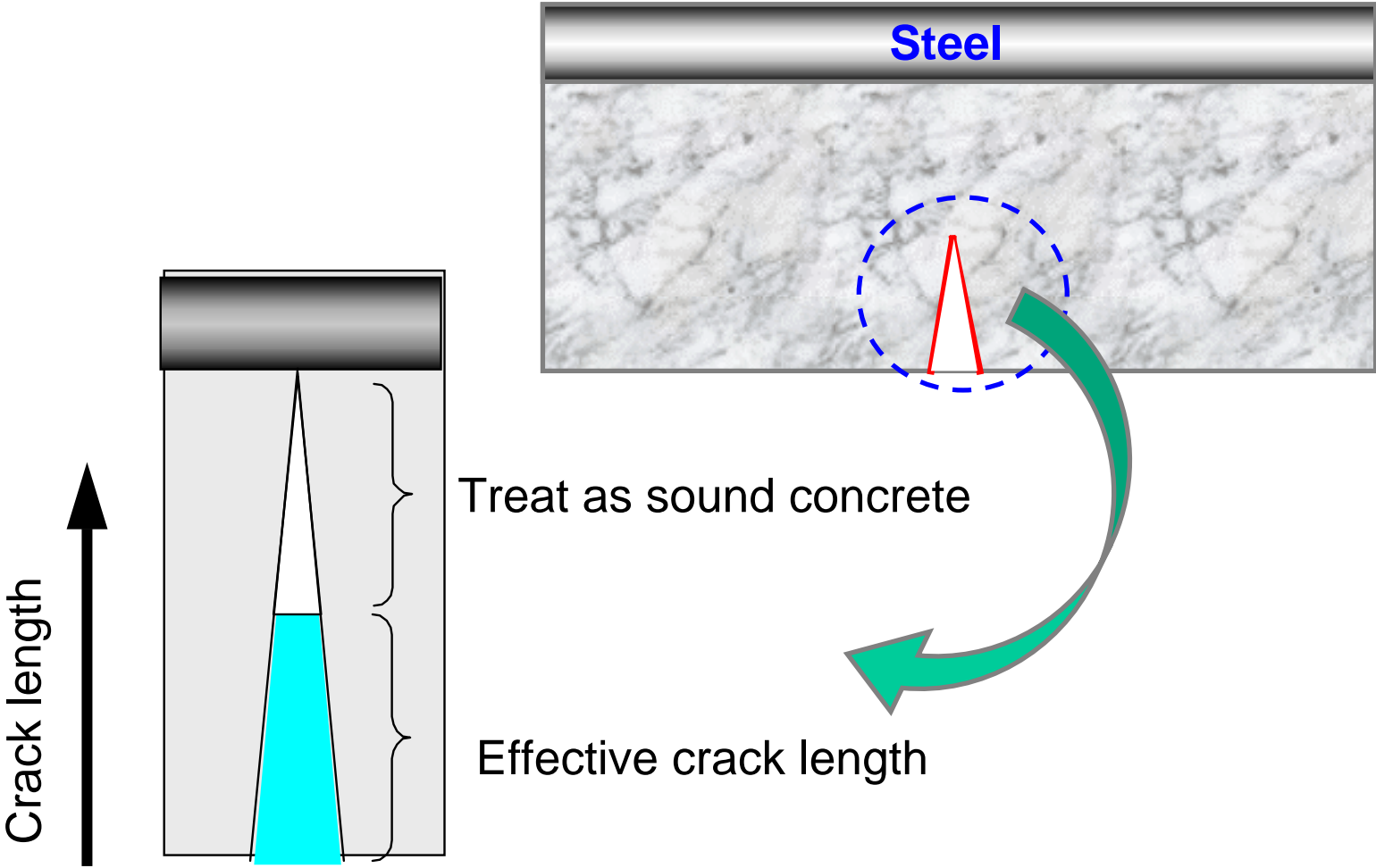
Cracks may exist by external loading, drying shrinkage etc..



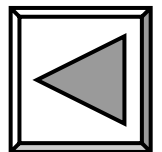
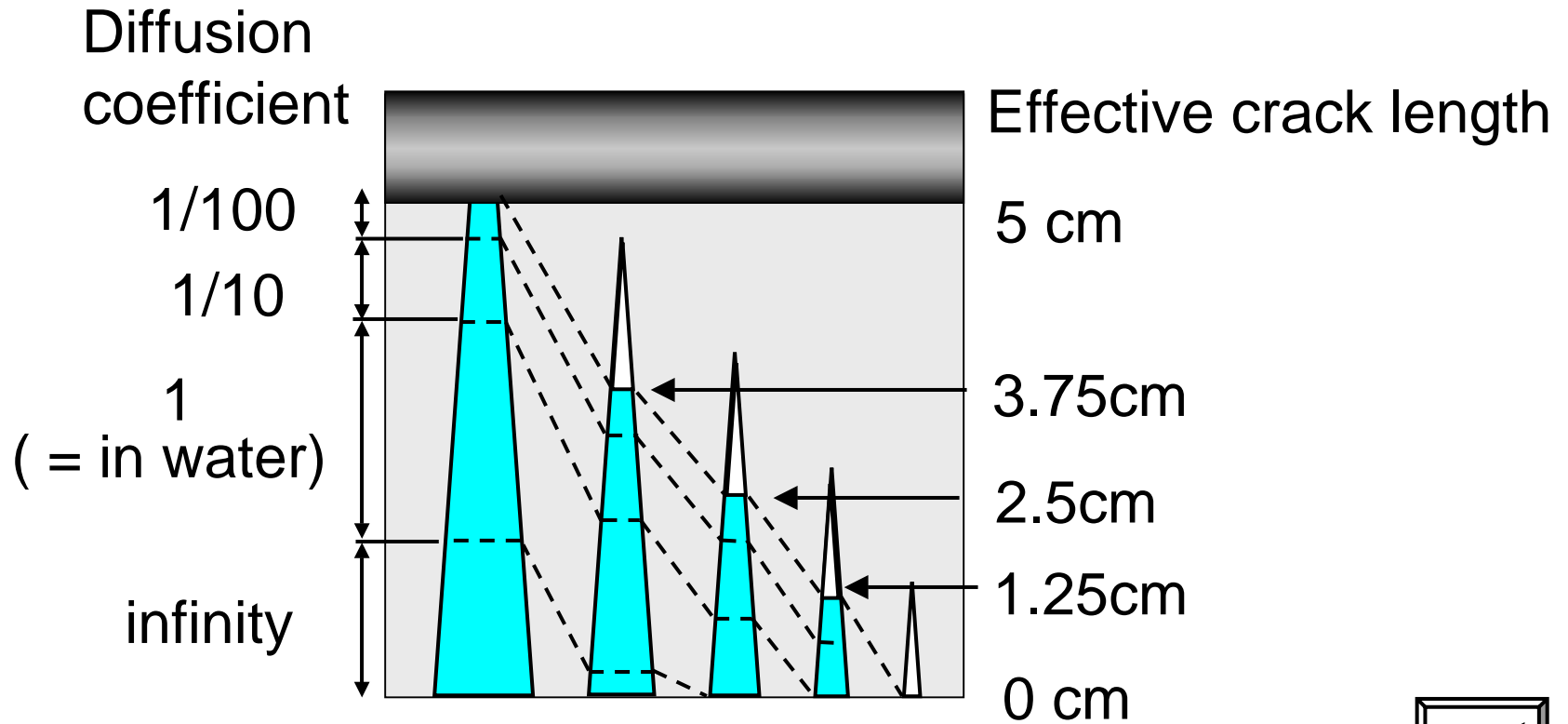
Bilinear route

Crack position

Definition of effective crack length



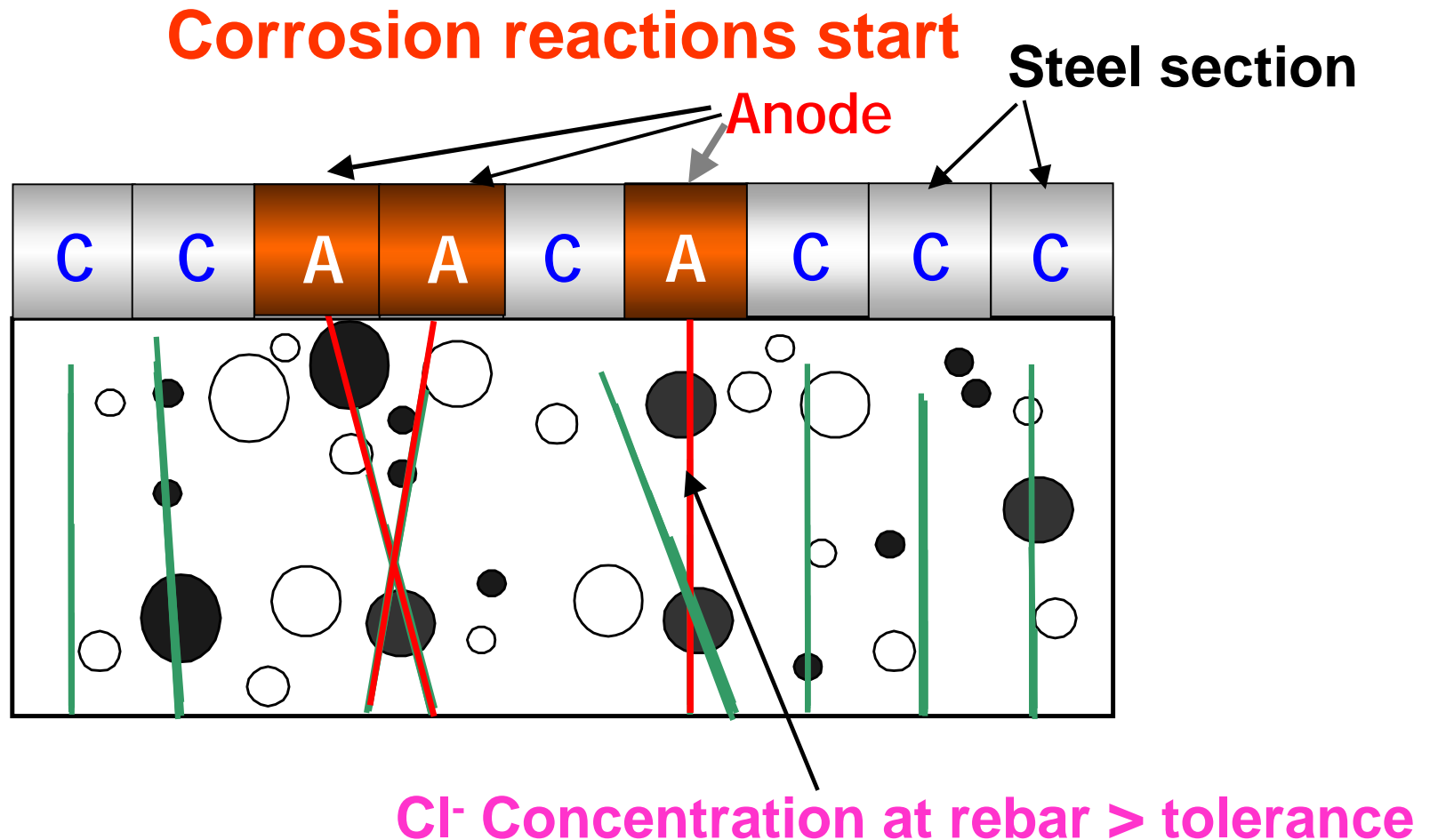
Relationship between effective crack and diffusion coefficient



Corrosion model

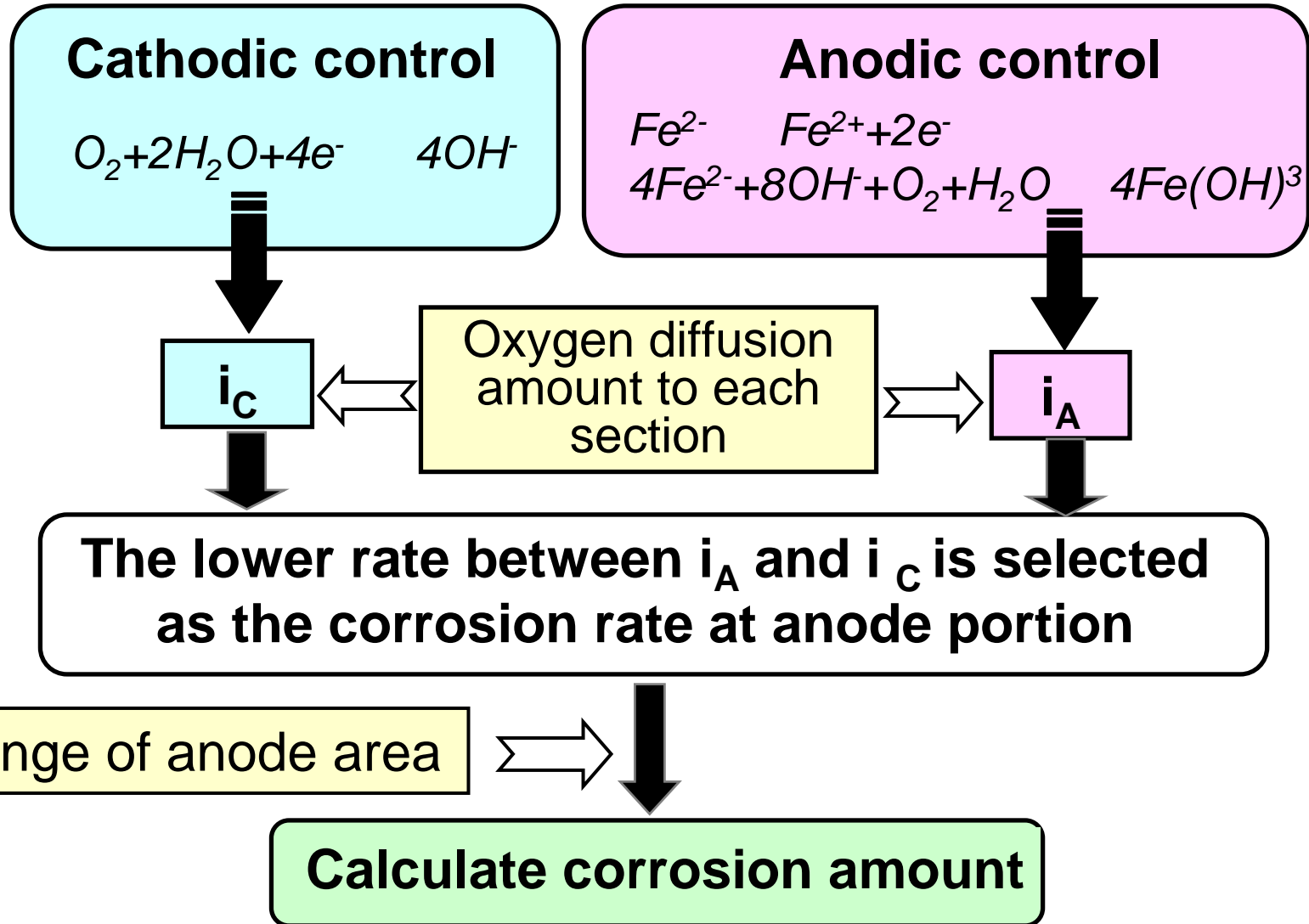
- based on macrocell corrosion theory-

Specification of Anode and Cathode area

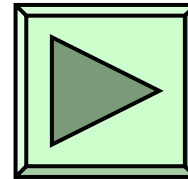
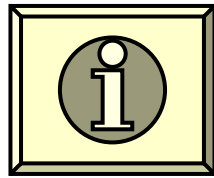


Corrosion model

Estimation of corrosion rate

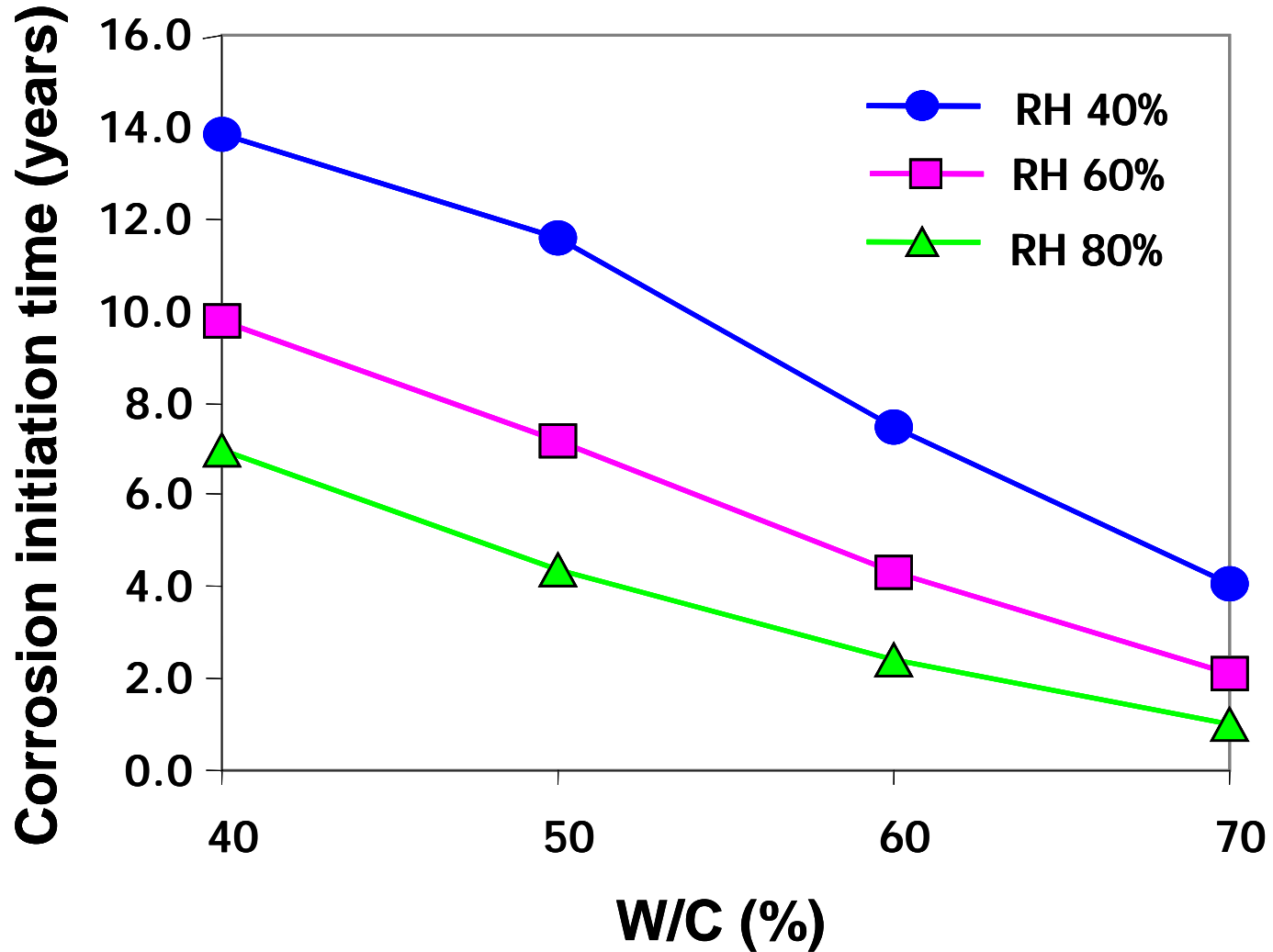


SIMULATION RESULTS



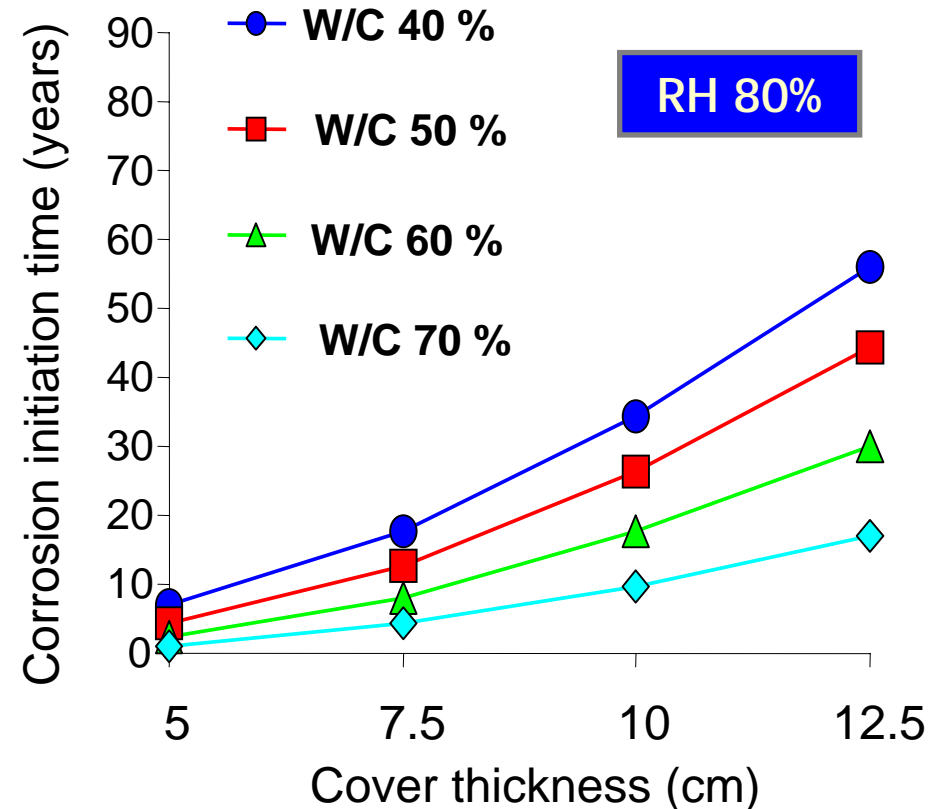
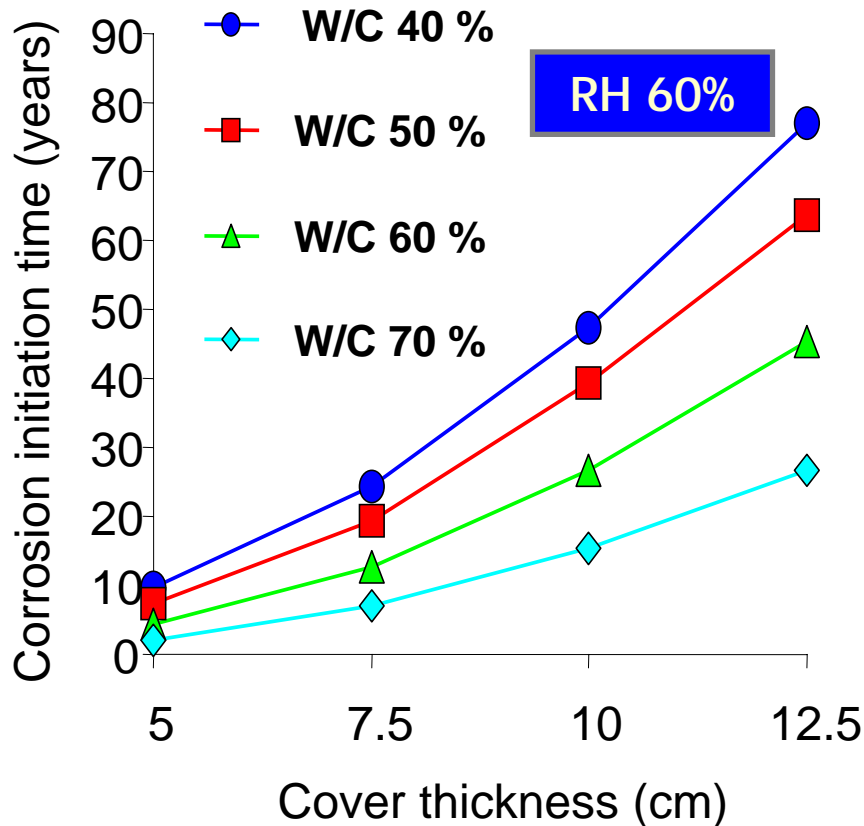
SIMULATION RESULTS

Corrosion initiation time



SIMULATION RESULTS

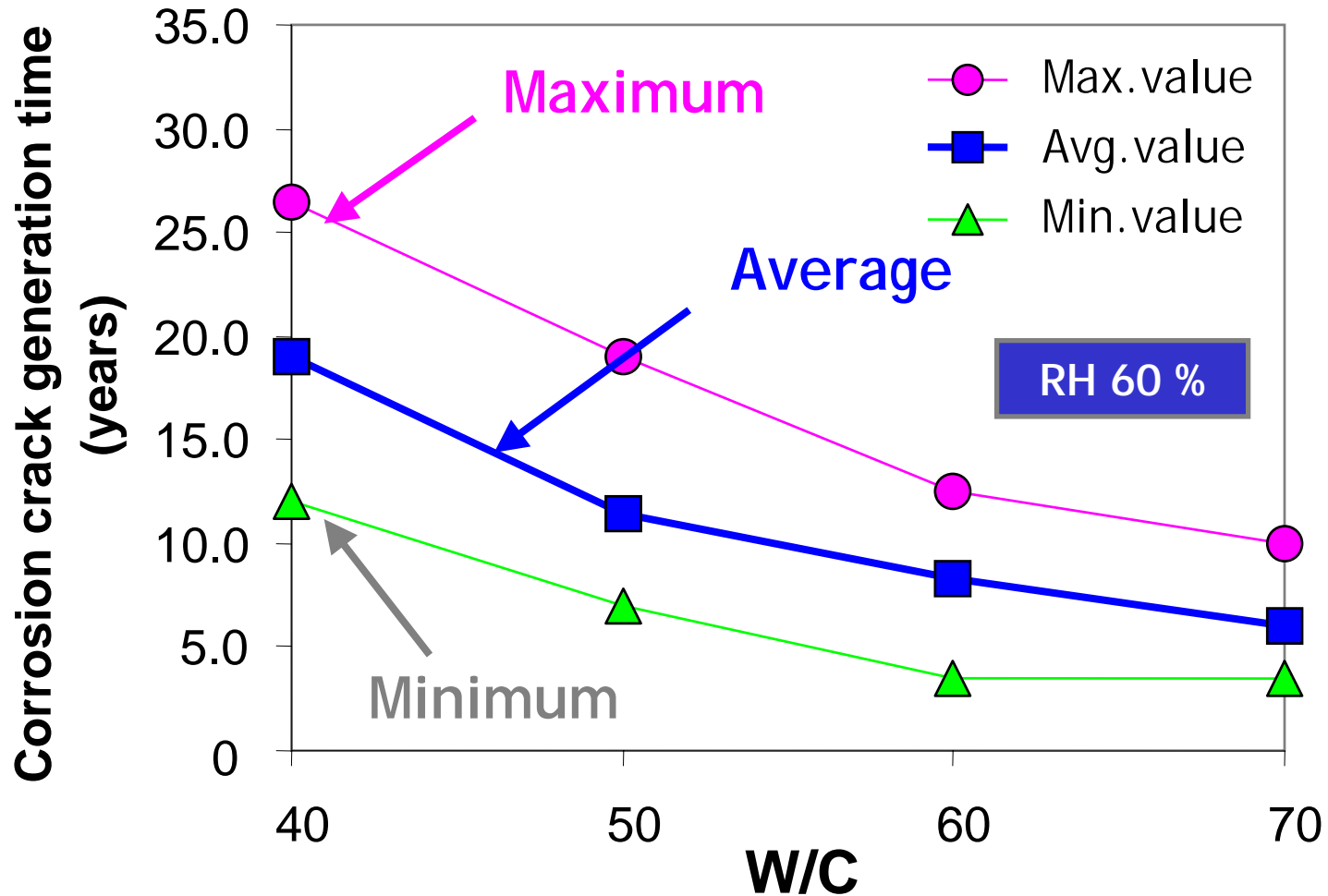
Corrosion initiation time



- ✚ the larger the cover thickness, lifetime increases clearly.
- ✚ Relative humidity is also influential parameter.

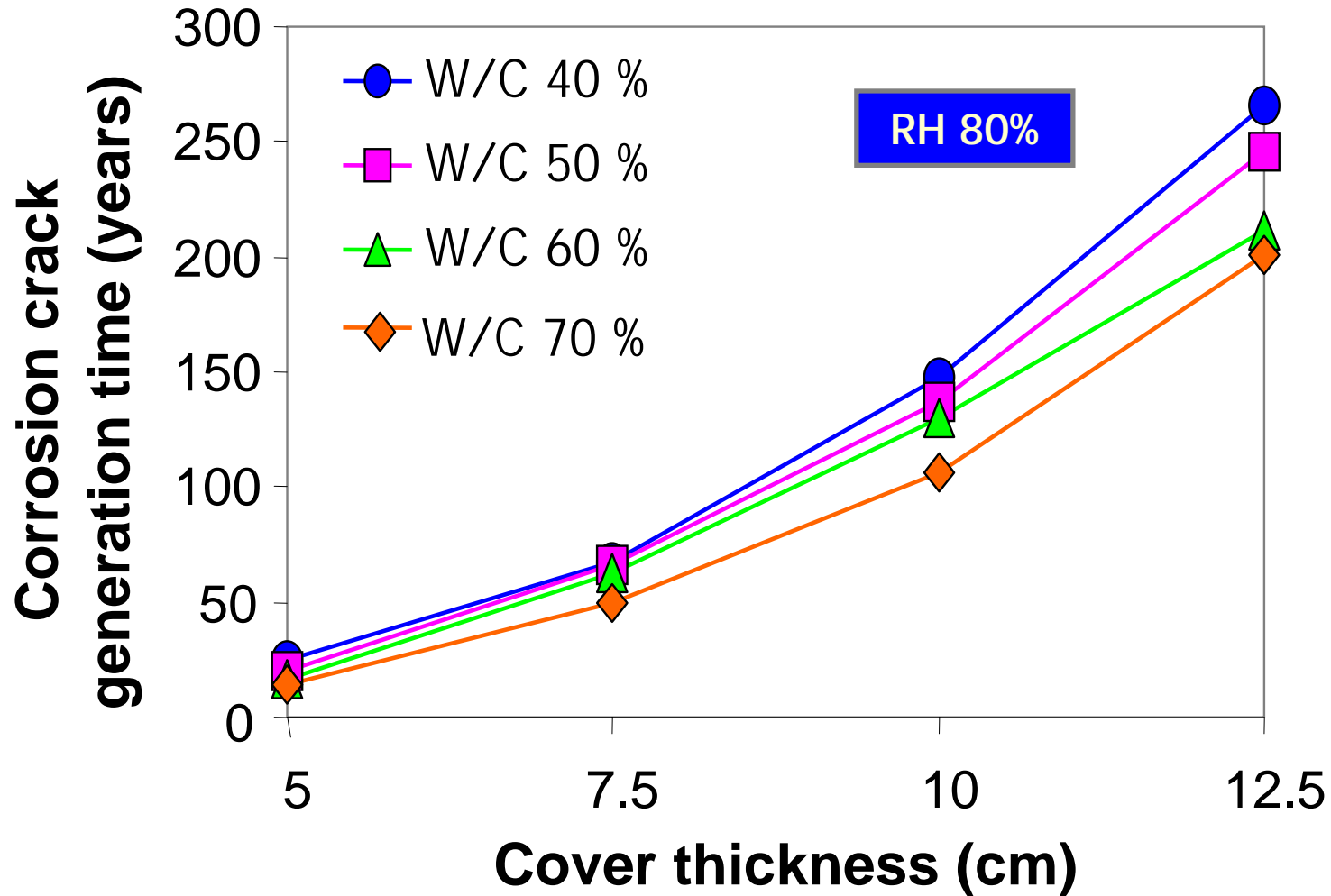
SIMULATION RESULTS

Corrosion crack generation time

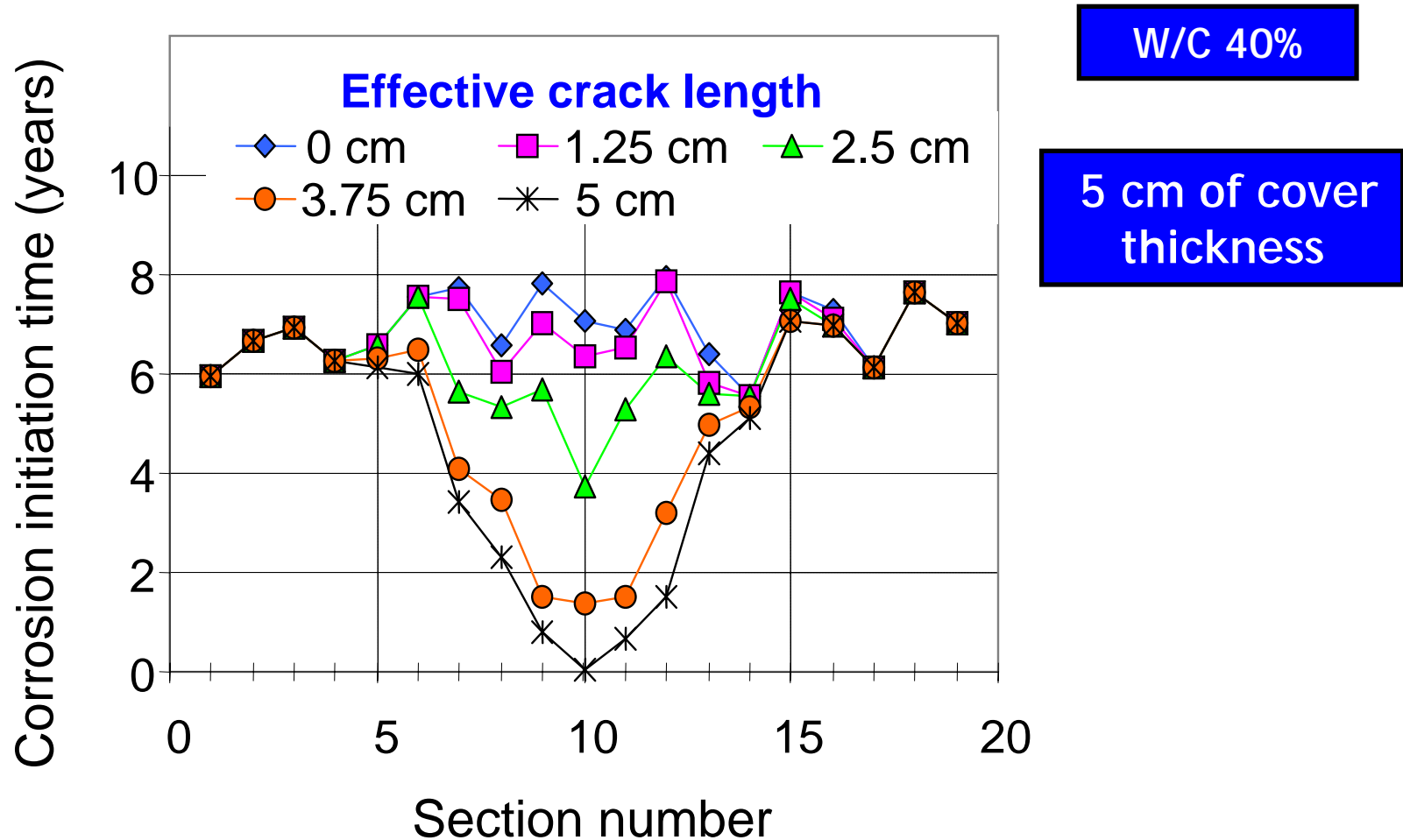


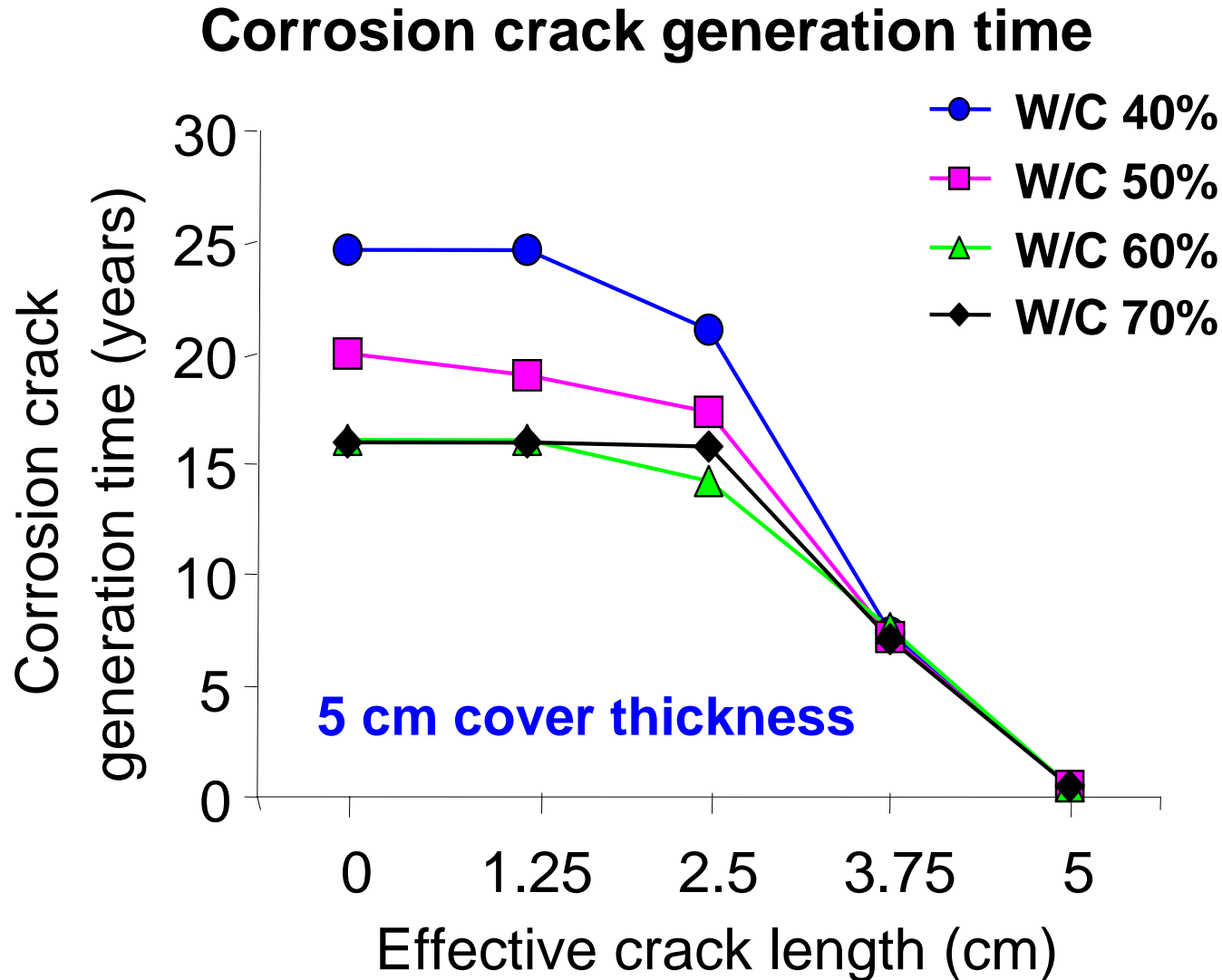
SIMULATION RESULTS

Corrosion crack generation time

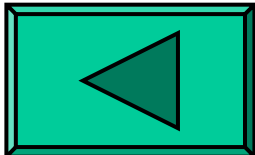


Corrosion initiation time





Example for evaluation of structural performance of deteriorated RC structure



**DYNAMIC BEHAVIOR OF REINFORCED
CONCRETE STRUCTURES DETERIORATED BY
CORROSION OF REINFORCEMENT**

Introduction

- some structures in the severe environmental condition may be in a deteriorated condition due to the corrosion of reinforcement
- piers are relatively vulnerable to earthquake because it is suffered with a very large inertial force

Introduction

Corrosion of
Reinforcement

Large
Earthquake

Some pier with corrosion of reinforcement may not have the structural capacities it was designed for

Rehabilitation and
Repairing is being
popular

Evaluation of the dynamic behavior of the piers deteriorated by corrosion becomes necessary

Introduction

Objective

- Evaluate the dynamic properties such as, **stiffness, ductility** and **energy absorption** of the piers deteriorated by the corrosion of reinforcement
- Behavior of the corroded piers against the cyclic loading which are designed by
 - Ordinary design, using JSCE code.
 - Seismic design part of JSCE along with the verification of ductility according to JRA's specification

Methodology

Specimen Type

S. No.	Designation	Design Principle	Axial Load	Corrosion Loss gm/cm ² /cm
1	POA-1	Using JSCE code for ordinary reinforced concrete design	200 kN	0.00
2	POA-2			0.19
3	POA-3			0.38
4	POA-4			0.56
5	PON-1		0	0.00
6	PON-2			0.19
7	PON-3			0.38
8	PON-4			0.56

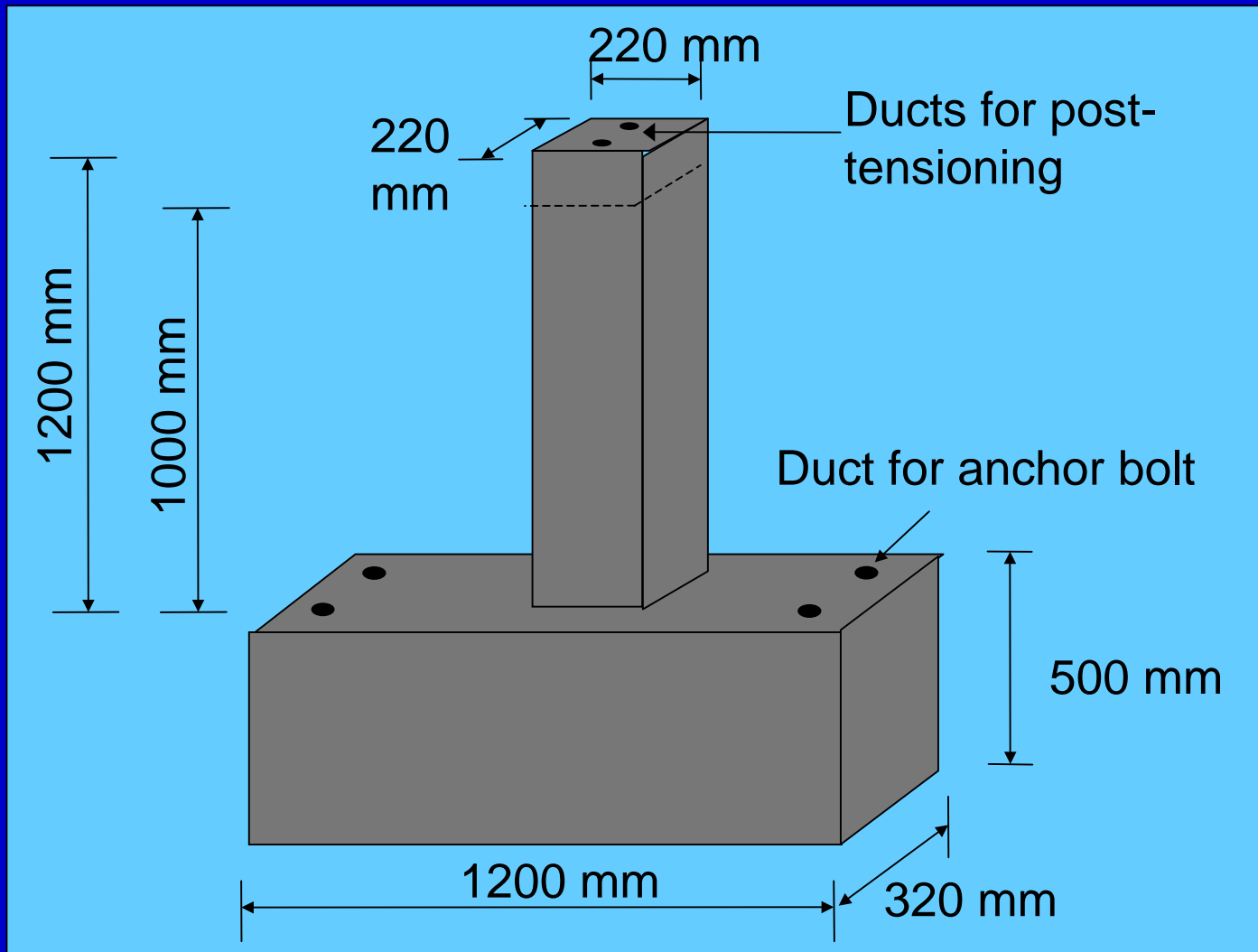
Methodology

Specimen Type (Contd..)

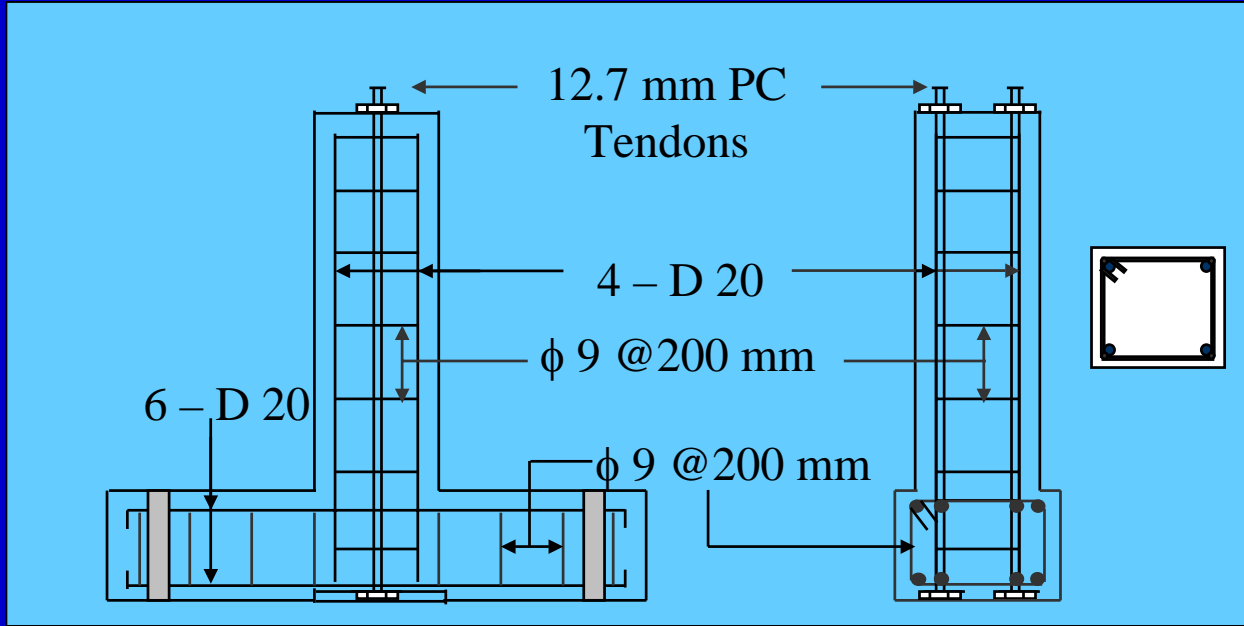
S. No.	Designation	Design Principle	Axial Load	Corrosion Loss gm/cm ² /cm
9	PEA-1	Using seismic resistant part of JSCE code in conjunction with JRA's specification	200 kN	0.00
10	PEA-2			0.19
11	PEA-3			0.38
12	PEA-4			0.56
13	PEN-1		0	0.00
14	PEN-2			0.19
15	PEN-3			0.38
16	PEN-4			0.56

Methodology

Specimen Size

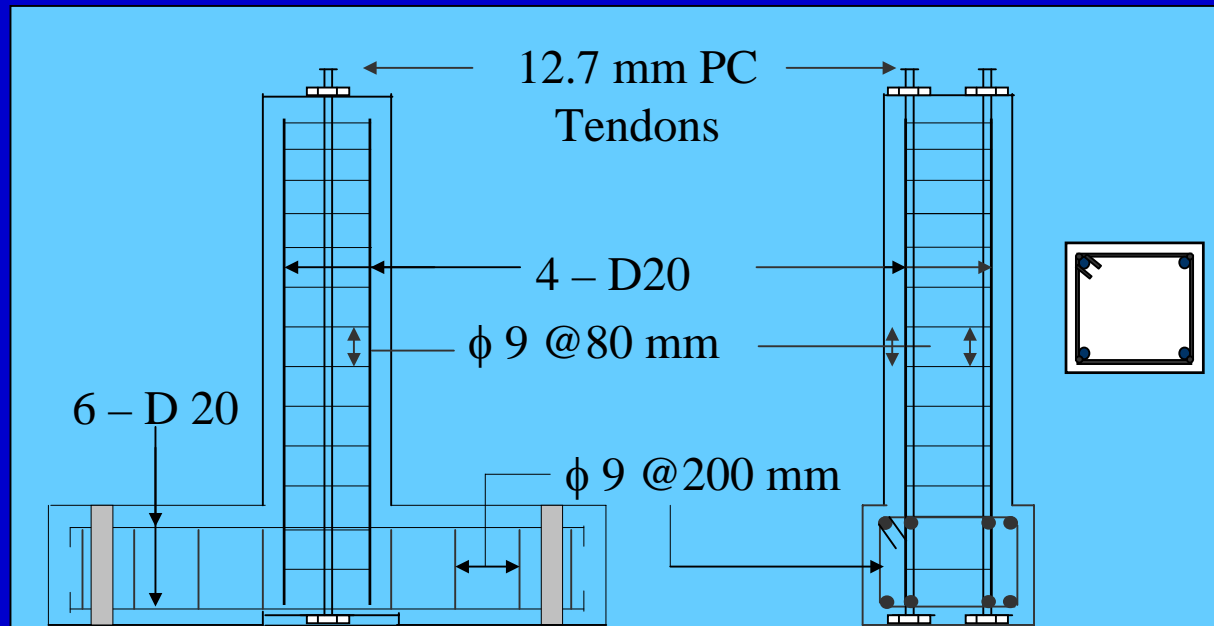


Reinforcement Arrangement

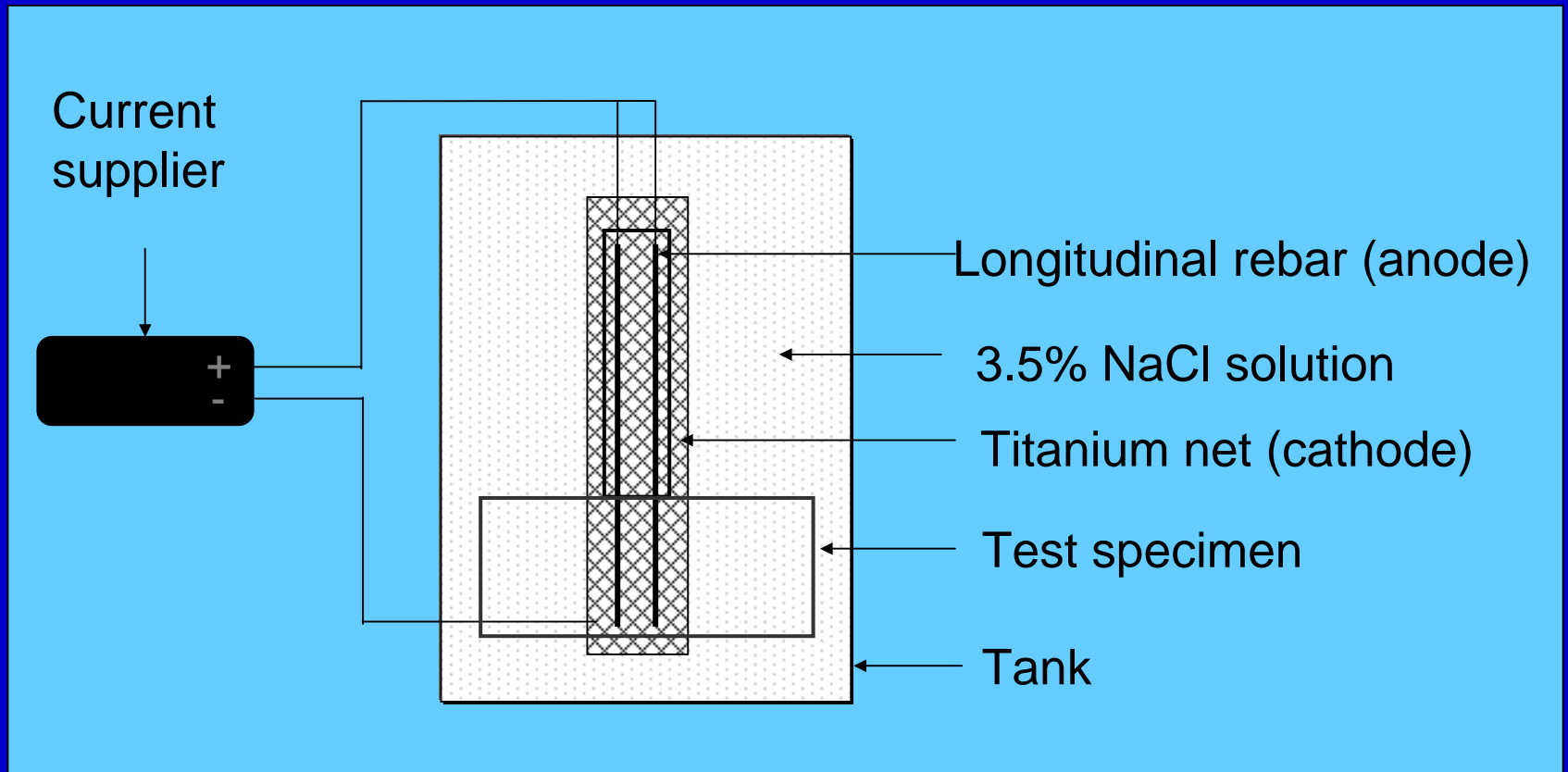


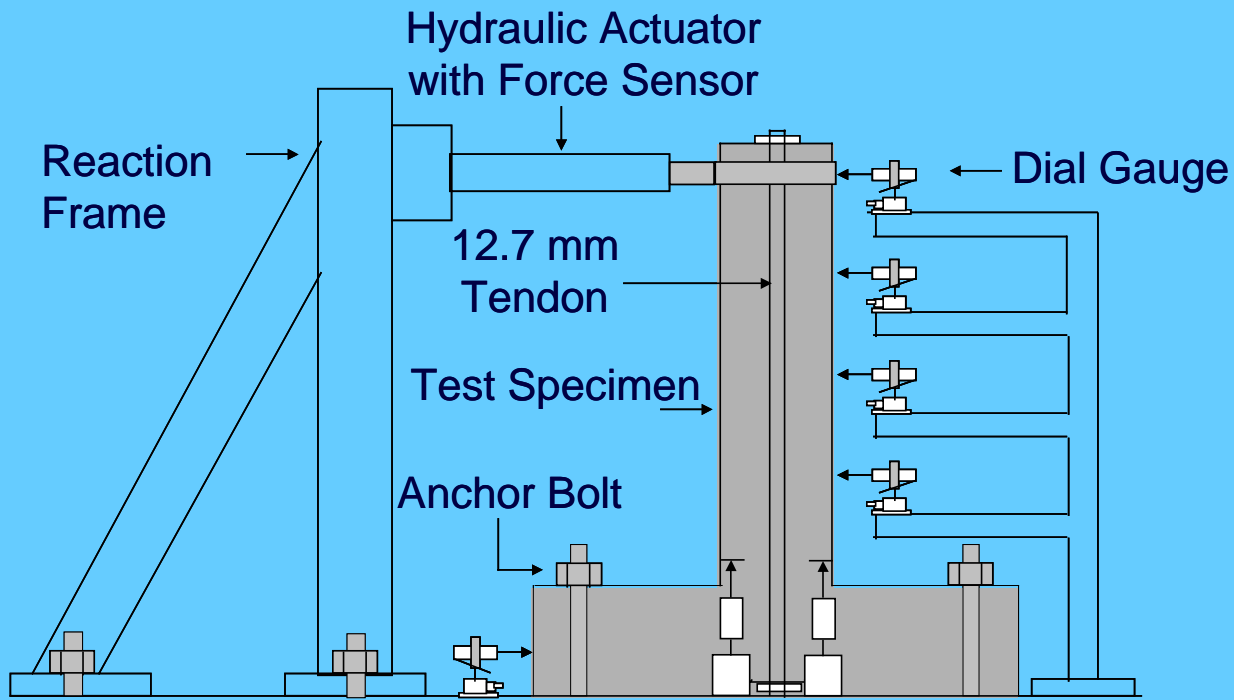
Ordinary Design

Seismic Design

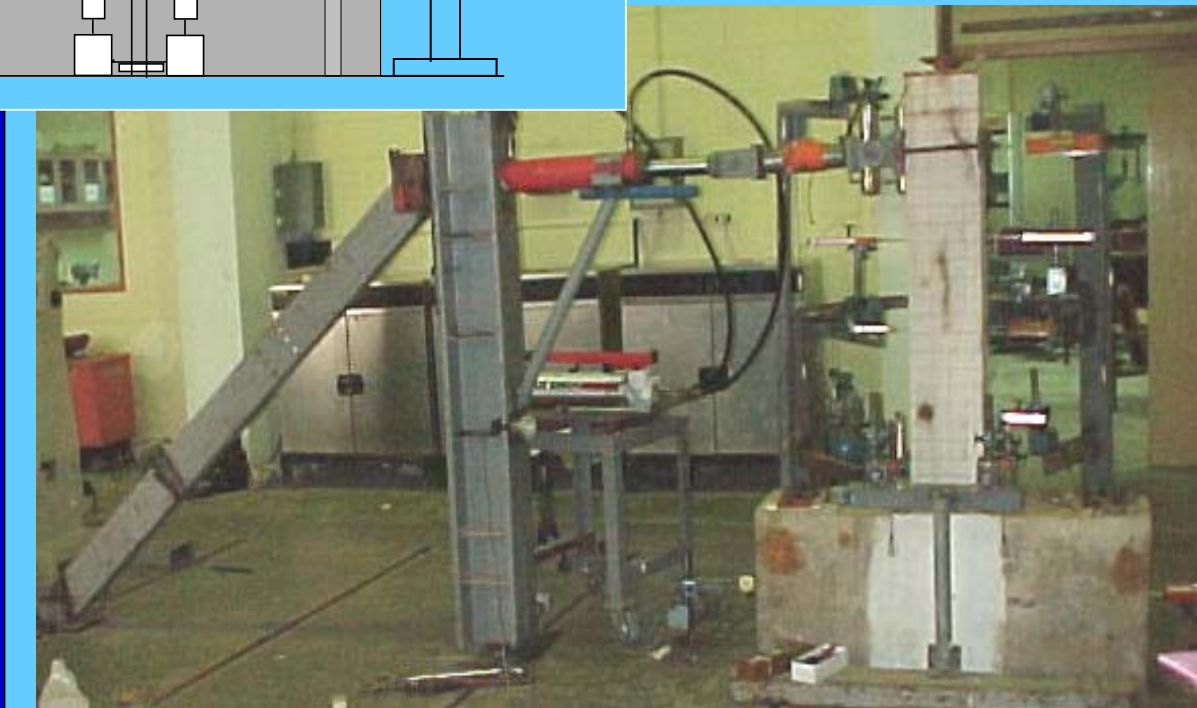


Accelerated Corrosion Test

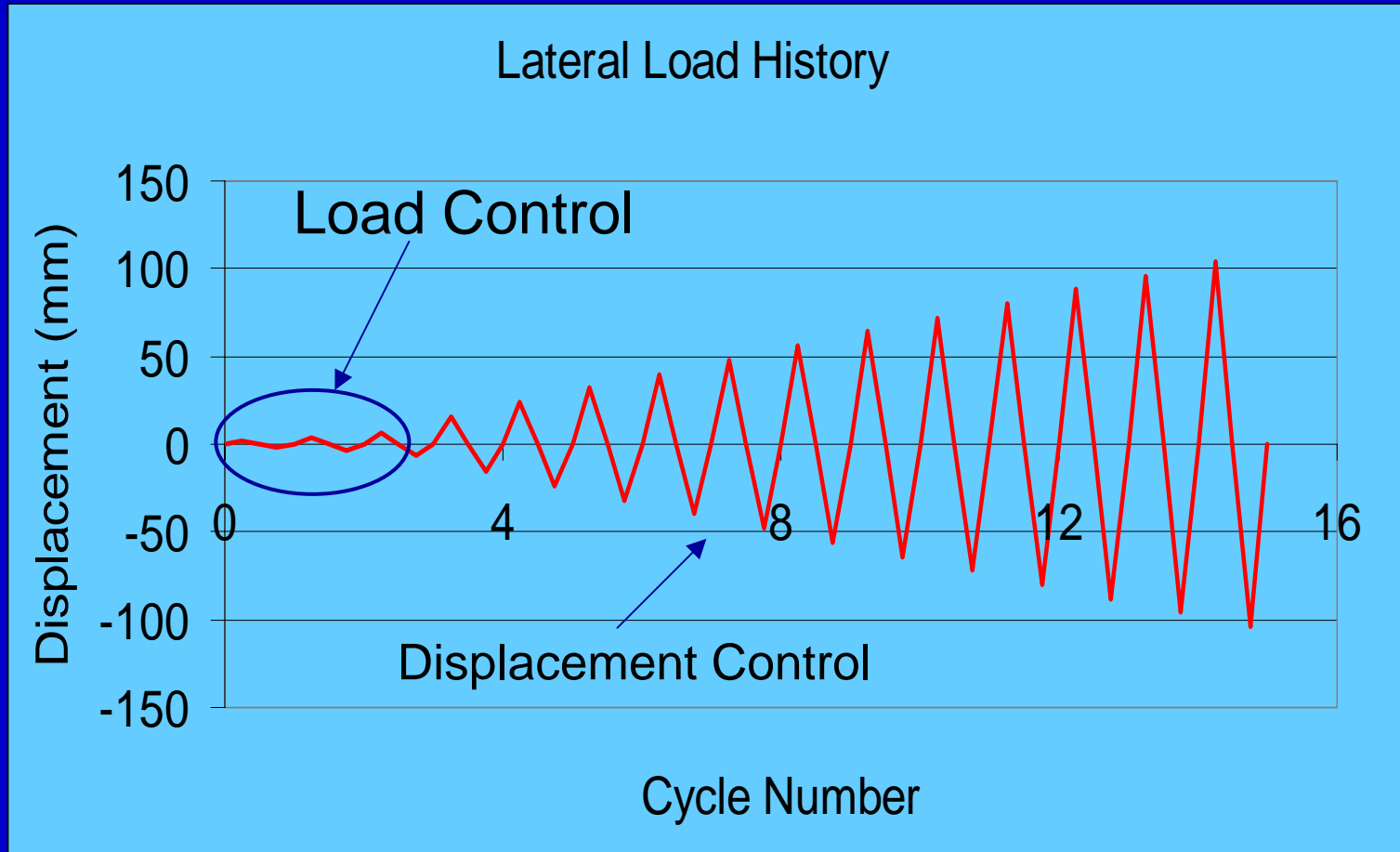




**Loading
Test
Condition**

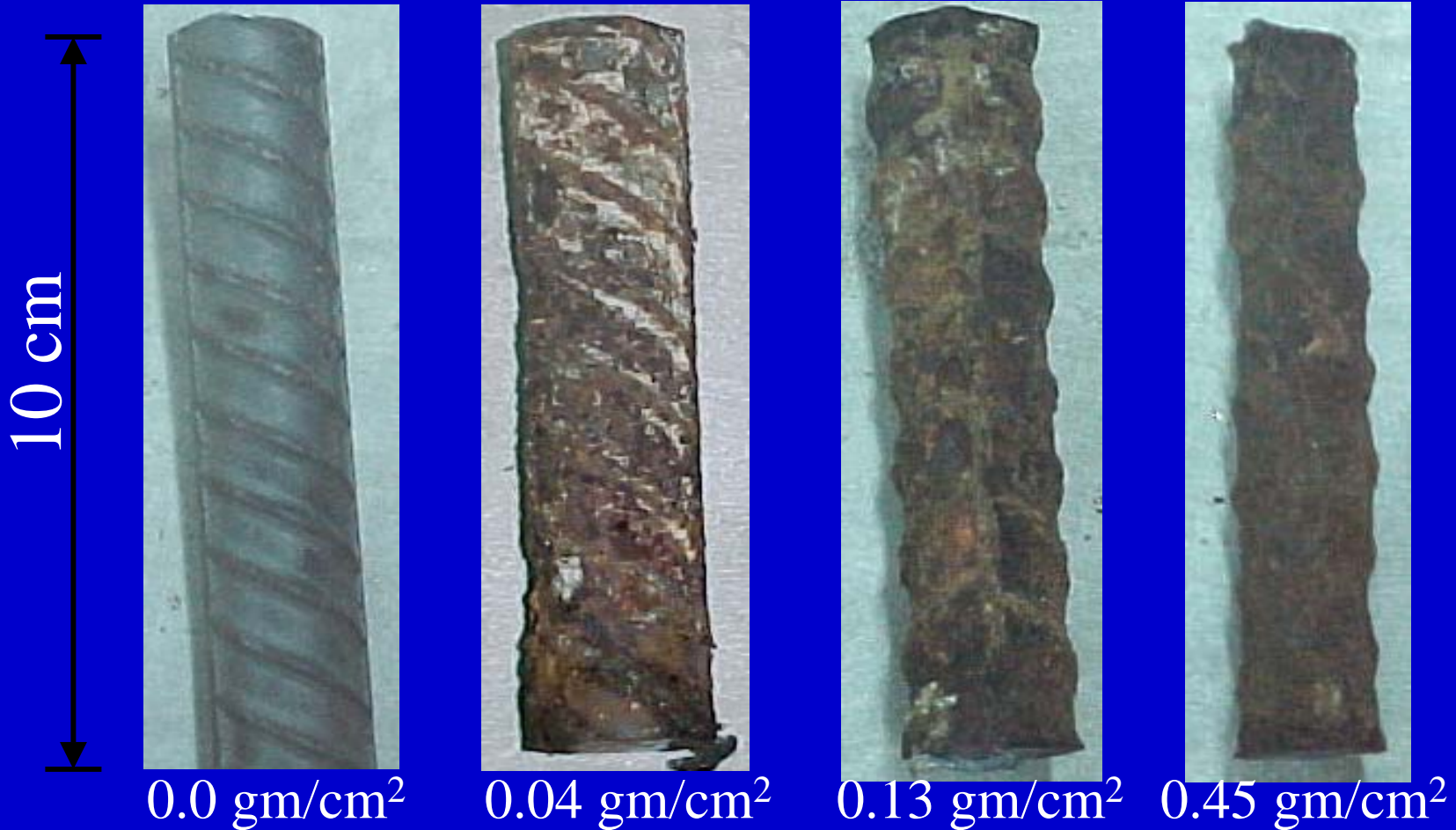


Loading Cycles



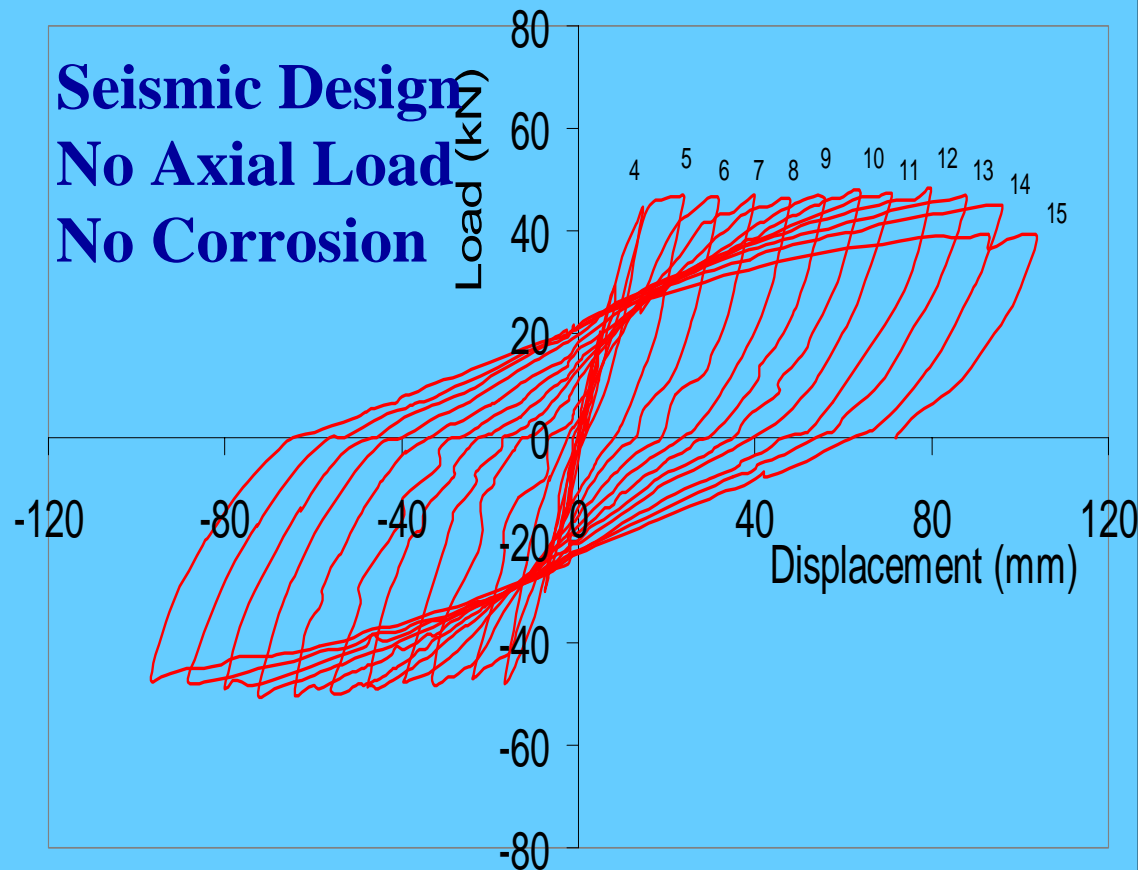
Methodology

Comparison of Various Corrosion Loss



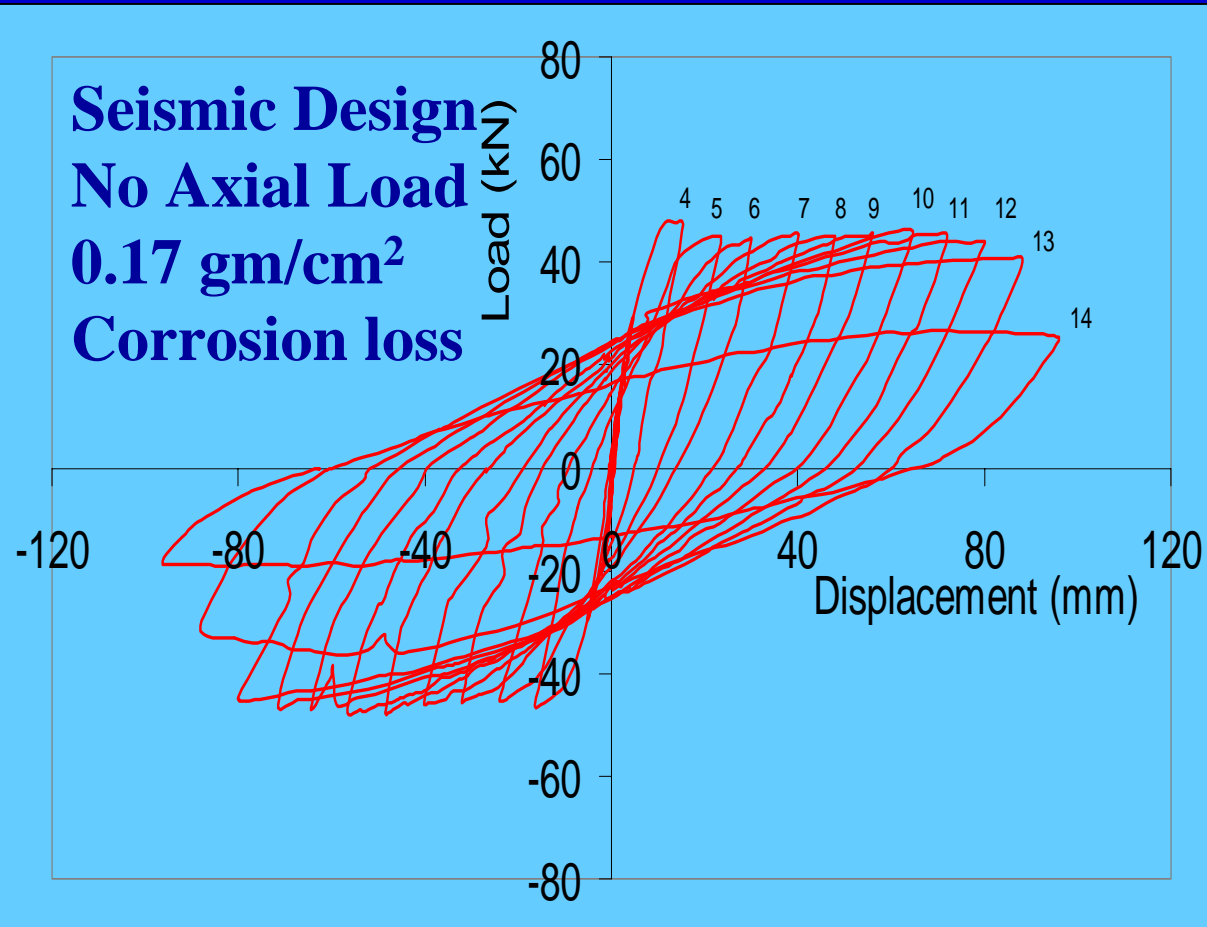
Results and Discussion

Load Displacement Curve



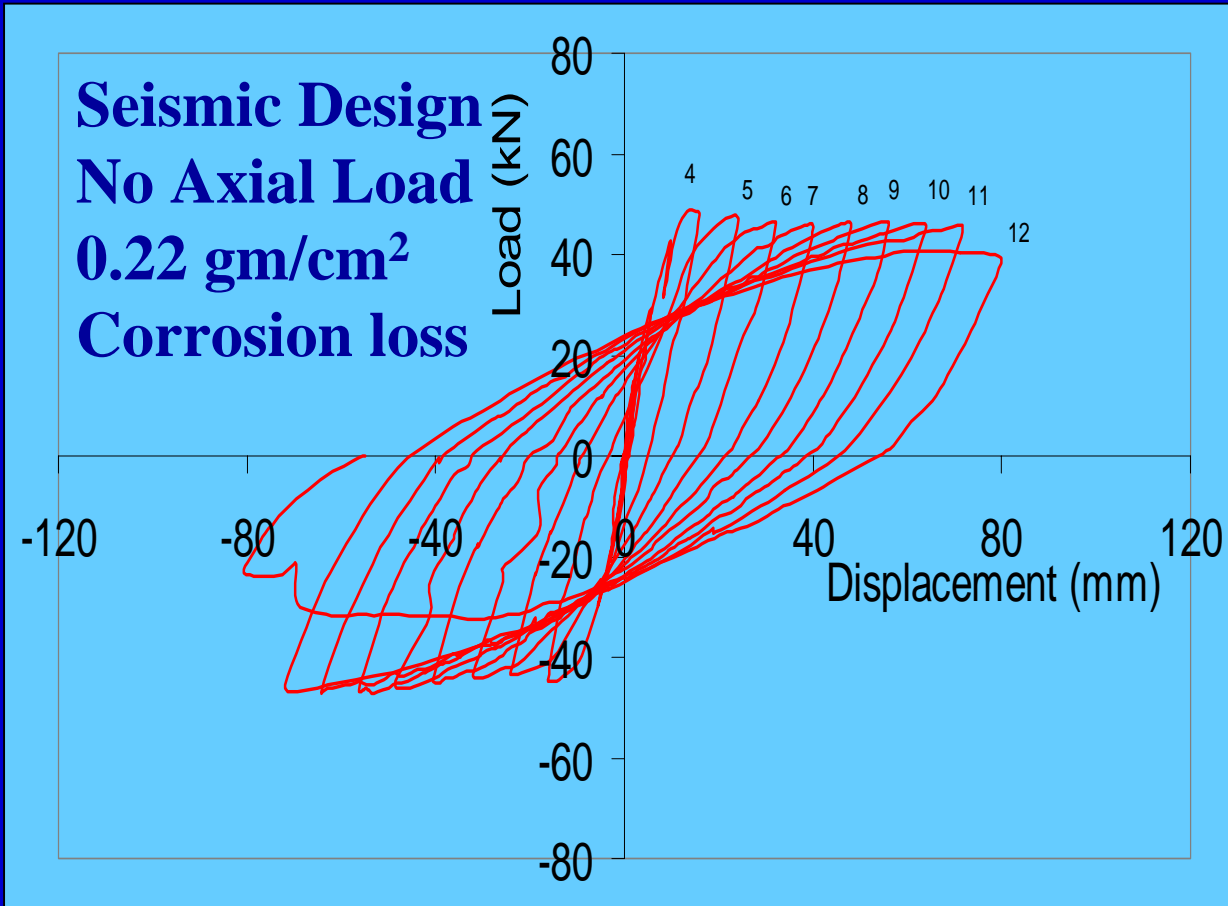
Results and Discussion

Load Displacement Curve



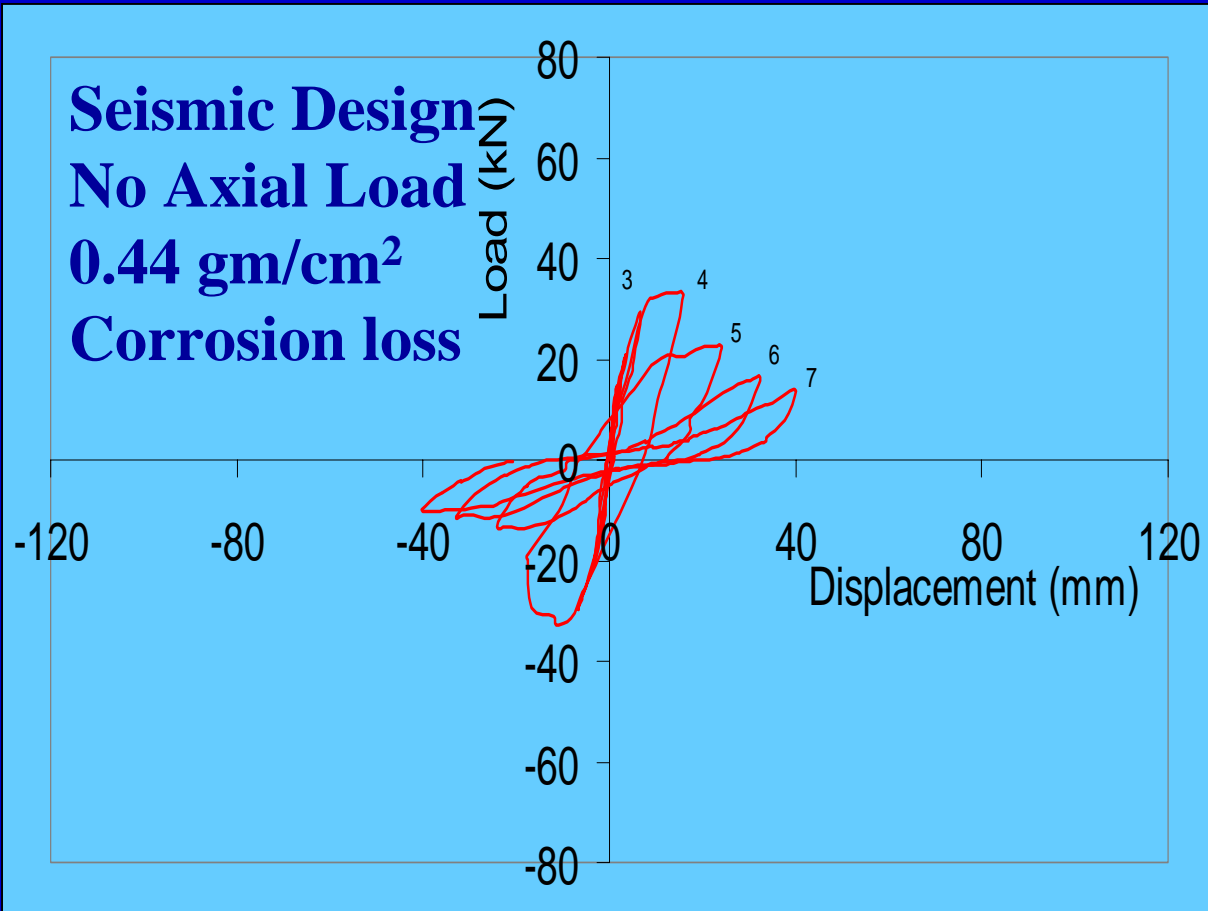
Results and Discussion

Load Displacement Curve



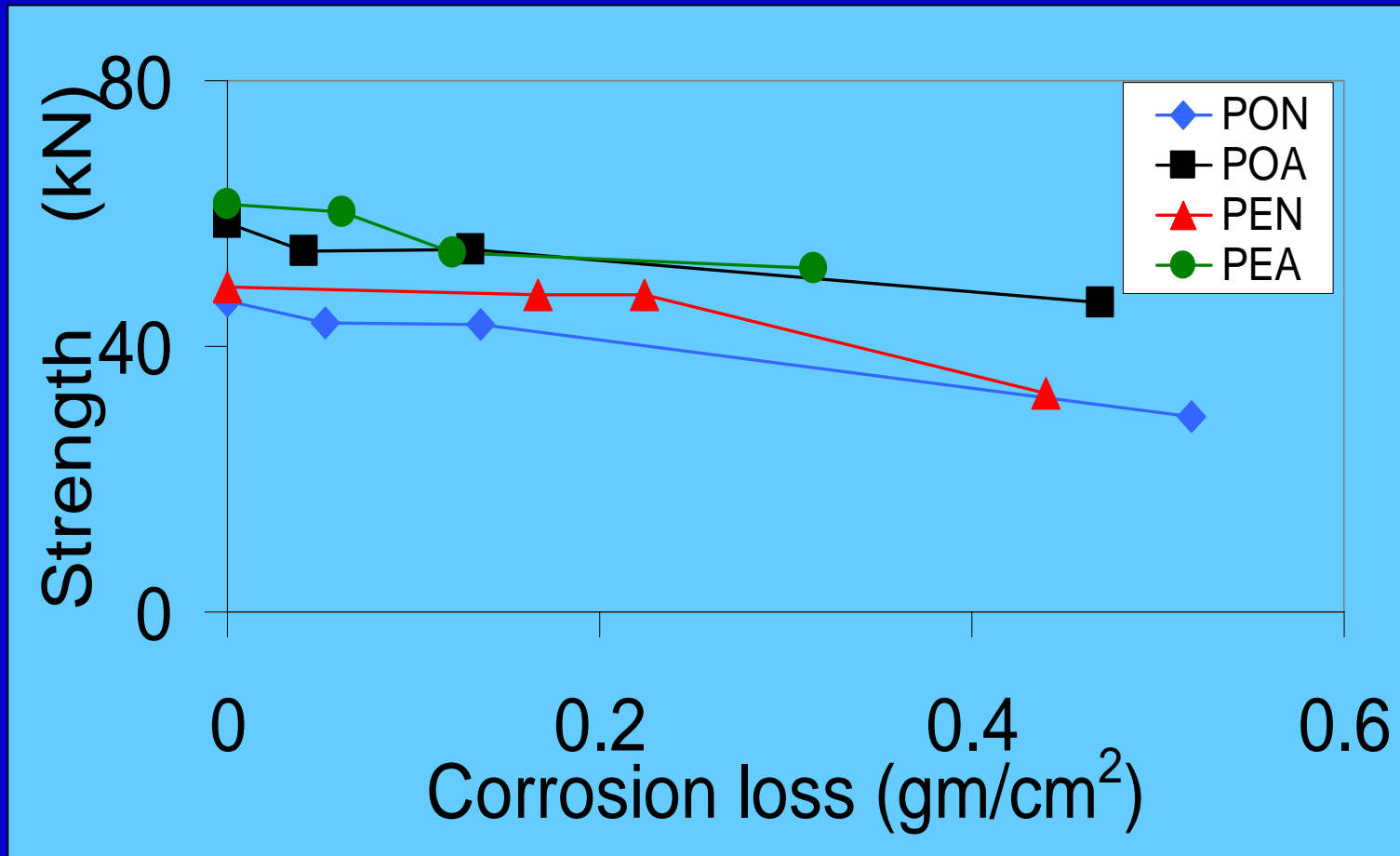
Results and Discussion

Load Displacement Curve



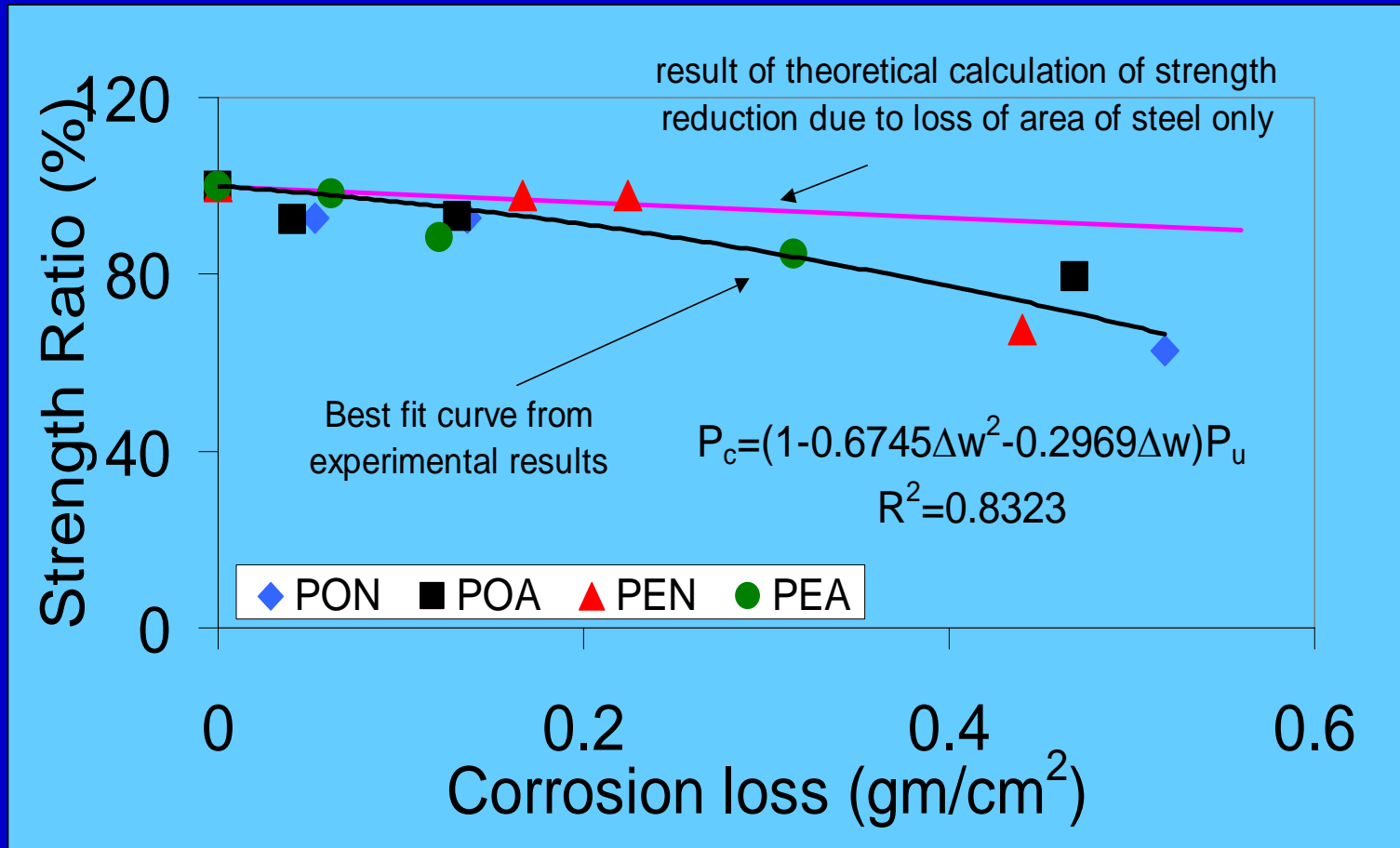
Results and Discussion

Strength Degradation



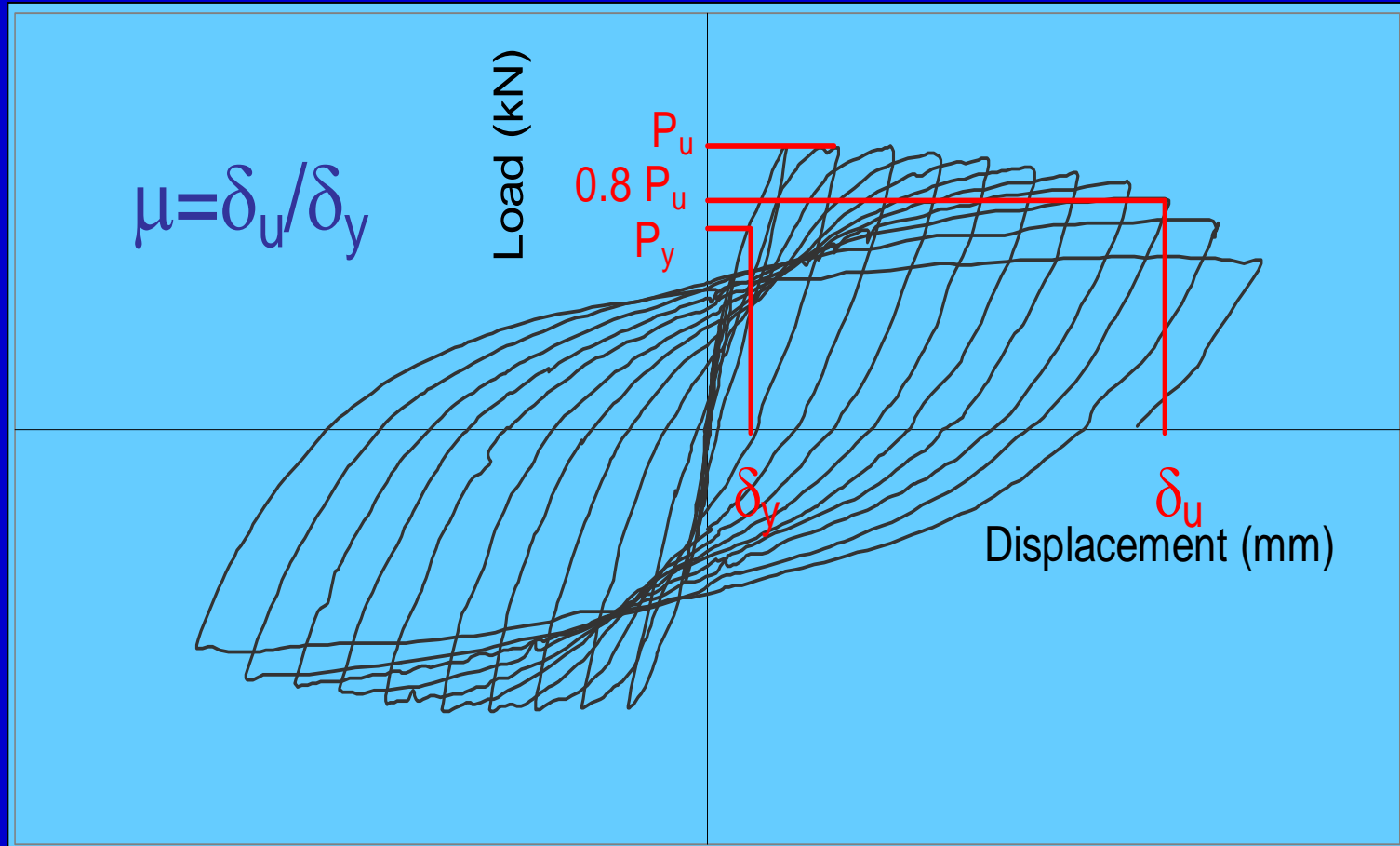
Results and Discussion

Strength Degradation (Contd...)



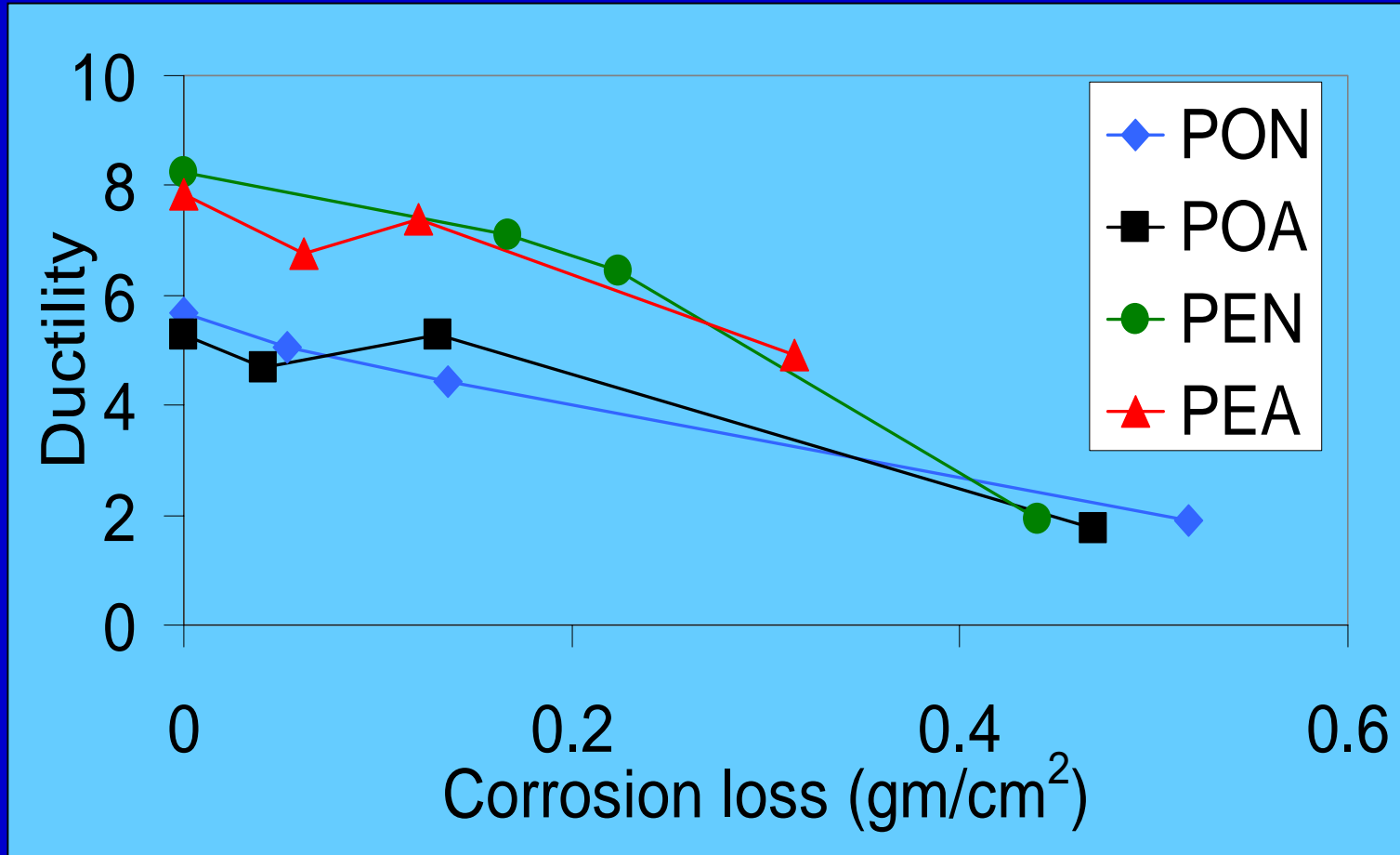
Results and Discussion

Ductility Degradation



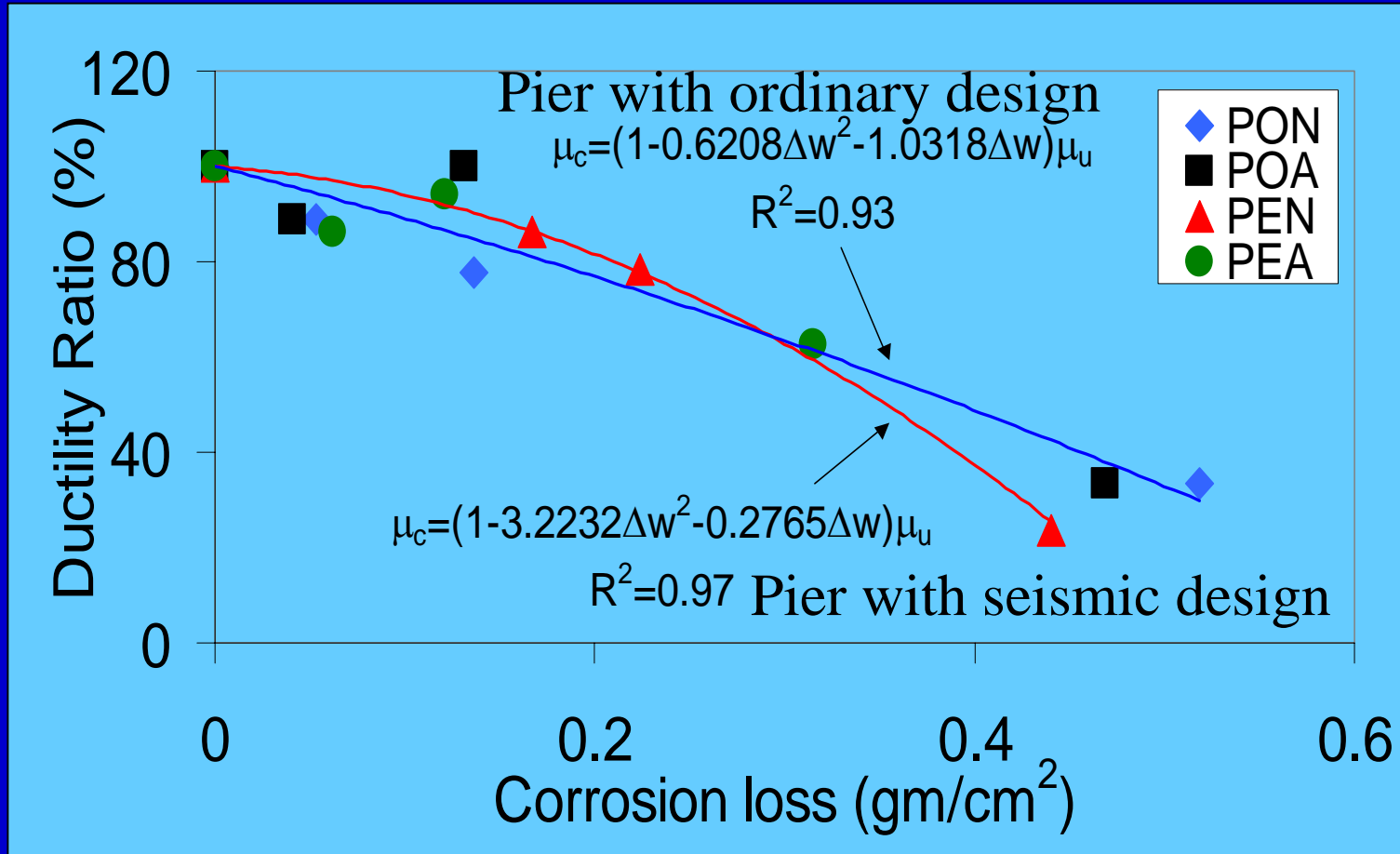
Results and Discussion

Ductility Degradation (Contd...)



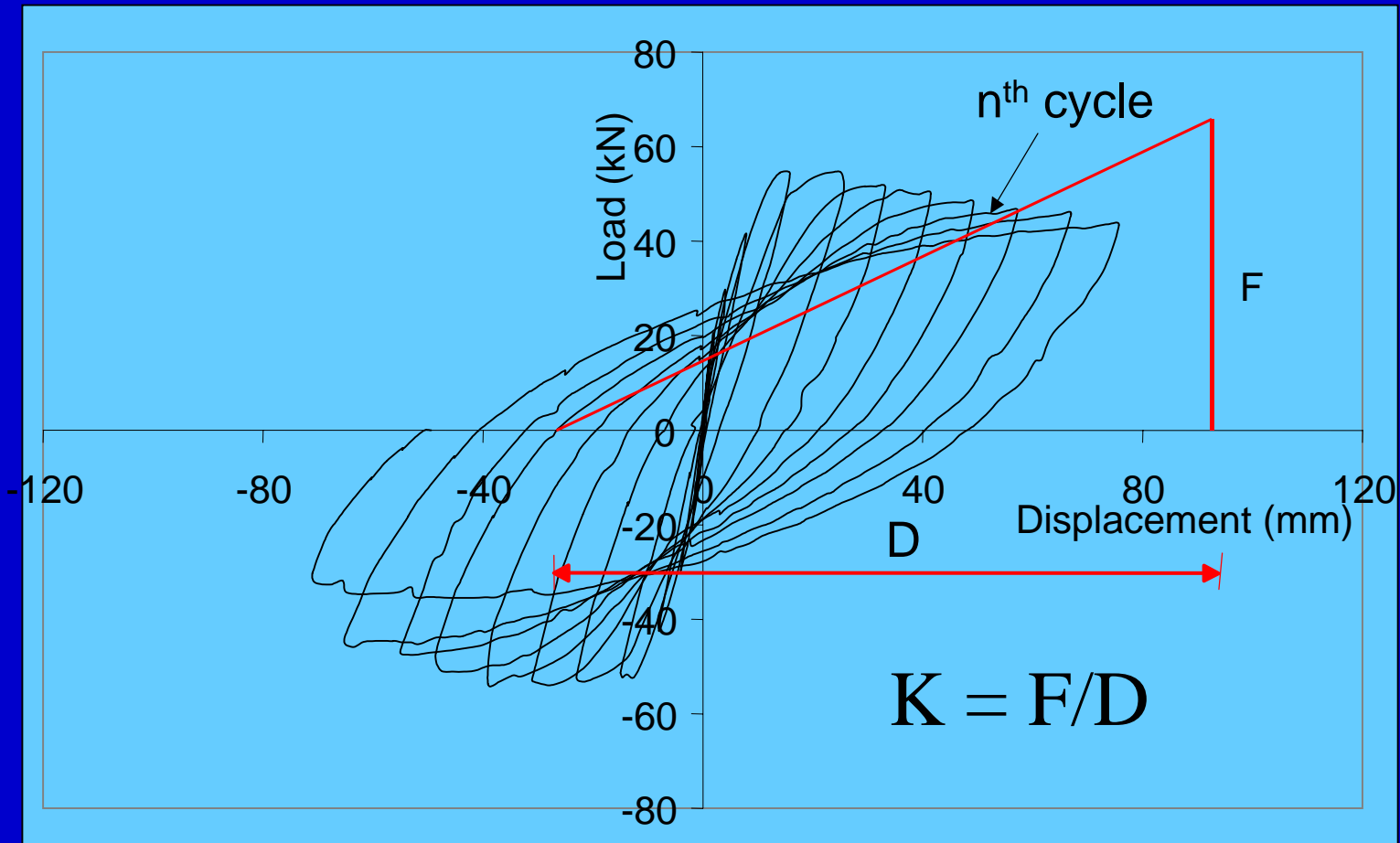
Results and Discussion

Ductility Degradation (Contd...)



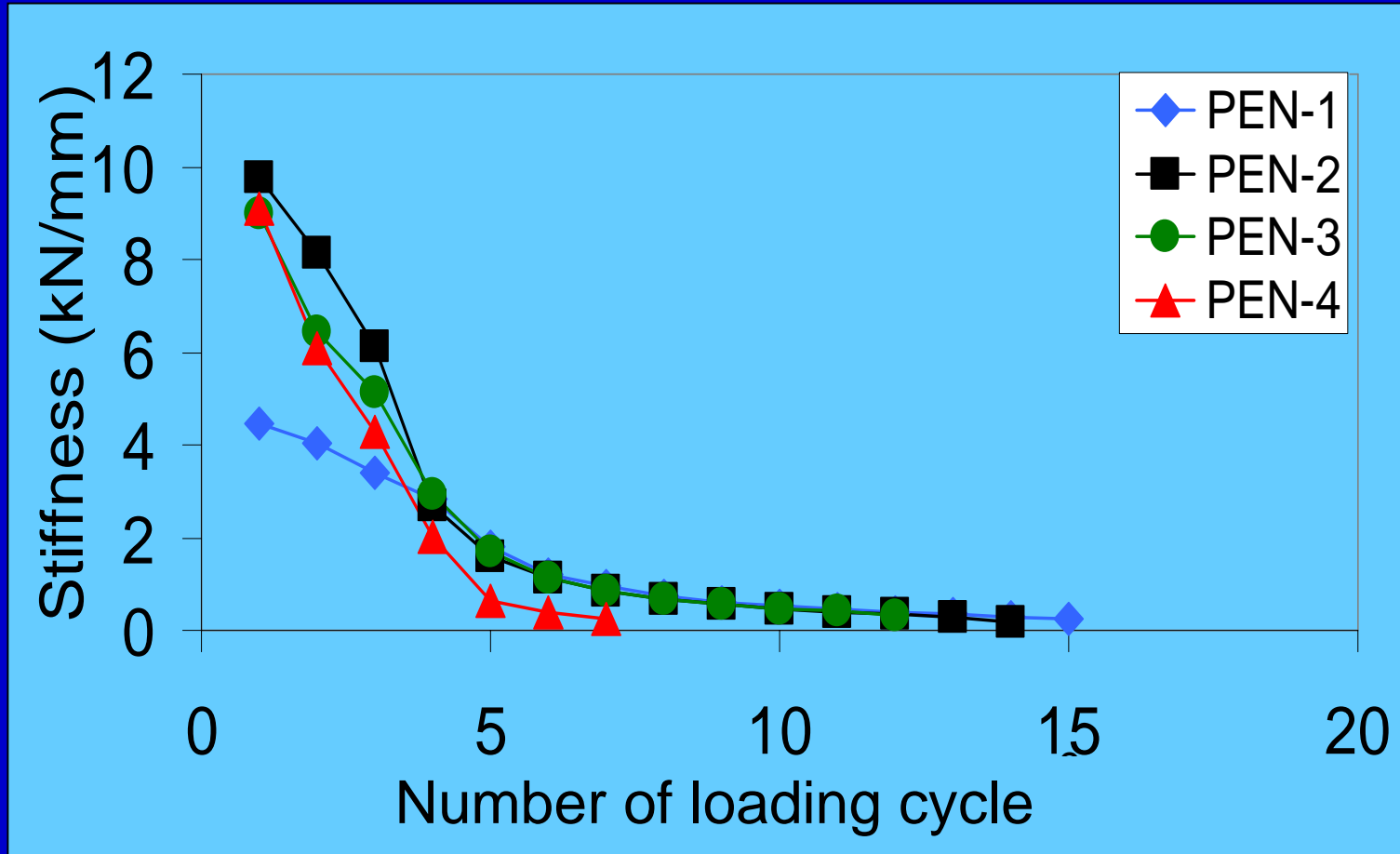
Results and Discussion

Stiffness Degradation



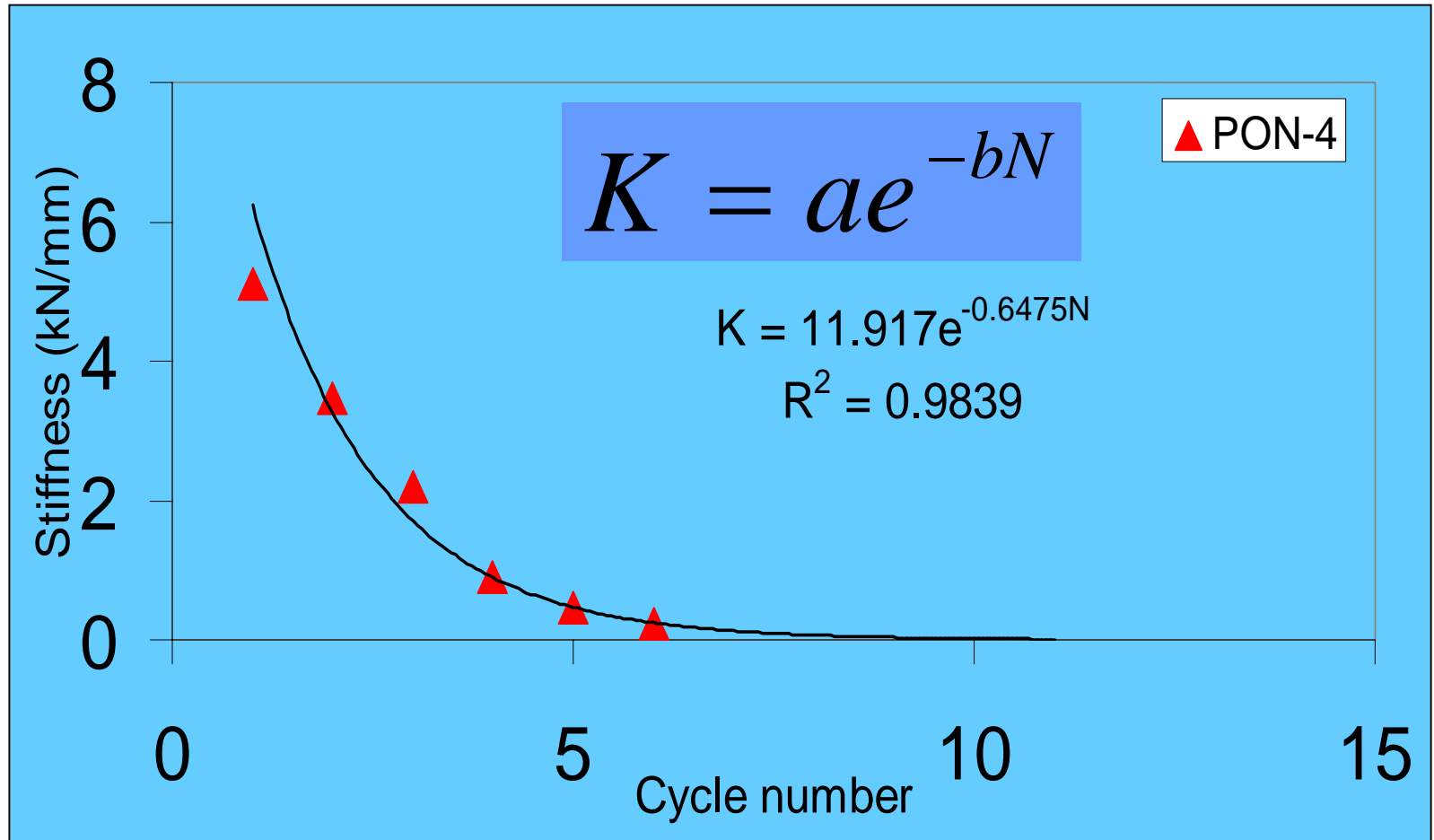
Results and Discussion

Stiffness Degradation (Contd)



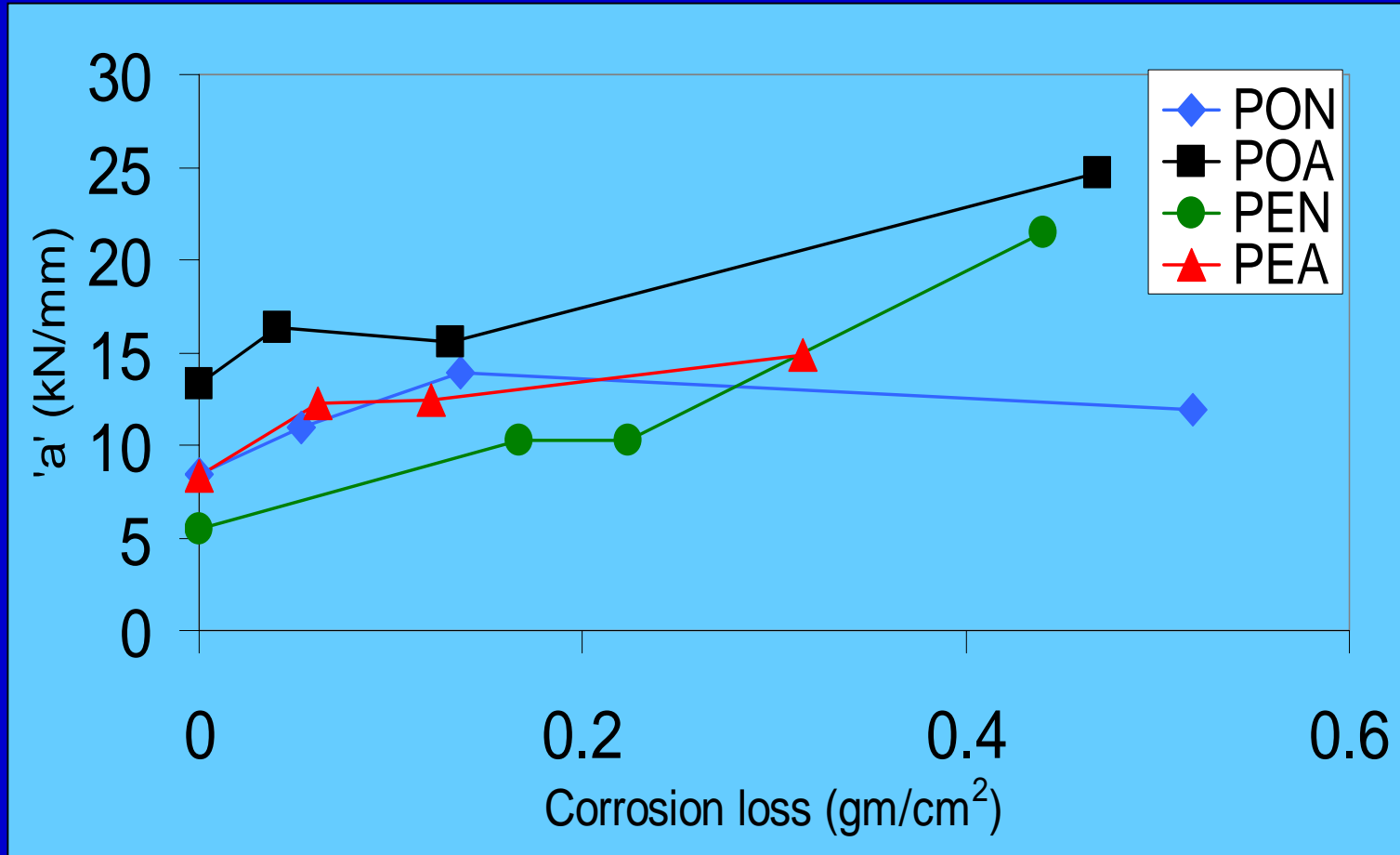
Results and Discussion

Stiffness Degradation (Contd...)



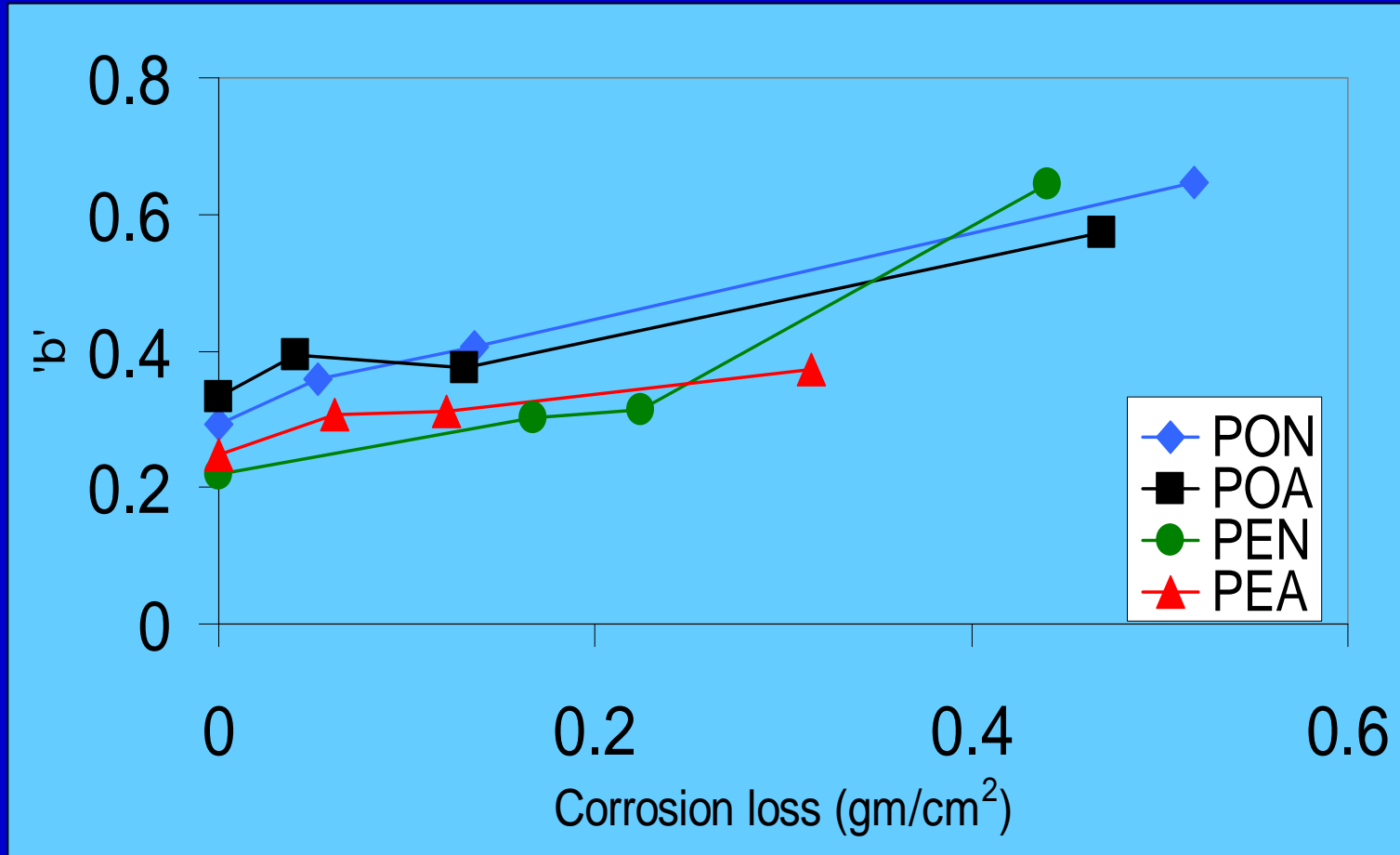
Results and Discussion

Stiffness Degradation (Contd....)



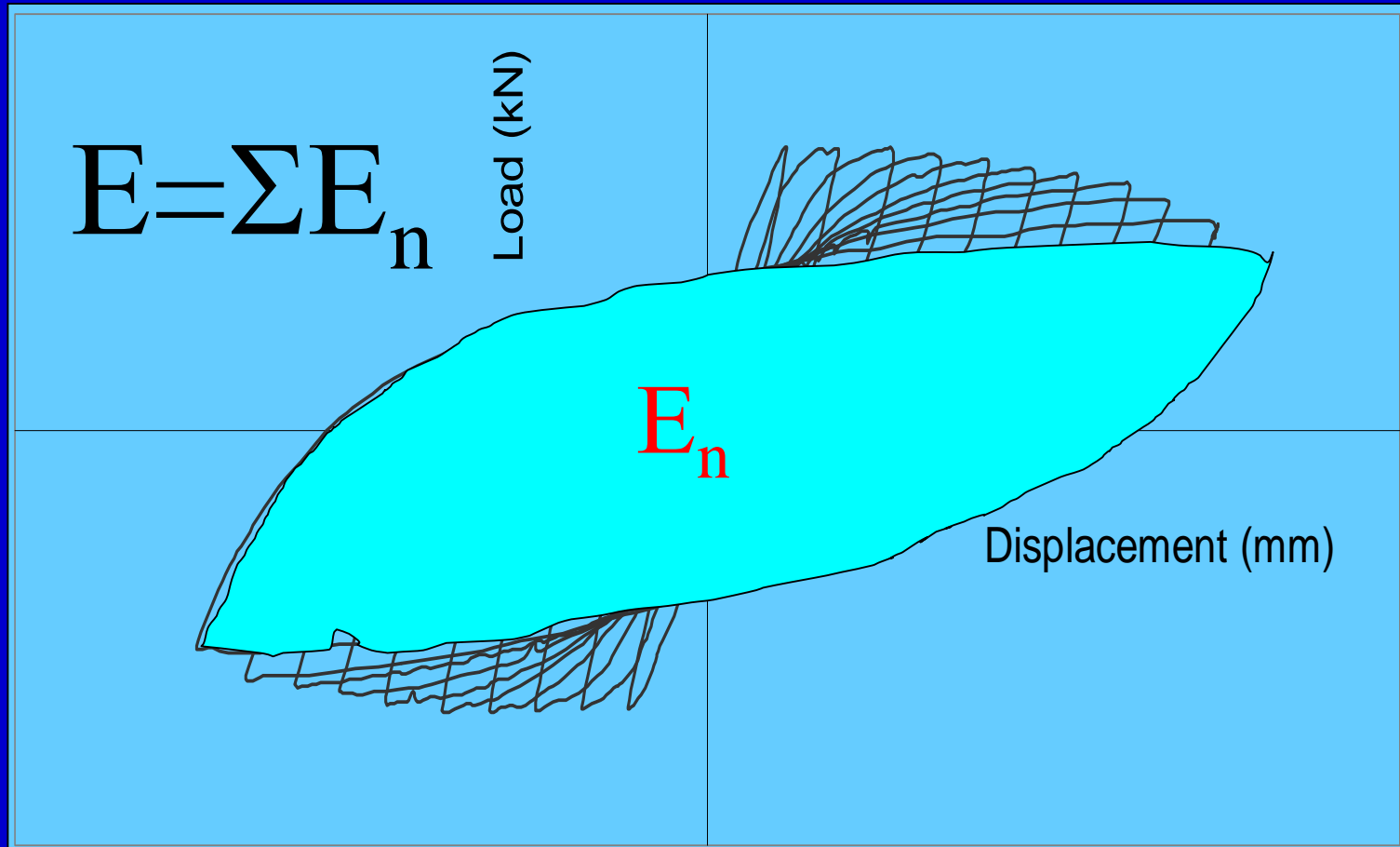
Results and Discussion

Stiffness Degradation (Contd....)



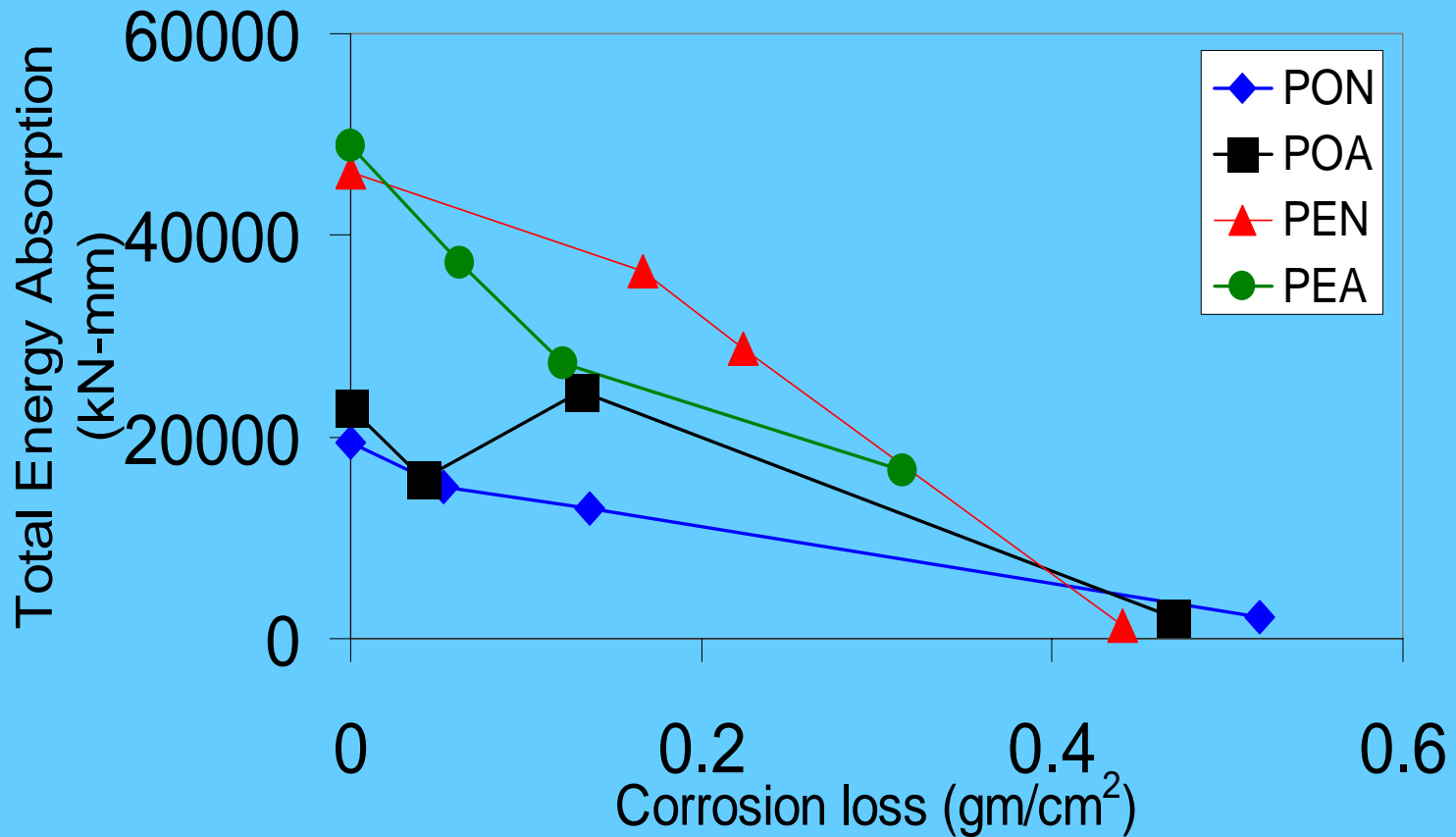
Results and Discussion

Energy Absorption Degradation



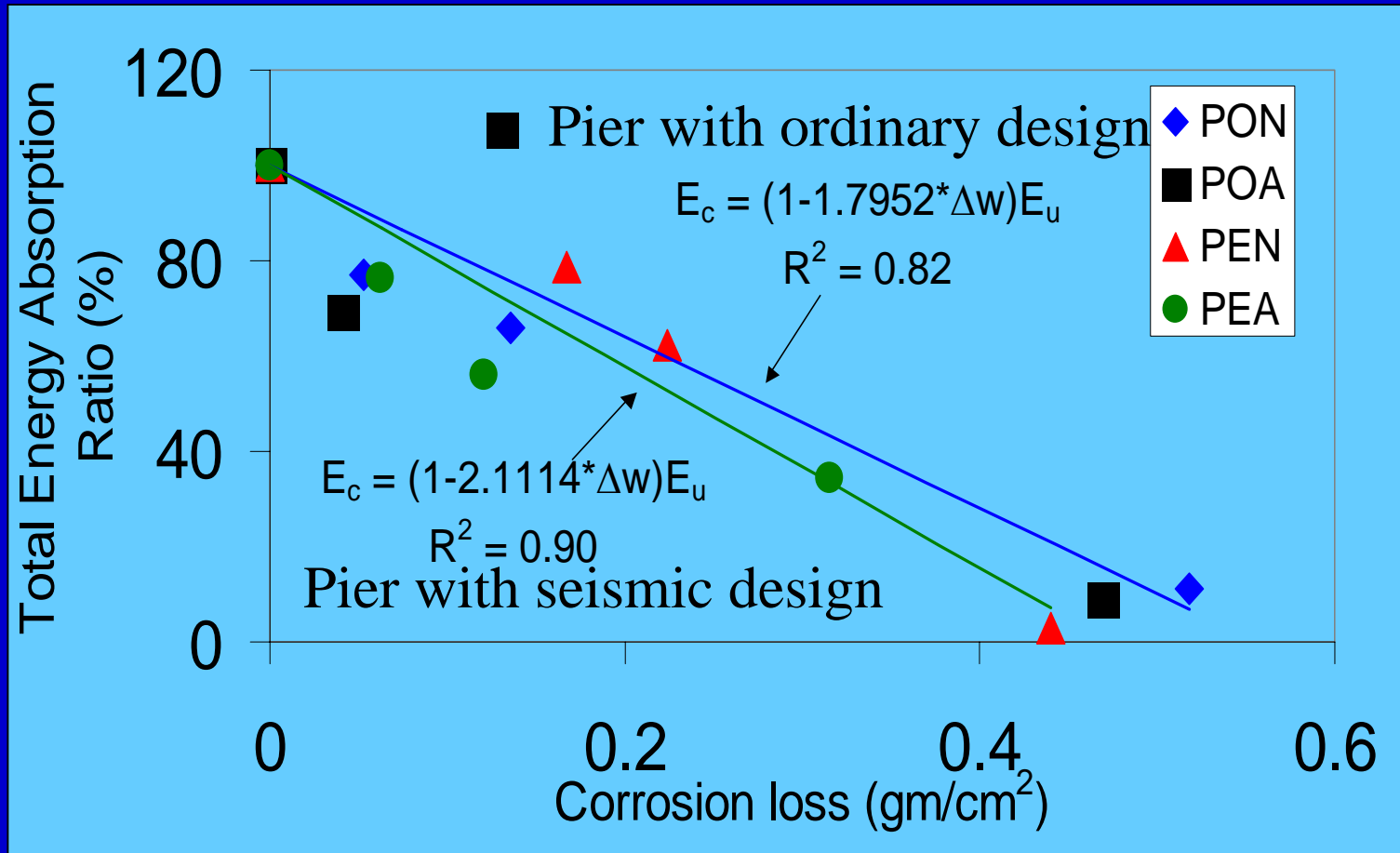
Results and Discussion

Energy Absorption Degradation



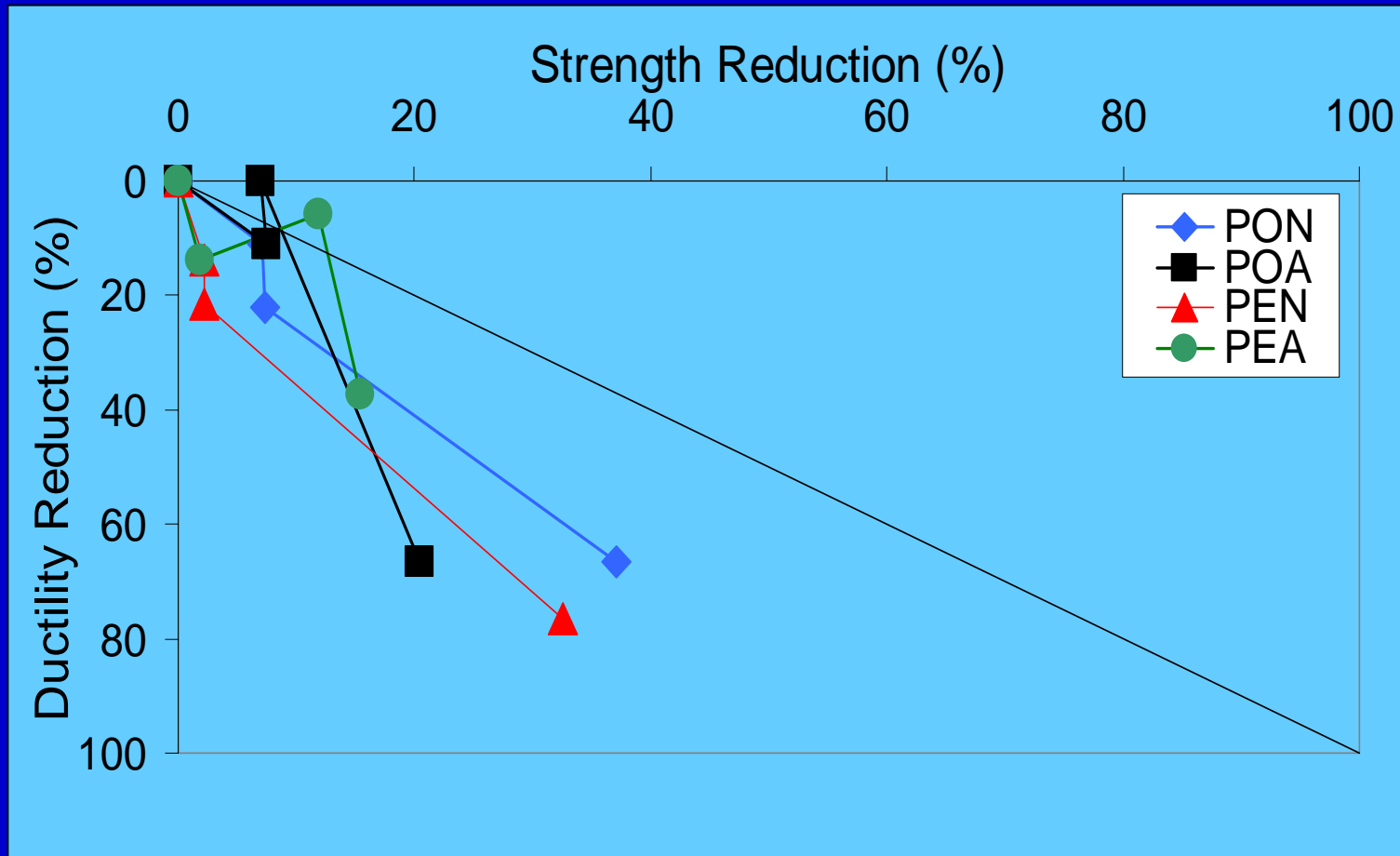
Results and Discussion

Energy Absorption Degradation (Contd...)



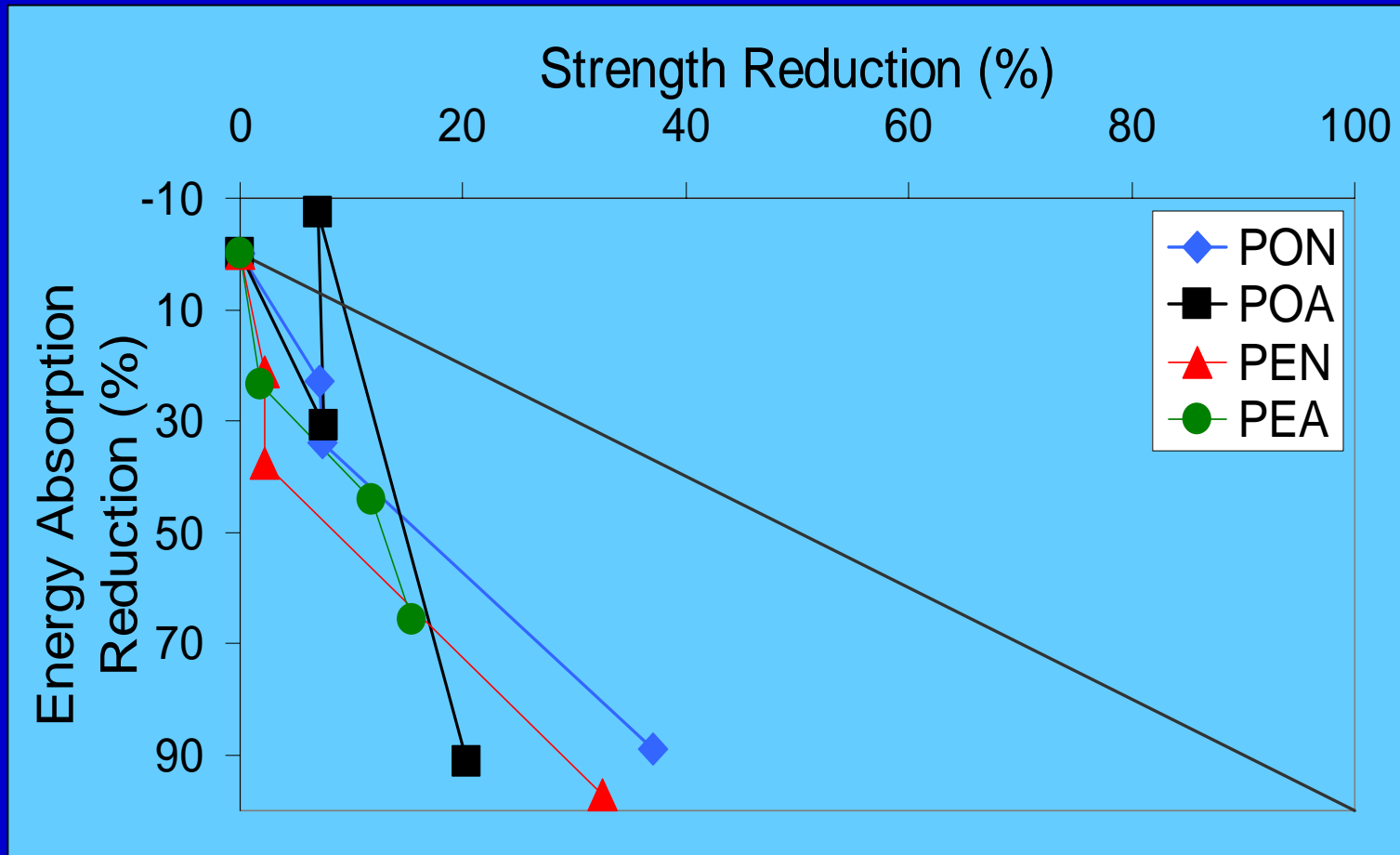
Results and Discussion

Comparison of Strength and Ductility



Results and Discussion

Comparison of Strength and Energy Absorption



Conclusions

- Seismic performances of reinforced concrete structures are seriously affected by corrosion of reinforcement.
- Strength of the pier is slightly reduced with the small increase in corrosion loss and with further increase degradation rate of strength is larger.

Conclusions

- Small corrosion amount in reinforcement increases stiffness significantly. However, within few cycles it degrades quickly
- With the increase in the corrosion loss of reinforcing bars, reduction rate of ductility and energy absorption of the pier is much higher than that of strength

Final Remarks

Final remarks

Problems awaiting solutions in near future

- To complete modeling performance degradation of structure with reinforcement corrosion process
- To evaluate environmental condition more correctly
- To evaluate construction works, including compaction, curing , etc.
- To establish life cycle cost evaluation method
- To systematize maintenance
- To establish total monitoring system including predictions of both chloride penetration and corrosion of reinforcement

